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EPA IM240 & Evap Technical Guidance

A Printed on Recycled Paper

IM240 & Evap Technical Guidance

Transportation and Regional Programs Division Office of Transportation and Air Quality U.S. Environmental Protection Agency

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This technical report does not necessarily represent final EPA decisions or positions. It is intended to present technical analysis of issues using data which are currently available. The purpose in the release of such reports is to facilitate the exchange of technical information and to inform the public of technical developments which may form the basis for a final EPA decision, position, or regulatory action.

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Introduction

This document is the successor to the August 1998 version of the EPA "IM240 & Evap Technical Guidance" and incorporates changes made since its publication. The following changes have been incorporated in this release of the EPA I/M technical guidance:

1) All references to the EPA evaporative emission purge test have been removed. Standards, procedures, specifications, and quality control practices are described in the August 1998 technical guidance.

2) A spreadsheet and example for usage of the Modal Fast Pass concept have been posted with the IM240 & Evap Technical Guidance on the EPA I/M web site..

3) K1 and K2 coefficients have been changed in 85.2205(b)(3)(iv)(E) to make them technically correct.

4) The exponent in the humidity correction factor in 85.2205(b)(3)(xi)(F) has been corrected for a typographical error.

5) References to procedures for treatment of OBD II evaporative emission controlled vehicles have been revised to state that guidance for these vehicles will be published in a separate document, not a revision of the IM240 & Evap Technical Guidance.

6) The standard for the fuel inlet pressure test, 85.2205(d)(2)(i) has corrected a typographical error. The value "8" has been changed to "6."

7) 85.2222(a)(2) has added a sentence stating fuel volatility is also a factor contributing to test variability when conducting the fuel inlet pressure test.

8) 85.2226(a)(3)(iii) has been revised to specify response time measurements at 2000, base inertia, and 5500 pounds of inertia.

9) 85.2227(b)(1)(i) has been added to specifically permit the use of flow based leak detection methods, but no standards have been proposed at present.

10) The text in 85.2227(c)(1)(iv) has been revised to clarify the term "automated." The new wording states automatic operation means automated measurement of the pass/fail condition <u>and</u> a requirement for a real time data link.

11) Paragraphs (ii) and (iii) of 85.2234 have been modified to provide more flexible load settings at 50 and 20 mph to achieve longer and more measurable coast down times. The 22 to 18 mph coastdown limit has been changed to ± 6 seconds.

12) The 0.4% of point tolerance in 85.2234(d)(3) has been revised to $\pm 2\%$ of point of a specific analyzer range, and the first sentence is modified to state its intent is to apply to the initial setting of a span point.

13) Paragraph 4 of 85.2234(g)(4) has been revised to state that driving trace quality is an example of how control charts for individual inspectors may used.

14) An equation has been added to 85.2239(b)(6) to define how "gpme" is calculated.

15) Appendix I, Derivation of GTRL Coefficients has been revised to clarify its content, and make it more compatible with terms and equations provided by Sierra Research in the supporting documentation when the EPA I/M Look-up Table is revised.

§85.2205 Test Standards

(a) IM240 Emission Standards

- (1) <u>Two Ways to Pass Standards</u>. If the corrected, composite emission rates calculated in §85.2205(b) exceed the standards for any exhaust component, additional analysis of test results shall look at the second phase of the driving cycle separately. Phase 2 shall include second 94 through second 239. Second-by-second emission rates in grams, and composite emission rates in grams per mile for Phase 2 and for the entire test shall be recorded for each gas. If the composite emission level is equal to or below the composite standard, or if the Phase 2 grams per mile emission level is equal to or below the applicable Phase 2 standard, then the vehicle shall pass the test for that exhaust component.
- (2) <u>Start-up Standards</u>. Start-up standards should be used during the first two years of program operation. Tier 1 standards are recommended for 1996 and newer vehicles and may be used for 1994 and newer vehicles certified to Tier 1 standards as well. The following exhaust emissions standards, in grams per mile, are recommended:

(i) <u>Light Duty Vehicles</u>.

Model Years	<u>Hydroca</u> Composite	<u>rbons</u> Phase 2	Carbon Mo Composite	onoxide Phase 2	Oxides of Composite	
1996+	0.80	0.50	15.0	12.0	2.0	2.0
1991-1995	1.20	0.75	20.0	16.0	2.5	2.5
1983-1990	2.00	1.25	30.0	24.0	3.0	3.0
1981-1982	2.00	1.25	60.0	48.0	3.0	3.0
1980	2.00	1.25	60.0	48.0	6.0	6.0
1977-1979	7.50	5.00	90.0	72.0	6.0	6.0
1975-1976	7.50	5.00	90.0	72.0	9.0	9.0
1973-1974	10.0	6.00	150	120	9.0	9.0
1968-1972	10.0	6.00	150	120	10.0	10.0

(ii) <u>High-Altitude Light Duty Vehicles</u>.

Model Years	Hydrocarbons		Carbon Mo	onoxide	Oxide Oxides of Nitro	
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2
1983-1984	2.00	1.25	60.0	48.0	3.0	3.0
1982	2.00	1.25	75.0	60.0	3.0	3.0

(iii) Light Duty Trucks (0 - 6000 pounds GVWR).

Model Years	Hydrocarbons		Carbon Mo	onoxide	Oxides of	Nitrogen
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2
1996+						
(<u><</u> 3750 LVW)	0.80	0.50	15.0	12.0	2.0	2.0
(>3750 LVW)	1.00	0.63	20.0	16.0	2.5	2.5
1991-1995	2.40	1.50	60.0	48.0	3.0	3.0
1988-1990	3.20	2.00	80.0	64.0	3.5	3.5
1984-1987	3.20	2.00	80.0	64.0	7.0	7.0
1979-1983	7.50	5.00	100	80.0	7.0	7.0

1975-1978	8.00	5.00	120	96.0	9.0	9.0
1973-1974	10.0	6.00	150	120	9.0	9.0
1968-1972	10.0	6.00	150	120	10.0	10.0

(iv) High-Altitude Light Duty Trucks (0 - 6000 pounds GVWR).

Model Years	Hydrocarbons		Carbon Mo	onoxide	Oxides of Nitrogen	
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2
1991+	3.00	2.00	70.0	56.0	3.0	3.0
1988-1990	4.00	2.50	90.0	72.0	3.5	3.5
1984-1987	4.00	2.50	90.0	72.0	7.0	7.0
1982-1983	8.00	5.00	130	104	7.0	7.0

(v) Light Duty Trucks (6001 - 8500 pounds GVWR).

Model Years	Hydrocarbons		Carbon Mo	onoxide	Oxides of	Nitrogen
	Composite	Phase 2	Composite	Phase 2	Composit	ePhase 2
1996+						
(<u><</u> 5750 ALVW)	1.00	0.63	20.0	16.0	2.5	2.5
(>5750 ALVW)	2.40	1.50	60.0	48.0	4.0	4.0
1991-1995	2.40	1.50	60.0	48.0	4.5	4.5
1988-1990	3.20	2.00	80.0	64.0	5.0	5.0
1984-1987	3.20	2.00	80.0	64.0	7.0	7.0
1979-1983	7.50	5.00	100	80.0	7.0	7.0
1975-1978	8.00	5.00	120	96.0	9.0	9.0
1973-1974	10.0	6.00	150	120	9.0	9.0
1968-1972	10.0	6.00	150	120	10.0	10.0

(vi) High-Altitude Light Duty Trucks (6001 - 8500 pounds GVWR).

Model Years	Hydrocarbons		Carbon Mo	onoxide	Oxides of Nit	
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2
1991+	3.00	2.00	70.0	56.0	4.5	4.5
1988-1990	4.00	2.50	90.0	72.0	5.0	5.0
1984-1987	4.00	2.50	90.0	72.0	7.0	7.0
1982-1983	8.00	5.00	130	104	7.0	7.0

(vii) <u>Heavy-Duty Trucks (greater than 8500 pounds GVWR).</u>¹

Model Years	Hydrocarbons		Carbon Mo	Carbon Monoxide		Oxides of Nitrogen	
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2	
1998+	2.00	1.30	30.0	24.0	4.0	4.0	
1991-1997	3.00	1.90	60.0	48.0	6.0	6.0	
1987-1990	3.00	1.90	60.0	48.0	8.0	8.0	

¹ The heavy-duty truck standards provided here were calculated using new vehicle certification standards and have not been subjected to field testing. This document provides no other guidance on heavy duty truck testing. Thus, anyone interested in performing IM240 tests on heavy-duty trucks should proceed with appropriate caution.

1985-1986	5.00	3.10	75.0	60.0	8.0	8.0
1979-1984	6.00	3.80	100.0	80.0	8.0	8.0
1974-1978	10.0	6.30	150.0	120.0	10.0	10.0
1970-1973	10.0	6.30	175.0	140.0	10.0	10.0
pre-1970	20.0	12.50	200.0	160.0	15.0	15.0

(3) <u>Final Standards</u>. The following exhaust emissions standards, in grams per mile, are recommended for vehicles tested in the calendar years 1997 and later. Tier 1 standards are recommended for all 1996 and newer vehicles but may be used for 1994 and newer vehicles.

(i) <u>Light Duty Vehicles</u>.

Model Years	Hydrocarbons		Carbon Mo	Carbon Monoxide		Oxides of Nitrogen	
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2	
1996+	0.60	0.40	10.0	8.0	1.5	1.5	
1983-1995	0.80	0.50	15.0	12.0	2.0	2.0	
1981-1982	0.80	0.50	30.0	24.0	2.0	2.0	
1980	0.80	0.50	30.0	24.0	4.0	4.0	
1977-1979	3.00	2.00	65.0	52.0	4.0	4.0	
1975-1976	3.00	2.00	65.0	52.0	6.0	6.0	
1973-1974	7.00	4.50	120	96.0	6.0	6.0	
1968-1972	7.00	4.50	120	96.0	7.0	7.0	

(ii) <u>High-Altitude Light Duty Vehicles</u>.

2 Composite Dhase 2 Composite Dhe	
2 Composite Phase 2 Composite Pha	se 2

(iii) Light Duty Trucks (0 - 6000 pounds GVWR).

Model Years	Hydrocarbons		Hydrocarbons Carbon Monoxide		Oxides of	Nitrogen
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2
1996+						
(<u><</u> 3750 LVW)	0.60	0.40	10.0	8.0	1.5	1.5
(>3750 LVW)	0.80	0.50	13.0	10.0	1.8	1.8
1988-1995	1.60	1.00	40.0	32.0	2.5	2.5
1984-1987	1.60	1.00	40.0	32.0	4.5	4.5
1979-1983	3.40	2.00	70.0	56.0	4.5	4.5
1975-1978	4.00	2.50	80.0	64.0	6.0	6.0
1973-1974	7.00	4.50	120	96.0	6.0	6.0
1968-1972	7.00	4.50	120	96.0	7.0	7.0

(iv) <u>High-Altitude Light Duty Trucks (0 - 6000 pounds GVWR)</u>.

Model Years	Hydrocarbons		Carbon Mo	onoxide	Oxides of	Nitrogen
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2
1988+	2.00	1.25	60.0	48.0	2.5	2.5
1984-1987	2.00	1.25	60.0	48.0	4.5	4.5

1982-1983

90.0

72.0

4.5 4.5

(v) Light Duty Trucks (6001 - 8500 pounds GVWR).

Model Years	Hydrocarbons		ars <u>Hydrocarbons</u> <u>Carbon Monoxide</u>		Oxides of 1	Nitrogen
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2
1996+						
(<5750 ALVW)	0.80	0.50	13.0	10.0	1.8	1.8
(>5750 ALVW)	0.80	0.50	15.0	12.0	2.0	2.0
1988-1995	1.60	1.00	40.0	32.0	3.5	3.5
1984-1987	1.60	1.00	40.0	32.0	4.5	4.5
1979-1983	3.40	2.00	70.0	56.0	4.5	4.5
1975-1978	4.00	2.50	80.0	64.0	6.0	6.0
1973-1974	7.00	4.50	120	96.0	6.0	6.0
1968-1972	7.00	4.50	120	96.0	7.0	7.0

(vi) High-Altitude Light Duty Trucks (6001 - 8500 pounds GVWR).

Model Years	Hydrocarbons		Carbon Mo	onoxide	Oxides of	<u>Nitrogen</u>
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2
1988+	2.00	1.25	60.0	48.0	3.5	3.5
1984-1987	2.00	1.25	60.0	48.0	4.5	4.5
1982-1983	4.00	2.50	90.0	72.0	4.5	4.5

(vii) Heavy-Duty Trucks (greater than 8500 pounds GVWR).

Model Years	Hydrocarbons					<u>Nitrogen</u>
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2
1998+	2.00	1.30	30.0	24.0	4.0	4.0
1991-1997	2.00	1.30	40.0	32.0	5.0	5.0
1987-1990	2.00	1.30	40.0	32.0	6.0	6.0
1985-1986	3.00	1.90	50.0	40.0	6.0	6.0
1979-1984	5.00	3.10	75.0	60.0	6.0	6.0
1974-1978	10.0	6.30	150.0	120.0	10.0	10.0
1970-1973	10.0	6.30	175.0	140.0	10.0	10.0
pre-1970	20.0	12.50	200.0	160.0	15.0	15.0

(4) <u>Fast-Pass</u>. Vehicles may be fast-passed using the following algorithm.

- (i) <u>Fast-Pass Algorithm</u>. Beginning at second 30 of the driving cycle, cumulative secondby-second emission levels for each second, calculated from the start of the cycle in grams, shall be compared to the cumulative fast-pass emission standards for the second under consideration. For exhaust components subject to Phase 2 standards, cumulative second-by-second emission levels calculated in grams from second 109 forward shall be compared to cumulative second-by-second fast-pass Phase 2 emission standards for the second under consideration.
- (ii) <u>Fast-Pass Standards</u>. A vehicle shall pass the IM240 for a given exhaust component if either of the following conditions occur:

- (A) cumulative emissions of each exhaust are below the full cycle fast-pass standard for the second under consideration; or,
- (B) at second 109 and later, (if the exhaust component is subject to Phase 2 standards) cumulative Phase 2 emissions of each exhaust component are below the Phase 2 fast-pass standards for the second under consideration;
- (iii) <u>Fast-Pass End of Test</u>. Testing may be terminated when fast-pass criteria are met for all subject exhaust components.
- (iv) <u>Applicability of Fast-Pass Standards</u>. If a fast-pass determination cannot be made for all subject exhaust components before the driving cycle ends, the pass/fail determination for each component shall be based on composite or Phase 2 emissions over the full driving cycle as described in §85.2205(a)(1).
- (v) <u>Fast-Pass Algorithms</u>. Vehicles may be fast-passed using other approaches if they are approved by the Administrator. States are encouraged to develop and use equations to define fast-pass standards for each composite emission standard rather than using tabular standards for each second of the test.

EPA-developed, tabular, fast-passed standards are included in Appendix A.

Fast-pass standards developed by Radian for Colorado are included in Appendix B.

Appendix C contains fast-pass standards generated by EPA for Wisconsin at the state's request. This was done to allow the state to move toward implementing final IM240 standards.

Appendix D contains fast-pass guidelines and 0.8 g/mi HC composite standards along with 0.5 g/mi HC Phase 2 cut points developed by Sierra Research under contract 68-C4-0056 Work Assignment 2-04. A complete listing of the modal regression coefficients would be too large to print in an appendix; however, the description in Appendix D is intended to provide background information and the rational behind this methodology. A complete series of coefficients are available on EPA's web site.

(b) Transient Test Score Calculations

(1) <u>Composite Scores</u>. The composite scores for the test shall be determined by dividing the sum of the mass of each exhaust component obtained in each second of the test by the number of miles driven in the test. The first data point is the sample taken from t=0 to t=1. The composite test value shall be calculated by the equation in §85.2205(b)(1)(i):

(i) Composite gpm
$$= \sum_{s=0}^{s} emissions(g) \\ \sum_{s=0}^{s} distance(miles)$$

Where: s = duration of test in seconds for fast pass = 239 seconds for complete IM240

(2) <u>Second-by-Second Mass Calculations</u>. The mass of each exhaust component shall be calculated to five significant digits for each second of the test using the following equations:

(i) Hydrocarbon mass:
$$HC_{mass} = V_{mix} * Density_{HC} * \frac{HC_{conc}}{1,000,000}$$

(ii) Carbon Monoxide mass:
$$CO_{mass} = V_{mix} * Density_{CO} * \frac{CO_{conc}}{1,000,000}$$

(iii) Oxides of Nitrogen mass: NOxmass =
$$V_{mix} * Density_{NO2} * K_H * \frac{NO_{conc}}{1,000,000}$$

(iv) Carbon Dioxide mass: CO2mass =
$$V_{mix} * Density_{CO2} * \frac{CO2_{conc}}{100}$$

(3) <u>Meaning of Terms</u>.

(i) V_{mix} = The CVS flow rate in cubic feet per second corrected to standard temperature and pressure.

- (ii) HC_{mass} = Hydrocarbon emissions in grams per second.
- (iii) Density_{HC} = Density of hydrocarbons is 16.33 grams per cubic foot assuming an average carbon to hydrogen ratio of 1:1.85 at 68°F and 760 mm Hg pressure.

(A)
$$HC_{conc} = HC_e - HC_d (1 - \frac{1}{DF})$$
 Where:

- (B) HC_e = Hydrocarbon concentration of the dilute exhaust sample, in ppm carbon equivalent.
- (C) HC_d = Background hydrocarbon concentration of the dilution air, in ppm carbon equivalent.

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(D) DF =
$$\frac{13.4}{\text{CO2}_{e} + (\text{HC}_{e} + \text{CO}_{e})*10^{-4}}$$

This is calculated on a second-by-second basis, where CO_2 is measured in % and HC and CO are measured in ppm. Note this DF does not account for pollutants in the background air and becomes less accurate as the airfuel ratio of the vehicle deviates from stoichiometric.

(E)
$$DF_{alt} = \frac{100 - K_1(CO_{2d}) - K_2(CO_d) - K_3(HC_d)}{K_1(CO_{2e} - CO_{2d}) + K_2(CO_e - CO_d) + K_3(HC_e - HC_d)}$$

This method of calculating DF is also done on a second-by-second basis and accounts for pollutants in the background air as well as being more accurate than the method in (D) above when the vehicle deviates from stoichiometric operation. All concentrations are expressed in volume percent and the values of the constants for gasoline fuel are: K1 = 7.4806, K2 = 5.5936, and K3 = 57.0945. Appendix E contains additional information on this subject.

If raw emission scores are being determined from dilute measurements, EPA recommends the use of this method for calculating DF.

- (v) CO_{mass} = Carbon monoxide emissions in grams per second.
- (vi) Density_{CO} = Density of carbon monoxide is 32.97 grams per cubic foot at 68° F and 760 mm Hg pressure.

(vii) CO_{conc} = Average carbon monoxide concentration per second of the dilute exhaust sample, corrected for background, water vapor, and CO₂ extraction, in ppm.

(A)
$$CO_{conc} = CO_e - CO_d (1 - \frac{1}{DF})$$

(B) CO_e = Carbon monoxide concentration of the dilute exhaust, in ppm.

(C)
$$CO_d$$
 = Background carbon monoxide concentration of the dilution air, in ppm.

- (viii) NO_{xmass} = Oxides of nitrogen emissions in grams per second.
- (ix) Density_{NO2} = Density of oxides of nitrogen is 54.16 grams per cubic foot assuming they are in the form of nitrogen dioxide at 68° F and 760 mm Hg pressure.
- (x) NO_{xconc} = Average concentration of oxides of nitrogen per second of the dilute exhaust sample, corrected for background in ppm.

(A)
$$NO_{xconc} = NO_{xe} - NO_{xd} (1 - \frac{1}{DF})$$

- (B) NO_{xe} = Oxides of nitrogen concentration of the dilute exhaust sample, in ppm.
- (C) $NO_{xd} = Background oxides of nitrogen concentration of the dilution air, in ppm.$
- (xi) K_H = humidity correction factor

$$K_{\rm H} = \frac{1.0}{1.0 - 0.0047 * (\rm H - 75.0)}$$

(B) H = Absolute humidity in grains of water per pound of dry air.

$$= \frac{43.478 * R_{a} * P_{d}}{P_{b} - (P_{d} * \frac{R_{a}}{100})}$$

(C) R_a = Relative humidity of the ambient air, percent.

(D)	Pd	=	Saturated vapor pressure, mm Hg at the ambient dry bulb temperature.
(E)	Pb	=	Barometric pressure, mm Hg.
(F)	Revised n	nethod	1^2
	К _Н	=	$e^{[0.004977(H-75)004447(T-75)]}$
(G)	Н	=	Absolute humidity in grains of water per pound of dry air.
(H)	Т	=	Temperature in °F.
	TE: If the caue of K _H shall		and $K_{\rm H}$ using either method of calculation is greater than 2.19, the et at 2.19.
(xiii) CO ₂₁	nass = C	Carboı	n dioxide emissions in grams per second.
(xiv) Densit			y of carbon dioxide is 51.81 grams per cubic foot at 68°F and m Hg.
(xv) CO _{2co}			ge carbon dioxide concentration per second of the dilute exhaust e, corrected for background, in percent.
(A)	CO _{2conc}	=	$CO_{2e} - CO_{2d} (1 - \frac{1}{DF})$
(B)	co _{2d}	=	Background carbon dioxide concentration of the dilution air, in

(4) <u>Negative Values</u>. Negative gram per second readings shall be integrated as zero and recorded as such. Negative values measured for ambient background concentrations (HC_d , CO_d , CO_{2d} , and NO_{xd}) used in 85.2205(b)(3) shall be calculated as zero and recorded as such.

percent.

(5) <u>Determination of Raw Exhaust Concentrations from IM240 Results</u>. Although the IM240 is a mass-based test, it is possible to estimate tailpipe concentrations from the dilute measurements for those vehicles only required to undergo an idle test. One method for performing this

²This revised method for calculating K_H as a function of both T and H is based on work performed by Sierra Research under contract 68-C4-0056, Work Assignment 2-04. If the calculated value of K_H exceeds 2.19, the value of K_H shall be set to 2.19. This analysis used the same MY69, 5-vehicle sample employed for the original K_H factor study that resulted in the current CFR standard K_H calculation method (listed in (xi)(A) above). However, in many cases IM testing occurs outside the temperature limits set by the CFR for the standard method; therefore, at this time EPA recommends using the revised method when testing above 86°F.

calculation can be found in SAE manuscript 980678. Additional clarification on this can be found in Appendix E.

(c) Evaporative System Pressure Test Standards

The methods described below are applicable to pre OBD II evaporative emission controlled vehicles. OBD II vehicles equipped with evaporative control monitors and certified to the enhanced evaporative emission standards are being phased-in with the 1996 through 1998 model years. Those vehicles must be tested using either OBD II scan tools, by measuring pressure loss through an evaporative emission "service port," or by following vehicle manufacturer specific instruction to avoid damaging rigid vapor lines which are prevalent on many vehicles equipped with enhanced evaporative emission control systems. Procedures for using OBD II scan tools will be published in a separate document.

All I/M programs conducting a pressure test must perform a leak check on the gas cap and provide a unique test result.

- <u>Visual Check</u>. The vehicle shall fail the evaporative system visual check if any part of the system is missing, damaged, improperly connected, or disconnected as described in §85.2222(b).
- (2) <u>Fuel Inlet Pressure Test.</u>
 - (i) <u>Pressure Test Method</u>. A vehicle shall fail the pressure test if the fuel vapor control system isolated between the fuel inlet and a clamp on the line between the fuel tank and the canister, (located as close to the canister as possible) loses more than 6 inches of water pressure over a period of 120 seconds starting from a stabilized pressure of 14 ± 1 inch of water.
 - (ii) <u>Fast-Pass</u>. Fast-pass determinations for the pressure test may be made anytime during the pressure decay between 20 and 120 seconds if the measured pressure exceeds:

$$P_{m} = P_{i} - (\frac{0.33 * P_{i} + 1.33}{120}) * t$$

Where: P_m = Measured pressure in inches of water

 P_i = Initial pressure in inches of water

t = Time in seconds

(d) Gas Cap Test Standards

The methods described below are applicable to pre OBD II evaporative emission controlled vehicles. OBD II vehicles equipped with evaporative control monitors and certified to the enhanced evaporative emission standards are being phased-in with the 1996 through 1998 model years. Procedures for OBD vehicles will be published in a separate document.

Pressure decay methods using a 1 liter head space are currently permitted under the June 1996 version of the IM240 technical guidance. As this method has been widely used in IM240 testing it will continue to be allowed. The pressure decay loss of 6 inches of WC from a starting pressure of 28 in. WC referenced to 70F and 1 atm and assuming a 1 liter head space, equates to a flow rate of about 80 cc/min.

- (1) <u>Visual Check</u>. The vehicle shall fail the gas cap visual check if the cap is missing, obviously defective, or the wrong style cap for the vehicle. An example of a wrong style includes a cam lock cap installed on fill pipe which requires a threaded cap. States conducting cap testing should work with OEM suppliers to develop a user friendly method of identifying wrong style gas caps.
- (2) <u>Pressure Decay Test Standard</u>. For pressure decay methods using a 1 liter head space and the June 1996 IM240 technical guidance, the fuel cap shall fail the pressure test if it loses more than 6 inches of water column (WC) pressure over a period of 10 seconds from a starting pressure of 28±1 inch WC.
- (3) <u>60 cc/min Flow Standard</u>. The gas cap leak rate may be determined by pressure loss measurement, direct flow measurement, or flow comparison methods and shall be compared to a pass/fail flow rate standard of 60 cubic centimeters per minute of air at 30 inches of water column. The flow rate methods shall be referenced to standard conditions of 70°F and 1 atm. If the leak rate exceeds 60 cc/min at a pressure of 30 inches of water column, the cap shall fail the test.

§85.2221 IM240 Test Procedures

(a) General Requirements

- (1) <u>Test Parameters</u>. The following information shall be determined for the vehicle being tested and used to automatically select the dynamometer inertia, power absorption settings, and evaporative emission test parameters.
 - (i) Model Year
 - (ii) Manufacturer
 - (iii) Model name
 - (iv) Body style
 - (v) Number of cylinders
 - (vi) Engine displacement

Alternative computerized methods of selecting dynamometer test conditions, such as VIN decoding, may be used.

- (2) <u>Ambient Conditions</u>. The ambient temperature, absolute humidity, and barometric pressure shall be recorded continuously during the transient test, or as a single set of readings if taken less than 4 minutes prior to the transient driving cycle.
- (3) <u>Restart</u>. If shut off, the vehicle shall be restarted as soon as possible before the test and shall be running at least 30 seconds prior to the transient driving cycle.

(b) **Pre-inspection and Preparation**

- (1) <u>Accessories</u>. All accessories (air conditioning, heat, defogger, radio, automatic traction control if switchable, etc.) shall be turned off by the inspector, if necessary.
- (2) <u>Traction Control and Four-Wheel Drive (4WD).</u> Vehicles with traction control systems that cannot be turned off shall not be tested on two wheel drive dynamometers. Vehicles with 4WD that cannot be turned off shall only be tested on 4WD dynamometers. If the 4WD function can be disabled, then 4WD vehicles may be tested on two wheel drive dynamometers.
- (3) <u>Leaks</u>. The vehicle shall be inspected for exhaust leaks. Audio assessment while blocking exhaust flow, or measurement of carbon dioxide or other gases, shall be acceptable. Vehicles with leaking exhaust systems shall be rejected from testing.
- (4) <u>Operating Temperature</u>. The vehicle temperature gauge, if equipped and operating, shall be checked to assess temperature. If the temperature gauge indicates that the engine is well below (less than 180°F) normal operating temperature, the vehicle shall not be fast-failed and shall get a second-chance emission test if it fails the initial test for any criteria exhaust component. Vehicles in overheated condition shall be rejected from testing.
- (5) <u>Tire Condition</u>. Vehicles shall be rejected from testing if tire cords, bubbles, cuts, or other damage are visible. Vehicles shall be rejected that have space-saver spare tires, or unreasonably sized tires on the drive axle. Vehicle tires shall be visually checked for adequate pressure level. Drive wheel tires that appear low shall be inflated to approximately 30 psi, or to tire side wall

pressure, or manufacturer's recommendation. The tires of vehicles being tested for the purposes of program evaluation under \$51.353(c) shall have their tires inflated to tire side wall pressure.

(6) <u>Ambient Background</u>. Background concentrations of hydrocarbons, carbon monoxide, oxides of nitrogen, and carbon dioxide (HC, CO, NO_X , and CO_2 , respectively) shall be sampled as specified in §85.2226(b)(2)(iv) to determine background concentration of dilution air. The sample shall be taken for a minimum of 15 seconds within 120 seconds of the start of the transient driving cycle, using the same analyzers used to measure tailpipe emissions except as provided in §85.2226(c)(4)(iv). Average readings over the 15 seconds for each gas shall be recorded in the test record. Testing shall be prevented until the average ambient background levels are less than 20 ppmC HC, 30 ppm CO, and 2 ppm NO_X , or outside ambient air levels (not influenced by station exhaust), whichever are greater.

Other methods that do not employ a fixed analysis time of 15 seconds may be used, if approved by the Administrator.

(7) <u>Sample System Purge</u>. While a lane is in operation, the CVS shall continuously purge the CVS hose between tests. The blower may be turned off if the CVS is not in operation, but the system shall be purged for 2 minutes prior to the start of a test if the blower has been turned off. The off time shall be computer monitored and recorded to a history file for quality assurance.

(c) Equipment Positioning and Settings

- (1) <u>Roll Rotation</u>. The vehicle shall be maneuvered onto the dynamometer with the drive wheels positioned on the dynamometer rolls. Prior to test initiation, the rolls shall be rotated until the vehicle laterally stabilizes on the dynamometer. Drive wheel tires shall be dried if necessary to prevent slippage during the initial acceleration.
- (2) <u>Cooling System</u>. The use of a cooling system is optional when testing at temperatures below 50°F. Furthermore, the hood may be opened at the state's discretion. If a cooling system is in use, testing shall not begin until the cooling system is positioned and activated. The cooling system shall be positioned to direct air to the vehicle cooling system, but shall not be directed at the catalytic converter.
- (3) <u>Vehicle Restraint</u>. Testing shall not begin until the vehicle is restrained. Any restraint system shall meet the requirements of §85.2226(a)(5)(vii). The parking brake shall be set for front wheel drive vehicles prior to the start of the test. The parking brake need not be set for vehicles that release the parking brake automatically when the transmission is put in gear.
- (4) <u>Dynamometer Settings</u>. Dynamometer power absorption and inertia weight settings shall be automatically chosen from an EPA-supplied electronic look-up table which will be referenced based upon the vehicle identification information obtained in 85.2221(a)(1). Vehicles not listed shall be tested using default power absorption and inertia settings in the latest version of the EPA I/M Look-up Table, as posted on EPA's web site: www.epa.gov/orcdizux/im.htm
- (5) <u>Exhaust Collection System</u>. The exhaust collection system shall be positioned to insure complete capture of the entire exhaust stream from the tailpipe during the transient driving cycle. The system shall meet the requirements of §85.2226(b)(2).

(d) Vehicle Conditioning

- Queuing Time. When the vehicle queue exceeds 20 minutes, a vehicle shall get a secondchance emission test if it fails the initial test and all criteria exhaust components are at or below 1.5 times the standard. At the state's discretion, second-chance testing may be granted if criteria exhaust components exceed any preset level above the standard.
- (2) <u>Program Evaluation</u>. Vehicles being tested for the purpose of program evaluation under §51.353(c) shall receive two full transient emission tests (i.e., a full 240 seconds each). Results from both tests and the test order shall be separately recorded in the test record. Emission scores and results provided to the motorist may be from either test.
- (3) <u>Discretionary Preconditioning</u>.
 - Any vehicle may be preconditioned by maneuvering the vehicle on to the dynamometer and driving the 94 to 239 second segment of the transient cycle in 85.2221(e)(1). This method has been demonstrated to adequately precondition the vast majority of vehicles (SAE 962091).

Other preconditioning cycles may be developed and used if approved by the Administrator.

 (ii) Alternatively, modal analysis of the failing second-by-second test data may be performed to identify vehicles that would benefit from additional pre-conditioning. Appendix F provides retest criteria developed by Sierra Research under EPA contract 68-C4-0056 Work Assignment 2-04.

(e) Vehicle Emission Test Sequence

(1)	Transient Driving Cycle.	The vehicle shall be driven over the following cycle:
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Time second	Speed mph	Time second	Speed mph	Time second	Speed mph	Time second	Speed mph	Time second	Speed mph
0	0	48	25.7	96	0	144	24.6	192	54.6
1	0	48 49	26.1	90 97	0	144	24.0 24.6	192	54.8
2	0	50	26.7	98	3.3	145	24.0	193	55.1
3	0	50	27.5	99	6.6	140	25.6	195	55.5
4	0	52	28.6	100	9.9	147	25.7	196	55.7
5	3	52	29.3	100	13.2	149	25.4	190	56.1
6	5.9	54	29.8	101	16.5	150	24.9	197	56.3
7	8.6	55	30.1	102	19.8	150	24.)	199	56.6
8	11.5	56	30.4	103	22.2	151	25.4	200	56.7
9	14.3	57	30.7	105	24.3	152	26	200	56.7
10	16.9	58	30.7	105	25.8	155	26	201	56.3
10	17.3	59	30.5	100	26.4	154	25.7	202	56
11	18.1	60	30.4	107	25.7	155	26.1	203	55
12	20.7	61	30.4	103	25.1	150	26.7	204	53.4
13	21.7	62	30.4	110	24.7	157	27.3	205	51.6
14	22.4	63	30.4	110	24.7	158	30.5	200	51.8
15	22.4	64	30.4	112	25.2	160	33.5	207	52.1
10	22.3	65	29.9	112	27.2	161	36.2	203	52.5
18	21.5	66	29.5	113	26.5	161	37.3	210	53
18	20.9	67	29.5	114	20.5	162	39.3	210	53.5
20	20.9	68	30.3	115	24	164	40.5	211 212	53.5 54
20	19.8	69	30.7	110	19.4	165	40.5	212	54.9
21	17.0	70	30.9	117	17.7	165	43.5	213	55.4
22	14.9	70	31	110	17.7	167	45.1	214	55.6
23	14.9	71	30.9	120	17.2	168	46	215	56
24	15.2	72	30.9	120	18.6	169	46.8	210	56
26	15.5	74	29.8	121	20	170	47.5	217	55.8
20	16	75	29.9	122	20.7	170	47.5	210	55.2
27	17.1	76	30.2	123	20.7	171	47.3	219	54.5
28	19.1	70	30.2	124	22.4	172	47.2	220	53.6
30	21.1	78	31.2	125	22.4	173	47.2	221	52.5
30	22.7	78	31.8	120	22.3	174	47.4	222	51.5
32	22.9	80	32.2	127	21.5	176	47.9	223	50.5
33	22.9	81	32.4	128	20.9	170	48.5	224	48
33	22.6	82	32.2	130	20.9	178	49.1	225	44.5
35	21.3	83	31.7	130	19.8	179	49.5	220	41
36	19	84	28.6	131	17.0	180	50	228	37.5
30	17.1	85	25.1	132	17.1	180	50.6	228	34
38	15.8	85	21.6	133	17.1	182	51	229	30.5
39	15.8	87	18.1	134	15.8	183	51.5	230	27
40	17.7	88	14.6	135	17.7	184	52.2	231	23.5
40	19.8	88 89	11.1	130	19.8	185	53.2	232	20
41 42	21.6	90	7.6	137	21.6	185	55.2 54.1	233	16.5
42	21.0	90	7.0	130	21.0	100	34.1	234	10.3

43							54.6		
44	24.2				24.5	188		236	9.5
45	24.6					189	55	237	6
46	24.9	94	0				54.9	238	2.5
47	25	95	0	143	24.7	191	54.6	239	0

- (2) <u>Driving Trace</u>. The inspector shall follow an electronic, visual depiction of the time/speed relationship of the transient driving cycle, or trace. The visual depiction of the trace shall be of sufficient magnification and adequate detail to allow accurate tracking by the driver and shall permit the driver to anticipate upcoming speed changes. The trace shall also clearly indicate gear shifts as specified in §85.2221(e)(3).
- (3) <u>Shift Schedule</u>. For vehicles with manual transmissions, inspectors shall shift gears according to the following shift schedule:

Shift Sequence (gear)	Speed (miles per hour)	Nominal Cycle Time (seconds)
1 - 2	15	9.3
2 - 3	25	47.0
De-clutch	15	87.9
1 - 2	15	101.6
2 - 3	25	105.5
3 - 2	17	119.0
2 - 3	25	145.8
3 - 4	40	163.6
4 - 5	45	167.0
5 - 6	50	180.0
De-clutch	15	234.5

Gear shifts shall occur at the points in the driving cycle where the specified speeds are obtained. For vehicles with fewer than six forward gears the same schedule shall be followed while disregarding shifts above the highest gear.

- (4) <u>Speed Excursion Limits</u>. Speed excursion limits shall apply as follows:
 - (i) <u>Upper Limit</u>. The upper limit is 2 mph higher than the highest point on the trace within 1 second of the given time.
 - (ii) <u>Lower Limit</u>. The lower limit is 2 mph lower than the lowest point on the trace within 1 second of the given time.
 - (iii) <u>Speed Variations</u>. Speed variations greater than the tolerances (such as may occur during gear changes) are acceptable provided they occur for no more than 2 seconds on any occasion.
 - (iv) <u>Underpowered Vehicles</u>. Speeds lower than those prescribed during accelerations are acceptable provided the vehicle is operated at maximum available power during such accelerations until the vehicle speed is within the excursion limits. If the vehicle is underpowered and unable to adequately follow the trace, it may at the State's discretion be rejected from testing or given an idle test.

- (v) <u>Exceedances</u>. Exceedances of the limits in §85.2221(5)(ii) through §85.2221(5)(iii) shall automatically result in a void test. The station manager can override the automatic void of a test if the manager determines that the conditions specified in §85.2221(e)(4)(iv) occurred.
- (5) <u>Speed Variation Limits</u>.
 - Limits. Based on work performed under contract 68-C4-0056, Work Assignment 2-04 the following Positive Kinetic Energy limits were developed by Sierra Research. These results are based on an analysis of 16,581 IM240 tests conducted in AZ.

(ii) PKE =
$$\sum_{t=0}^{t} PP_{t} \int_{x=0}^{x} dx$$

where: $PP_t = V_t^2 - V_{(t-1)}^2 \text{ mi}^2/\text{hr}^2 \text{ for } V_t > V_{(t-1)}$

 $PP_t = 0$ for $V_t = V_{(t-1)}$

x = distance (mi)

(iii) <u>PKE Limits</u>. Full Test PKE Limits:

Upper Limit 3456 mi/hr²

Lower Limit 3082 mi/hr²

NOTE: The test cycle shall be invalid for a pass/fail determination if the PKE value is below the lower limit for a passing vehicle or above the upper limit for a failing vehicle. PKE values alone should not be used to make an early pass/fail determination.

Test cycles with PKE values outside the lower and upper limits shall be valid for preconditioning provided that all other requirements are met.

- (iv) <u>Second-by-Second Limits</u>. Second-by-Second PKE upper and lower limits are listed in Appendix G.
- (6) <u>Distance Criteria</u>. The actual distance traveled for the transient driving shall be measured. If the absolute difference between the measured distance and the theoretical distance for the actual test exceeds 0.05 miles, the test shall be void.
- (7) <u>Vehicle Stalls</u>. Vehicle stalls during the test shall void the test and result in a new test. More than 3 stalls shall result in rejecting the vehicle from testing.

- (8) <u>Inertia Weight Selection</u>. The inertia weight selected for the vehicle shall be verified as specified in §85.2226(a)(1)(i). For systems employing electrical inertia simulation, an algorithm identifying the actual inertia force applied during the transient driving cycle shall be used to determine proper inertia simulation.
- (9) <u>CVS Operation</u>. The CVS operation shall be verified for each test for a CFV-type CVS by measuring either the absolute pressure difference across the venturi or measuring the blower vacuum behind the venturi for minimum levels needed to maintain choke flow for the venturi design. The operation of an SSV-type CVS shall be verified throughout the test by monitoring the difference in pressure between upstream and throat pressure. The minimum values shall be determined from system calibrations. Monitored pressure differences below the minimum values shall void the test.

(f) Emission Measurements

(1) <u>Exhaust Measurement</u>. The emission analysis system shall sample and record dilute exhaust HC, CO, CO₂, and NO_x during the transient driving cycle as described in \$85.2226(c).

§85.2222 Evaporative System Pressure and Gas Cap Test Procedures

(a) General Requirements

- (1) <u>Pressure Test</u>. The on-vehicle pressure tests described in §85.2222(c) shall be performed after any tailpipe emission test. Vehicles receiving a pressure test specified in §85.2222(c) should also be given a gas cap leak test specified in §§85.2222(d).
- (2) <u>Controlling Test Variability</u>. The pressure test shall be conducted in a manner that minimizes changes in temperature, since pressure measurements are affected by changes in the vapor space temperature. Volume compensation for the pressure test is not required, but the vapor space volume will affect the pressure decay measurement. Excessive fuel vapor pressure, although not controllable at the time of test, may affect the accuracy and repeatability of the result.
- (3) <u>Gas Cap Test Requirement</u>. A gas cap test described in §85.2222(d) may be performed before or after the tailpipe emission test.
- (4) <u>Alternative Techniques</u>. Alternative gas cap or pressure test procedures may be used if they are shown to be equivalent or better than those described below.

(b) **Pre-inspection and Preparation**

- (1) <u>Visual Inspection Canister</u>. The evaporative canister(s) shall be visually checked to the degree practical. A missing or obviously damaged canister(s) shall fail the visual evaporative system check.
- (2) <u>Visual Inspection System</u>. The evaporative system hoses shall be visually inspected for the appearance of proper routing, connection, and condition, to the degree practical. If any evaporative system hose is misrouted, disconnected, or damaged, the vehicle shall fail the visual evaporative system check.
- (3) <u>Visual Inspection Gas Cap</u>. If the gas cap is missing, obviously defective, or the wrong style cap for the vehicle, the vehicle shall fail the visual inspection.

(c) Fuel Inlet Pressure Test

- (1) Equipment Set-up. The vapor vent line(s) from the gas tank to the canister(s) shall be clamped off as close to the canister(s) as practical without damaging evaporative system hardware. Dual fuel tanks shall be checked individually if the complete vapor control system can not be accessed by pressurizing from the fill pipe interface of only one fuel tank. The proper adapter, as specified in §85.2227(c)(2)(i) shall be selected.
- (2) <u>Starting Pressure</u>. The gas tank shall be pressurized to 14±1 inch of WC, or a vehicle specific pressure as identified in the I/M Look-up Table.
- (3) <u>Stability</u>. Pressure stability shall be monitored for a period of 10 seconds prior to the start of the pressure decay measurement. One definition of stability is a loss of no more than 5 inches WC over a 10 second period when the initial pressure is 14±1 inch WC. If the loss of pressure in 10 seconds exceeds this value, two more attempts shall be made to reach stability. Failure to achieve stability likely indicates the presence of a large leak and therefore failure of the pressure test. Alternate definitions of stability may be proposed by the State and approved by the Administrator. Stability criteria for flow comparator or direct flow measurement methods do not apply.

- (4) <u>Volume Compensation</u>. Pressure decay measurements are affected by the vapor volume in the fuel tank. Volume-compensated pressure decay measurements are presently not required. By design, flow comparator or flow measurement methods do not require volume corrections.
- (5) <u>Pressure Monitoring</u>. Close the pressure source and measure the loss in pressure over a 120 second interval. Fast-pass determinations may be made using the equations in §85.2205(d)(2)(ii).
- (6) <u>Clamp Removal</u>. Remove the clamp on the vapor line and carefully relieve pressure and remove the adapter used to supply pressure to the vapor space.

(d) Gas Cap Test

- (1) <u>Cap Installation</u>. The fuel cap, or caps, shall be removed from the fuel inlet(s) and installed on a portable or bench test rig -using the adapter appropriate for the gas cap as specified in §85.2227(d)(1)(ii).
- (2) <u>Leak Measurement</u>. The gas cap leak rate shall be measured and compared against a 60 cc/min at 30 in. WC flow standard. Pressure decay measurement using instruments with a 1 liter head space shall be made from an initial pressure of 28 in. WC and be compared against a loss of 6 in. WC in 10 seconds.
- (3) <u>Cap Replacement</u>. The fuel cap(s) shall be replaced on the fuel inlet and tightened appropriately.

§85.2226 IM240 Equipment Specifications

(a) Dynamometer Specifications

- (1) <u>General Requirements</u>.
 - (i) <u>Capacity</u>. The dynamometer structure (e.g., bearings, rollers, pit plates, etc.) shall accommodate all light-duty vehicles and light-duty trucks up to 8500 pounds GVWR.
 - (ii) <u>Test Parameters</u>. Road load horsepower and inertia simulation shall be automatically selected from the EPA I/M Look-up Table, or equivalent data base, based on the vehicle parameters in the test record.
 - (iii) <u>Alternative Designs</u>. Alternative dynamometer specifications, designs, and error checking methods may be used if the alternative provides proper dynamometer loading over the IM240 driving cycle.
 - (iv) <u>Units</u>. Specifications in this section are generally expressed in units of horsepower. System designs using equivalent units of force, English or SI, are permissible.
 - (v) <u>Ambient Range</u>. The dynamometer shall be designed to meet specifications at an ambient temperature range of 35 to 110°F, and at absolute humidity values representative of the IM240 testing location.
- (2) <u>Power Absorption</u>.
 - (i) <u>Power Absorber Design</u>. The power absorber unit shall be an electric AC or DC motor/absorber design. Eddy current designs may be approved if proven equivalent to other designs in terms of inertia response time, total load, and emissions performance over an IM240 driving cycle.
 - (ii) <u>Range</u>.
 - (A) <u>Mechanical Inertia Dynamometers</u>. Dynamometers using clutchable flywheels shall have sufficient power absorber capacity to accommodate the TRLHP values in the EPA I/M Look-up Table.
 - (B) <u>Electric Inertia Dynamometers</u>. Dynamometers using a combination of mechanical base inertia and supplemental electrical inertia shall have sufficient power absorber capacity to accommodate the sum of the TRLHP values in the EPA I/M Look-up Table plus the power absorbed from accelerating a vehicle at 3.3 mph/sec at the equivalent test weight (ETW) specified in the I/M Look-up Table.
 - (iii) <u>Accuracy</u>. The power absorber shall be adjustable across the required horsepower range at 50 mph in 0.1 horsepower increments. The accuracy of the power absorber or power exchange unit, for road load simulation only, shall be ± 0.25 horsepower or $\pm 3\%$ of point, whichever is greater.
 - (iv) <u>Indicated Horsepower</u>. At constant velocity, the power absorber shall load the vehicle according the following equations:

IHP = TRLHP - PLHP - GTRL

Where: IHP is the dynamometer indicated, or set, horsepower.

TRLHP is the track, or total, horsepower for a particular vehicle.

PLHP is the dynamometer parasitic loss horsepower.

GTRL is the generic tire/roll loss of a vehicle on the dynamometer.

TRLHP, PLHP, GTRL, and therefore IHP, are all expressed as three term polynomials of the type:

 $HP = A*Obmph + B*Obmph^2 + C*Obmph^3$

Where: HP represents individual expressions relating IHP, TRLHP, PLHP, or GTRL as a function of velocity.

A, B, or C represent horsepower coefficients for the individual expressions relating IHP, TRLHP, PLHP, or GTRL as a function of velocity.

Obmph is the velocity in miles per hour.

Expressions for TRLHP, and GTRL are found in Appendices H and I.

- (3) <u>Inertia</u>.
 - <u>Range</u>. The dynamometer shall provide inertia simulation capability of 2000 to 5500 pounds for light duty vehicles and trucks less than or equal to 5500 pounds ETW. Dynamometers used for testing light duty vehicles and trucks over 5500 ETW shall have inertia simulation capability to set the inertia at the correct value as referenced in the EPA I/M Look-up Table.
 - (ii) <u>Mechanical Inertia Simulation</u>. The dynamometer shall be equipped with clutchable mechanical flywheels with inertia selectable to a 250 pound sensitivity. The tolerance on the base inertia weight and the flywheels shall be within 1% of the specified test weights. The test system shall be equipped with a method, independent from the flywheel selection system, that identifies which flywheels are actually rotating during the transient driving cycle.
 - (iii) <u>Electric Inertia Simulation</u>. Electric inertia simulation, or a combination of electric and mechanical simulation may be used in lieu of mechanical flywheels, provided that the performance of the electrically simulated inertia complies with the following specifications.
 - (A) <u>System Response</u>. The torque response to a step change shall be at least 90% of the command value within 200 milliseconds, and shall be within 2 percent of the commanded torque by 300 milliseconds after the command is issued. Any overshoot of the commanded torque value shall not exceed 25 percent of the torque value. Response time measurements shall be performed at 2000, base inertia, and 5500 pounds of inertia.
 - (B) <u>Simulation Error</u>. An inertia simulation error (ISE) shall be continuously calculated any time the actual dynamometer speed is between 10 and 60 mph. The average positive ISE over the driving cycle shall be calculated by the equation in \$85.2226(a)(3)(iii)(C), and shall not exceed 2 percent of the inertia weight selected (IW_s) for the vehicle under test.

(C) ISE =
$$\left(\frac{IW_{s} - I_{t}}{IW_{s}}\right) * 100$$

Where: ISE = Inertia simulation error expressed in percent.

 $IW_s = Total inertia desired, or selected, in pounds mass.$

 I_t = Total inertia being simulated by the dynamometer in pounds mass.

(D)
$$I_t = I_m + \frac{32.2}{V} \int_{t=0}^{t} (F_m - F_{rl}) dt$$

Where: $I_f = Total$ inertia being simulated by the dynamometer in pounds mass.

 I_m = Base mechanical inertia of the dynamometer in pounds mass.

 $32.2 = \text{Gravitational constant}, (ft)(lbm)/(lbf)(sec^2).$

V = Measured roll speed in feet/second.

 F_m = Force measured by the load cell converted to force at the roll surface in pounds.

 F_{rl} = Dynamometer road load expressed as a three term polynomial in pounds force at the measured roll speed.

t = Time in seconds.

(4) Dynamometer Parasitic Loss

- (i) <u>Friction Curves</u>. The dynamometer internal friction curves, typically bearing and windage friction expressed as a function of velocity, shall be capable of being automatically measured, stored, and accurately accounted for over the IM240 driving cycle.
- (ii) <u>Friction Curve Definition</u>. Parasitic loss friction shall be expressed in a tabular format as a function of velocity, or as a polynomial of the type:

 $PLHP = A_p * Obmph + B_p Obmph^2 + C_p Obmph^3$

Where: PLHP represents the dynamometer parasitic friction, expressed in horsepower.

 A_p , B_p , and C_p are coefficients relating a least squares fit of dynamometer friction and velocity.

Obmph is dynamometer roll surface velocity in miles per hour.

- (5) <u>Rolls</u>.
 - (i) <u>Size and Type</u>. The dynamometer shall be equipped with twin rolls. The rolls shall be coupled side to side. In addition, the front and rear rolls shall be coupled. The dynamometer roll diameter shall be between 8.5 and 21.0 inches. The spacing between the roll centers shall comply with the equation in §85.2226(a)(5)(iii). The dynamometer rolls shall accommodate an inside track width of 30 inches and an outside track width of at least 100 inches.
 - (ii) <u>Roll Installation</u>. Rolls shall be installed in the floor such that vehicles will be within ± 5 degrees of horizontal.
 - (iii) <u>Roll Spacing</u>. The spacing between the roll centers shall comply with the following equation to within +0.5 inches and -0.25 inches.

Roll Spacing = $(24.375 + D) * Sin 31.5^{\circ}$

Where: Roll Spacing is the distance between the roll centerlines in inches.

D = Roll diameter in inches

- (iv) <u>Roll Surface</u>. The surface finish and hardness shall be such that tire slippage is minimized when testing vehicles using the inertia weight and horsepower settings found in the EPA I/M Look-up Table while following the IM240 driving schedule, and that tire wear and noise are minimized. Knurled roll surfaces are acceptable.
- (v) <u>Test Distance and Vehicle Speed</u>. The total number of dynamometer roll revolutions shall be used to calculate the distance traveled. Pulse counters may be used to calculate the distance directly if there are at least 16 pulses per revolution. The measurement of the actual roll distance for the composite and each phase of the transient driving cycle shall be accurate to within ± 0.01 mile. The measurement of the roll speed shall be accurate to within ± 0.1 mph over the IM240 driving schedule.
- (vi) <u>Vehicle Lift</u>. A vehicle lift system located between the dynamometer rolls shall be provided to facilitate drive axle positioning and vehicle egress from the dynamometer.
- (vii) <u>Vehicle Restraint System</u>. The dynamometer shall include a system of safely restraining the forward and side-to-side motion of front wheel drive vehicles, and the forward motion of rear wheel drive vehicles during the IM240 driving schedule, while allowing unobstructed ingress and egress from the dynamometer.
- (6) <u>Load Cell</u>.
 - (i) <u>Torque Measurement</u>. The dynamometer shall have a torque measurement system accurate to within $\pm 2\%$ of full scale.
 - (ii) <u>Dead Weights</u>. Dead weights used to calibrate a torque meter or load cell shall be traceable to NIST and be accurate to within $\pm 0.5\%$.
 - (iii) <u>Dynamic Calibrations</u>. Designs using an F = MA method for calibrating the load cell are also acceptable.
- (7) <u>Driver's Aid</u>.

- (i) <u>Video Display</u>. The dynamometer shall be equipped with a video display device able to be easily positioned to accommodate all test vehicles while clearly visible to the driver. The display shall have a method that allows the driver to accurately and smoothly follow the desired driving cycle.
- (ii) <u>Remote Capabilities</u>. The dynamometer shall have a means of allowing the driver to start the test, perform an emergency stop, and perform other necessary and convenient functions related to the test while inside the vehicle.
- (8) <u>Other</u>.
 - (i) <u>Augmented Braking</u>. Augmented braking shall be used during vehicle decelerations on the driving cycle. Augmented braking shall be actuated only when the negative force applied by the vehicle at the roll surface is greater than 110 pounds. If the augmented braking is not linked to driver braking, the driver shall be signaled to not accelerate during this period.
 - (ii) <u>Cooling Fan</u>. The cooling fan capacity shall be 5400 ±300 SCFM, positioned within 12 inches of the intake to the vehicle's cooling system, and avoid unrepresentative cooling of the engine and exhaust control system.

(9) <u>All Wheel Drive Dynamometers</u>.

- (i) <u>Design</u>. The dynamometer shall meet the requirements for two wheel drive vehicles and be capable of testing traction control and all wheel drive vehicles in a safe manner without damaging the vehicle.
- (ii) <u>Wheelbase</u>. The all wheel drive dynamometer shall be capable of testing vehicles having a wheelbase between 84 and 125 inches, or as necessary to meet the wheelbase values in the I/M Look-up Table. The system shall provide a locking mechanism to secure the roll at the desired wheelbase.
- (iii) <u>Speed Synchronization</u>. Front and rear wheels shall maintain speed synchronization within ± 0.1 mph.

(b) Constant Volume Sampler

- (1) <u>General Design Requirements</u>.
 - (i) <u>Venturi Type</u>. A constant volume sampling (CVS) system of the critical flow venturi (CFV) or the sub-sonic venturi (SSV) type shall be used to collect vehicle exhaust samples. The CVS system and components shall generally conform to the specifications in §86.109-90.
 - (ii) <u>CVS Flow Size</u>. The CVS system shall be sized in a manner that prevents condensation in the dilute sample over the range of ambient conditions to be encountered during testing. A 700 SCFM system is assumed to satisfy this requirement. The range of ambient conditions may require the use of heated sample lines. Should heated sample lines be used, the lines and components shall be heated to a minimum of 120°F and a maximum of 250°F, which shall be monitored during the driving cycle.
 - (iii) <u>CVS Compressor</u>. The CVS compressor flow capacity shall be sufficient to maintain proper flow in the main CVS venturi with an adequate margin. For CFV CVSs the

margin shall be sufficient to maintain choke flow. The capacity of the blower relative to the CFV flow capacity shall not be so large as to create a limited surge margin.

- (iv) <u>Materials</u>. All materials in contact with exhaust gas shall be unaffected by and shall not affect the sample (i.e., the materials shall not react with the sample, and neither shall they taint the sample as a result of out gassing). Acceptable materials include stainless steel, Teflon[®], silicon rubber, and Tedlar[®].
- (v) <u>Alternative Designs</u>. Alternative CVS specifications, materials, or designs may be allowed upon a determination by the Administrator, that for the purpose of properly conducting an approved short test, the evidence supporting such deviations will not significantly affect the proper measurement of emissions.

(2) <u>Sample System</u>.

- (i) <u>Sample Probe</u>. The sample probe within the CVS shall be designed such that a continuous and adequate volume of sample is collected for analysis. The system shall have a method for determining if the sample collection system has deteriorated or malfunctioned such that an adequate sample is not being collected, or that the response time has deteriorated such that the time correlation for each emission constituent is no longer valid.
- (ii) <u>CVS Mixing Tee</u>.
 - (A) Design and Effect. The mixing tee for diluting the vehicle exhaust with ambient air shall be at the vehicle tailpipe exit as in \$86.109-90(a)(2)(iv). The dilution mixing tee shall be capable of collecting exhaust from all light-duty vehicle and light-duty truck exhaust systems. The design used shall not cause static pressure in the tailpipe to change such that the emission levels are significantly affected. A change of ± 1.0 inch of water or less, as measured at the tailpipe, shall be acceptable.
 - (B) Locating Device. The mixing tee shall have a device for positively locating the tee relative to the tailpipe with respect to distance from the tailpipe, and with respect to positioning the exhaust stream from the tailpipe(s) in the center of the mixing tee flow area. The locating device, or the size of the entrance to the tee shall be such that if a vehicle moves laterally from one extreme position on the dynamometer to the other extreme, that mixing tee will collect all of the exhaust sample.
- (iii) <u>Dual Exhaust</u>. For dual exhaust systems, the design used shall insure that each leg of the sample collection system maintains equal flow. Equal flow will be assumed if the design of the "Tee" intersection for the dual CVS hoses is a "Y" that minimizes the flow loss from each leg of the "Y," if each leg of the dual exhaust collection system is approximately equal in length (± 1 foot), and if the dilution area at the end of each leg is approximately equal. In addition, the CVS flow capacity shall be such that the entrance flow velocity for each leg of the dual exhaust system is sufficient to entrain all of the vehicle's exhaust from each tailpipe.
- (iv) <u>Background Sample</u>. The mixing tee shall be used to collect the background sample. The position of the mixing tee for taking the background sample shall be within 12 lateral and 12 longitudinal feet of the position during the transient driving cycle, and approximately 4 vertical feet from the floor.

(v) <u>Integrated Sample</u>. A continuous dilute sample shall be provided for integration by the analytical instruments in a manner similar to the method for collecting bag samples as described in §86.109-90.

(c) Analytical Instruments

- (1) <u>General Requirements</u>.
 - (i) <u>Instrument Specifications</u>. The emission analysis system shall automatically sample, integrate, and record the specified emission values for HC, CO, CO2, and NOx. Performance of the analytical instruments with respect to accuracy and precision, drift, interferences, noise, etc. shall be similar to instruments used for testing under §86 Subparts B, D, and N. Analytical instruments shall perform in this manner in the full range of operating conditions in the lane environment.
 - (ii) <u>Alternative Designs</u>. Alternative analytic equipment specifications, materials, designs, or detection methods may be allowed upon a determination by the Administrator, that for the purpose of properly conducting an approved short test, the evidence supporting such deviations will not significantly affect the proper measurement of emissions.

(2) Detection Methods and Instrument Ranges

- (i) <u>Total Hydrocarbon Analysis</u>. Total hydrocarbon analysis shall be determined by a flame ionization detector. If a 700 SCFM CVS is used, the analyzer calibration curve shall cover at least the range of 0 ppmC to 2,000 ppmC. Use of a different CVS flow capacity shall require an adjustment to these ranges. Appropriate documentation supporting any adjustment in ranges shall be available. The calibration curve must comply with the quality control specifications in §85.2234(d) for calibration curve generation.
- (ii) <u>Carbon Monoxide Analysis</u>. CO analysis shall be determined using a non-dispersive infrared analyzer. If a 700 SCFM CVS is used, CO analysis shall cover at least the range of 0 ppm to 10,000 ppm (1%). In order to meet the calibration curve requirements, two CO analyzers may be required one from 0 to 1000 or 2000 ppm, and one from 0 to 1% CO. Use of a different CVS flow capacity shall require an adjustment to these ranges. Appropriate documentation supporting any adjustment in ranges shall be available. The calibration curve requirements and the quality control specifications in §85.2234(d) apply to both analyzers.
- (iii) Carbon Dioxide Analysis. CO_2 analysis shall be determined using an NDIR analyzer. If a 700 SCFM CVS is used, CO_2 analysis shall cover at least the range of 0 ppm to 40,000 ppm (4%). Use of a different CVS flow capacity shall require an adjustment to these ranges. Appropriate documentation supporting any adjustment in ranges shall be available. The calibration curve must comply with the quality control specifications in §85.2234(d) for calibration curve generation.
- (iv) <u>Oxides of Nitrogen Analysis</u>. NOx analysis shall be determined using chemiluminescence. The NOx measurement shall be the sum of nitrogen oxide and nitrogen dioxide. Alternatively, NO_x measurements may be made by re-calibrating the chemiluminescence analyzer in NO only mode, then running the analyzer in NO only mode and multiplying the result by 1.03. This will eliminate the need for the converter and flow balance checks in §85.2234(d)(5) and §85.2234(d)(6).

If a 700 SCFM CVS is used, the NOx analysis shall cover at least the range of 0 ppm to 500 ppm. Use of a different CVS flow capacity shall require an adjustment to these

ranges. Appropriate documentation supporting any adjustment in ranges shall be available. The calibration curve must comply with the quality control specifications in §85.2234(d) for calibration curve generation.

- (3) <u>System Response Requirements</u>. Historically, continuously integrated emission analyzers have been required to have a response time of 1.5 seconds or less to 90% of a step change, where a step change was 60% of full scale or better. System response times between a step change at the probe and reading 90% of the change shall be less than 10 seconds.
- (4) <u>Integration Requirements</u>.
 - (i) <u>Sampling Frequency</u>. The analyzer voltage responses, CVS pressure(s), CVS temperature(s), dynamometer speed, and dynamometer power shall be sampled at a frequency of no less than 5 Hertz, and the voltage levels shall be averaged over 1 second intervals.
 - (ii) <u>Time Alignment</u>. The system shall properly time correlate each analyzer signal and the CVS signals to the driving trace.
 - (iii) Engineering Units. The one-second average analyzer voltage levels shall be converted to concentrations by the analyzer calibration curves. Corrected concentrations for each gas shall be derived by subtracting the pre-test background concentrations from the measured concentrations, according to the method in §85.2205(b). The corrected concentrations shall be converted to grams, for each second, using the equations specified in §85.2205(b) to combine the concentrations with the CVS flow over the same interval. The grams of emissions per test phase shall be determined using the equations in §85.2205(b).
 - (iv) <u>Multiple Analyzers</u>. When multiple analyzers are used for any constituent, the integration system shall simultaneously integrate both analyzers. The integrated values for the lowest analyzer in range shall be used for each second.
 - (v) <u>Background Samples</u>. For all constituents, the background concentration levels from the lowest range shall be used, including the case where multiple analyzers may have been used.
- (5) <u>Analytical System Design</u>.
 - (i) <u>Materials</u>. All materials in contact with exhaust gas prior to and throughout the measurement portion of the system shall be unaffected by and shall not affect the sample (i.e., the materials shall not react with the sample, and neither shall they taint the sample as a result of out gassing). Acceptable materials include stainless steel, Teflon, silicon rubber, and Tedlar[®].
 - (ii) <u>System Filters</u>. The sample system shall have an easily replaceable filter element to prevent particulate matter from reducing the reliability of the analytical system. The filter element shall provide for reliable sealing after filter element changes. If the sample line is heated, the filter system shall also be heated.
 - (iii) <u>Availability of Intermediate Calculation Variables</u>. Upon request prior to a test, all intermediate calculation variables shall be available to be downloaded to electronic files or hard copy. These variables shall include those that calculate the vehicle emission test results, perform emission analyzer and dynamometer function checks, and perform quality assurance and quality control measurements.

§85.2227 Evaporative System Equipment Specifications

(a) General Requirements

- Equipment Design. Automated and computerized test systems shall be used for the evaporative system tests wherever they are appropriate. Pass/fail decisions shall be made automatically. The systems shall be tamper resistant and designed to avoid damage to the vehicle during installation, testing, and removal.
- (2) <u>Alternative Systems</u>. Alternative purge, pressure, or gas cap test equipment specifications or designs may be proposed by a State if they are supported by data and approved in advance by the Administrator.

(b) Evaporative System Pressure Test Equipment

- (1) <u>General Requirements</u>.
 - <u>Alternative Designs</u>. Flow measurement or flow comparator leak detection methods are acceptable if supported by data and approved in advance by the Administrator. Standards for flow based methods have not been established.
 - (ii) <u>Pressurizing Gas</u>. Nitrogen, or an equivalent non-toxic, non-greenhouse, inert gas, shall be used for pressurizing the evaporative system. Air should only be used if the pressurized vapor space is outside the combustible limits for the vehicle fuel type.
 - (iii) <u>Automatic Operation</u>. The process for filling the vapor space, monitoring compliance, recording data, and making a pass/fail decision shall be automatic. After the determination that the evaporative system has been filled to the specified pressure level, and upon initiation of the test, the pressure level in the evaporative system shall be recorded at a frequency of no less than 1 Hertz until the conclusion of the test.
 - (iv) <u>Test Abort</u>. The system shall be equipped with an abort system that positively shuts off and relieves pressure. The abort system shall be capable of being activated quickly and conveniently by the inspector should the need arise.
 - (v) <u>Grounding</u>. A fillpipe pressure test must be designed to prevent electrostatic discharge that would pose a flammability risk during the test.
- (2) <u>Adapters and Clamps</u>.
 - (i) <u>Fuel Inlet Adapters</u>. Adapters attached to the fuel fillpipe inlet shall be used to supply pressurized gas into the fuel tank. Adapters shall be available for at least 95 percent of the fuel inlets that are used on U.S. light duty vehicles and light duty trucks for the model years covered by the program.
 - (ii) <u>Hose Clamp</u>. The hose clamp used for the fuel inlet pressure test shall be designed to apply only enough pressure to close the flexible vent line between the fuel tank and canister without damaging it. The nose of the clamp shall be smooth-surfaced or otherwise designed to avoid damage to the vent line.
- (3) <u>Pressure Gauge</u>. The device for measuring pressure shall have a minimum range of 0 to 28 inches of water and an accuracy of ± 0.3 inches of water, or 2% of point, whichever is greater.

(c) Gas Cap Test Equipment

(1) <u>General Requirements</u>.

- (i) <u>Alternative Designs</u>. Leak testers failing gas caps with a test standard below 60 cc/min at 30 in. WC are permissible provided they do not falsely fail gas caps designed to meet vehicle manufacturer OEM specifications, are repeatable and accurate in a centralized I/M environment, and demonstrate quantifiable reductions in real world mass emissions. OEM leak rates for individual manufacturers are proprietary. Information submitted to EPA shows some vehicle manufacturers had maximum leak rates up to 20 cc/min at 30 inches of WC.
- (ii) <u>Gas Cap Adapters</u>. The gas cap tester shall accommodate at least 95 percent of the gas caps that are used on U.S. light duty vehicles and trucks for the model years covered by the gas cap test program.
- (iii) <u>Pressurizing Gas</u>. Air, Nitrogen, or an equivalent non-toxic, non-greenhouse, inert gas, shall be used for pressurizing the gas cap tester.
- (iv) <u>Automatic Operation</u>. The process for making a pass/fail decision shall be automated. The gas cap tester shall provide for automated pass/fail determination and automated transfer of the pass/fail result to a host computer, i.e. a real-time data link.
- (v) <u>Over-Pressurization</u>. The tester shall control the supply pressure of the gas used for pressure decay, direct flow measurement, or flow comparison methods and prevent over-pressurization.
- (2) <u>Gas Cap Tester</u>. Gas cap testers employing internal reference orifices, or pressure measurement devices, shall be traceable to NIST flow or pressure measurement standards.
 - (i) <u>Range</u>. The tester shall identify passing gas caps with a leak rate equal to or less than 60 cc/min of air at 30 inches of WC, and failing caps with leak rates more than 60 cc/min at 30 inches of WC at reference conditions of 70F and 1 atm.
 - (ii) <u>Filter</u>. A serviceable air filter shall be incorporated upstream of flow orifices.
 - (iii) <u>Power Supply</u>. Battery powered testers shall be equipped with an automatic shutoff and a low-battery indicator.
 - (iv) <u>Accuracy</u>. Pressure decay, direct flow measurement, or flow comparison methods shall be accurate to ± 3 cc/min at the 60 cc/min flow standard.
 - (v) <u>Reference Caps and Orifices</u>. NIST traceable reference passing fuel caps or orifices of nominal 52-56 cc/min, and NIST traceable reference failing fuel caps or orifices of nominal 64-68 cc/min shall be supplied with the tester for daily verification tests.
 - (vi) <u>Head Space</u>. Pressure decay methods shall employ a head space sized to produce correct results at the 60 cc/min at 30 in. WC standard.
§85.2234 IM240 Test Quality Control Requirements

(a) General Requirements

- (1) <u>Manufacturers' Recommendations</u>. Manufacturers' recommendations for equipment installation, calibration, and maintenance, shall be followed.
- (2) <u>Statistical Process Control</u>. SPC tracking methods shall be established for appropriate equipment checks and custom diagnostic or verification tests.
- (3) <u>Modifications to Quality Control Requirements</u>. Changes to the type or frequency of the quality checks are permitted provided they are based on SPC analysis, or data from experimental studies.

(b) Dynamometer

- (1) Dynamometer Manufacturer Recommendations
 - (i) <u>Minimum Requirements</u>. The dynamometer manufacturer's requirements for periodic diagnostic checks, calibration, scheduled maintenance, and recommended quality control monitoring shall be followed.
 - (ii) <u>Warm-up Requirements</u>. The dynamometer manufacturer's procedure for insuring proper warm-up over a 35 to 110°F temperature range shall be followed.

(2) <u>Coast Down Testing</u>

- (i) <u>Frequency</u>. Dynamometers with electric and mechanical inertia simulation shall receive a daily unloaded (vehicle off the dynamometer) coast down check over the range of 60 to 10 mph. This daily check shall be run at alternating combinations of inertia and road load settings. Dynamometers using only mechanical flywheels for inertia simulation shall also receive additional weekly coast down checks to properly characterize the friction at other combinations of flywheel weights. The number of these coast downs shall be established based on the dynamometer design and quality control monitoring.
- (ii) Load Settings. Inertia and power absorber settings shall be representative of vehicle test conditions, and shall result in nominal coast down times of 15-20 seconds when time is measured between 55 and 45 mph, and 22-33 seconds when time is measured between 22 and 18 mph. Inertia settings for clutchable flywheel dynamometers are discretionary but should attempt to be above and below the base inertia of the dynamometer and represent high and low inertia weight vehicles.
- (iii) <u>Quality Control Limits</u>. Actual control limits for the coast down tests shall be established by statistical process control practices. The 55 to 45 mph and 22 to 18 mph coastdown times shall be within ± 1 second, and ± 6 seconds, respectively, of the theoretical coast down times. These ± 1 and ± 6 second limits are based on the 15-20 and 22-33 second coastdown times in the preceding paragraph. Theoretical coastdown time is based on the following equation:

$$t = \frac{\left(\frac{0.5 * ETW}{32.2} * (V_{I}^{2} - V_{F}^{2})\right)}{550 * HP}$$

Where: t = The coastdown time in seconds

ETW = The Equivalent Test Weight in pounds V_I = The initial roll velocity in feet/second V_F = The final roll velocity in feet/second IHP = The dynamometer indicated horsepower

An alternative to the ± 1 or ± 6 second limits is to perform an unloaded coastdown from 60 to 10 mph and reduce the speed/time data to produce a polynomial relationship between horsepower (or force) versus time. The measured horsepower curve shall be within ± 0.25 horsepower or $\pm 3\%$ of point, whichever is greatest.

Dynamometers which exceed specific SPC limits or the coast down limits presented above, shall be removed from service until corrective action is taken to assure the dynamometer is performing satisfactorily.

- (3) Parasitic Loss Checks
 - (i) <u>Frequency</u>. Checks of the parasitic loss curve shall be conducted at a frequency recommended by the dynamometer manufacturer, as required by inspection of quality control data, or as necessary following service to the dynamometer.
 - Quality Control Limits. Parasitic loss measurements shall be measured between 10 and 60 mph. Identification of outlier data shall be established by examination of quality control data.

Dynamometers which exceed dynamometer specific SPC limits for parasitic loss checks shall be removed from service until corrective action is taken to ensure the dynamometer is performing satisfactorily.

(4) <u>Roll Speed</u>.

- (i) <u>Frequency</u>. Weekly checks of the roll speed measurement system shall be made, or at intervals recommended by the dynamometer manufacturer, or as required by inspection of quality control data, or as necessary following service to the dynamometer.
- (ii) <u>Quality Control Limits</u>. If roll speed checks are conducted, the measured roll speed shall agree to within ±0.1 mph of the calibration standard. Dynamometers which exceed the 0.1 mph limit shall be removed from service until corrective action is taken to ensure the dynamometer is performing satisfactorily.

(5) <u>Acceptance Criteria</u>

- (i) <u>General</u>. Prior to dynamometer acceptance, the dynamometer shall demonstrate compliance with the design criteria for the load cell accuracy, power absorber curve accuracy, roll geometry, dynamometer simulation error, electric inertia response time, and parasitic loss measurement. These criteria are specified in §85.2226(a).
- (ii) <u>Base Inertia Verification</u>. The base inertia of dynamometers shall be verified before dynamometer acceptance. The base inertia weight plus individual prime weights shall be verified for dynamometers which simulate inertia with mechanical flywheels. The

specified base inertia shall agree with acceptance testing measurements within ± 10 pounds.

(iii) <u>Independent Speed and Distance Verification</u>. An independent method of verifying dynamometer roll speed and distance measurement accuracy shall be performed before dynamometer acceptance to ensure compliance with the specifications in §85.2226(a)(5)(v).

(c) Constant Volume Sampler

- (1) <u>Flow Calibration</u>. The flow of the CVS shall be calibrated at six flow rates upon initial installation, 6 months following installation, and every 12 months thereafter. SPC tracer gas injection data may be used to verify CVS flow in lieu of the annual calibration requirement. This data shall be made available to EPA upon request. The flow rates shall include the nominal rated flow-rate and a rate below the rated flow-rate for both critical flow venturis and subsonic venturis, and a flow-rate above the rated flow for sub-sonic venturis. The flow calibration points shall cover the range of variation in flow that typically occurs when testing. A complete calibration shall be performed following repairs to the CVS that could affect flow.
- (2) <u>System Check</u>. CVS flow calibration at the nominal CVS design flow shall be checked once per day using a procedure equivalent to that in \$86.119(c). Deviations greater than $\pm 4\%$ shall result in automatic lockout of official testing until corrected. At the State's discretion, the frequency of this may be reduced to weekly.
- (3) <u>Cleaning Flow Passages</u>. The sample probe shall be checked at least once per month, and cleaned if necessary in order to maintain proper sample flow. CVS venturi passages shall be checked once per year and cleaned if necessary.
- (4) <u>Probe Flow</u>. The indicator identifying the presence of proper probe flow for the system design (e.g., proportional flow for CFV systems, minimum flow for time correlation of different analyzers) shall be checked on a daily basis. Lack of proper flow shall require corrective action.
- (5) <u>Leak Check</u>. The vacuum portion of the sample system shall be checked for leaks on a daily basis and each time the system is serviced.
- (6) <u>System Response Time Check</u>. The response time of each analyzer shall be checked upon initial installation and after each repair or modification to the flow system that would reasonably be expected to affect the response time, and at least once per week. The check shall include the complete sample system from the sample probe to the analyzer. Statistical process control shall be used to monitor compliance and establish quality control limits. At a minimum, response time measurements that deviate significantly from the average response time for all CVS systems designed to the same specification in the program shall require corrective action before testing may resume.

(7) <u>Mixing Tee Acceptance Test</u>.

- (i) <u>Static Pressure Requirement</u>. The design of the mixing tee shall be evaluated by running the transient driving cycle on at least two vehicles, representing the high and low ends of engine displacement and inertia. Changes in the static tailpipe pressure with and without CVS, measured on a second-by-second basis within 3 inches of the end of the tailpipe, shall not exceed ±1.0 inch of water.
- (ii) <u>Single Exhaust System</u>. The ability of the mixing tee design to capture all of the exhaust as a vehicle moves laterally from one extreme position on the dynamometer to the other extreme shall be evaluated with back-to-back testing of three vehicles,

representing the high and low ends of engine displacement and inertia. The back-toback testing shall be done with the mixing tee at the tailpipe and with an airtight connection to the tailpipe (i.e., the mixing tee will be effectively moved downstream, as in typical FTP testing). The difference in carbon-balance fuel economy between the mixing tee located at the vehicle and the positive connection shall be no greater than 5%.

(iii) <u>Dual Exhaust System</u>. The design of the dual exhaust system shall be evaluated with back-to-back testing of three vehicles, representing the high and low ends of engine displacement and inertia, with an airtight connection to the tailpipe (i.e., the mixing tee will be effectively moved downstream, as in typical FTP testing, for these qualification tests). The difference in carbon-balance fuel economy between the two methods shall be no greater than 5%.

(d) Analysis System

- (1) <u>Calibration Curve Generation</u>.
 - (i) <u>Initial Installation Calibration</u>. Upon initial installation, calibration curves shall be generated for each analyzer. If an analyzer has more than one measurement transducer, each transducer shall be considered as a separate analyzer in the analysis system for the purposes of curve generation and analysis system checks.
 - (ii) <u>Complete Range Calibration</u>. The calibration curve shall consider the entire range of the analyzer as one curve.
 - (iii) <u>Calibration Point Spacing</u>. When both a low range analyzer and a high range analyzer are used for a single gas (e.g., CO), the high range analyzer shall use at least 5 calibration points plus zero in the lower portion of the high range scale corresponding to approximately 100% of the full-scale value of the low range analyzer. For all analyzers, at least 5 calibration points shall be used to define the calibration curve above the 5 lower calibration points. The calibration zero gas shall be used to set the analyzer to zero.

Alternatively, gas dividers may be used to generate a 10-point calibration curve employing equally spaced points.

- (iv) <u>Calibration Curve Fits</u>. The calibration curves generated shall be a polynomial of the best fit and no greater than 4th order, and shall fit the data within $\pm 2.0\%$ at each calibration point as specified in §86.120-90, §86.122-78, §86.123-78, and §86.124-78.
- (v) <u>Mid-scale Verification</u>. Each curve shall be verified for each analyzer with a confirming calibration standard between 30-60% of full scale that is not used for curve generation. Each confirming standard shall be measured by the curve within 2.5%.
- (2) <u>Spanning Frequency</u>. The zero and up-scale span points shall be checked at 3 hour intervals following the daily mid-scale curve check specified in \$85.2234(d)(4) and adjusted if necessary. If the up-scale span point drifts by more than 2.0% from the previous check official testing shall be prevented and corrective action shall be taken to bring the system into compliance. If the zero point drifts by more than 2 ppmC HC, 1 ppm NO_X, 10 ppm CO, or 40 ppm CO₂, official testing shall be prevented and corrective action shall be taken to bring the system into compliance, or the unit may be zeroed prior to each test.
- (3) <u>Limit Check</u>. The tolerance on the initial adjustment of a change in the up-scale span point shall be $\pm 2\%$ of point on the appropriate analyzer range. A software algorithm to perform the zero and span adjustment and subsequent calibration curve adjustment shall be used.

Cumulative software up-scale zero and span adjustments greater than $\pm 10\%$ from the latest calibration curve shall cause official testing to be prevented and corrective action shall be taken to bring the system into compliance. Zero and span potentiometers on the analyzer may be used between calibrations to minimize software corrections; however, a zero and span check shall be performed after any adjustment of a potentiometer.

- (4) <u>Daily Calibration Checks</u>. The curve for each analyzer shall be checked and adjusted to correctly read zero using a working zero gas, and an up-scale span gas within the tolerance in §85.2234(d)(3), and then by reading a mid-scale span gas within 2.5% of point, on each operating day prior to vehicle testing. If the analyzer does not read the mid-scale span point within 2.5% of point, the analyzer shall automatically be prevented from official testing. The up-scale span gas concentration for each analyzer may be up to 90% of full scale, and the mid-point concentration shall correspond to approximately 15% of full scale.
- (5) <u>Monthly NO_x Converter Checks</u>. The converter efficiency of the NO_2 to NO converter shall be checked on a monthly basis. The check shall be equivalent to §86.123-78 (for reference see TSD Form 305-01) except that the concentration of the NO gas shall be in the range of 75-400 ppm. Alternative methods may be used if approved by the Administrator.

This check is not required if the measurements of NO only are being performed per 85.2226(c)(2)(iv) with the NOx analyzer run in NO only mode.

(6) <u>Monthly NO/NO_X Flow Balance</u>. The flow balance between the NO and NO_X test modes shall be checked monthly. The check may be combined with the NO_X converter check as illustrated in EPA NVFEL test laboratory Form 305-01.

This check is not required if the measurements of NO only are being performed per 85.2226(c)(2)(iv) with the NOx analyzer run in NO only mode.

- (7) <u>Monthly Calibration Checks</u>. The basic calibration curve shall be verified monthly by the same procedure used to generate the curve in §85.2234(d)(1), and to the same tolerances.
- (8) <u>FID Check</u>.
 - (i) <u>FID Optimization</u>. Upon initial operation, and after maintenance to the detector, each FID shall be checked, and adjusted if necessary, for proper peaking and characterization using the procedures described in SAE Paper No. 770141 or by analyzer manufacturer recommended procedures.
 - (ii) <u>Methane Response</u>. The response of each FID to a methane concentration of approximately 50 ppm CH₄ shall be checked once per month. If the response is outside of the range of 1.00 to 1.30, corrective action shall be taken to bring the FID response within this range. The response shall be computed by the equation in \$85.2234(d)(8)(iii). The frequency of this check may be reduced by providing 1 year of data for each analyzer that demonstrates less frequent checks are acceptable. If less frequent checks are used, the response check data shall be made available to EPA upon request.
 - (iii) <u>Methane Response Definition</u>. Ratio of Methane Response = FID response to CH₄ gas in ppmC /ppm CH₄ in the cylinder.
- (9) <u>Mid-Span or Cross-Checks</u>. On a quarterly basis, and whenever gas bottles are changed, each analyzer in a given facility shall analyze a sample of a test gas. The test gas used for these cross checks shall be a 1% NIST traceable mid-span bottle and the same bottle shall be used for all

analyzers at a given facility. The analyzer shall read this mid-span gas within 2.5% of the labeled value or the analyzer shall be taken out of service.

Alternatively, all gas bottles entering a facility shall be verified using a master bench and NIST traceable SRM, CRM, NTRM, or RGM gases. Quarterly checks would then be performed on each analyzer using three points at 25%, 50%, and 75% of full scale.

- (10) <u>Interference Test</u>. The CO analyzer shall be checked for water vapor interference prior to initial service. The interference limits in this paragraph shall apply to analyzers used with a CVS of 700 SCFM or greater. For analyzers used with lower flow rate CVS units, the allowable interference response shall be proportionately adjusted downward.
 - (i) <u>CO Analyzer</u>. A CO instrument will be considered to be essentially free of CO₂ and water vapor interference if its response to a mixture of 3% CO₂ in N₂ which has been bubbled through water at 20°C produces an equivalent CO response, as measured on the most sensitive CO range, which is less than 1% of full scale.

(e) Gases

- (1) <u>General Requirements</u>. Gas blends may contain up to three of any of the following components: HC, CO, CO₂, and NO. The HC component shall be propane. The diluent for blends containing HC shall be air. The diluent for blends containing NO shall be N₂. CO and CO₂ may be used with either air or N₂ as the diluent. Blends containing four interest components may be used only if approved by the Administrator. Blends containing NO₂ shall also require approval by the Administrator prior to use, except if used to perform the NO_x converter check specified in §85.2234(d)(5). Any interference effects between components in a gas blend shall be addressed in the quality control and quality assurance process. When a gas audit of the analytical system is performed, the auditor shall indicate whether CO₂ is present in the audit gas mixture prior to performing the audit.
- (2) <u>Calibration Gases</u>. Gases used to generate and check calibration curves shall be traceable to a NIST SRM, CRM, NTRM, or RGM and have a stated uncertainty to within 1% of the standard by gas comparison methods. Calibration zero gas shall be used when using a gas divider to generate intermediary calibration gases.
- (3) Span Gases. Gases used for up-scale span adjustment, cross-checks, and for mid-scale span checks shall be traceable to NIST SRM, CRM, NTRM, or RGM and have a stated uncertainty to within 2% of the standard by gas comparison methods. Span gas concentrations shall be verified immediately after a monthly calibration curve check and before being put into service. If the reading on the span gases exceeds 2.5% of the label value, the system or gases shall be taken out of service until corrective action is taken. When a gas divider is used to generate span gases, the diluent gas shall not have impurities any greater than the working zero gas.
- (4) <u>Calibration Zero Gas</u>. The impurities in the calibration zero gas shall not exceed 0.1 ppmC, 0.5 ppm CO, 1 ppm CO₂, and 0.1 ppm NO. Calibration zero grade air shall be used for the FID zero calibration gas. Calibration zero grade nitrogen or calibration zero grade air shall be used for CO, CO₂, and NO_x zero calibration gases.
- (5) <u>Working Zero Gas</u>. The impurities in working zero grade gases shall not exceed 1 ppmC, 2 ppm CO, 400 ppm CO₂, and 0.3 ppm NO_x. Working zero grade air or calibration zero grade air shall be used for the FID zero span gas. Working or calibration zero grade nitrogen or air shall be used for CO, CO₂, and NO_x zero span gases.

- (6) <u>FID Fuel</u>. The fuel for the FID shall consist of a mixture of 40% ($\pm 2\%$) hydrogen, and the balance helium. The FID oxidizer shall be zero grade air, which can consist of artificial air containing 18 to 21 mole percent of oxygen.
- (7) <u>Gas Naming Protocol</u>. Gases used for calibration or auditing shall be named according to a written established practice that has been approved by the Administrator. An accepted gas naming procedure for I/M test purposes is the IM240 Gas Certification Protocol dated 10/27/94, or its latest revision. Copies of the 10/27/94 document are available upon request from EPA.

(f) Overall System Performance

- (1) <u>Emission Levels</u>. For each test lane, the average, median, 10th percentile and 90th percentile of the composite emissions (HC, CO, CO₂, and NO_X) measured shall be monitored on a monthly basis. Differences in the monthly average of greater than $\pm 10\%$ by any one lane from the facility-average or combined facility-average, or by any one facility from the combined facility-average shall require an investigation to determine whether the single lane or facility has a systematic equipment or operating error or difference. Where it can be determined that the averages from one facility (or facilities) are offset from the average of the other facilities based on the mix of vehicles tested, the $\pm 10\%$ limit shall be compared to the expected offset. If systematic equipment or operating errors or differences causing the offset are found, such errors shall be corrected. The sample period may be adjusted to assure that a reasonably random sample of vehicles was tested in each lane.
- (2) <u>Pass/Fail Status</u>. The average number of passing vehicles and the average number of failing vehicles shall be monitored monthly for each test lane. Differences in the monthly average of greater than $\pm 15\%$ by any one lane from the facility-average or combined facility-average, or by any one facility from the combined facility-average shall require an investigation to determine whether the single lane or facility has a systematic equipment or operating error or difference. Where it can be determined that the averages from one facility (or facilities) are offset from the average of the other facilities based on the mix of vehicles tested, the $\pm 15\%$ limit shall be compared to the expected offset. If systematic equipment or operating errors or differences causing the offset are found, such errors shall be corrected. The sample period may be adjusted to assure that a reasonably random sample of vehicles was tested in each lane.

(g) Control Charts

- (1) <u>General Requirements</u>. Control charts and Statistical Process Control theory shall be used to determine, forecast, and maintain performance of each test lane, each facility, and all facilities in a given network. The control charts shall cover the performance of key parameters in the test system. When key parameters approach control chart limits, close monitoring of such systems shall be initiated and corrective actions shall be taken when needed to prevent such systems from exceeding control chart limits. If any key parameter exceeds the control chart limits, corrective action shall be taken to bring the system into compliance. The control chart limits specified are those values listed for the test procedures, the equipment specifications, and the quality control specifications that cause a test to be voided or require equipment to be removed from service. These values are "fit for use" limits, unlike a strict interpretation of SPC control chart theory which may use tighter limits to define the process. The test facility is encouraged to apply SPC strict control chart theory to determine when equipment or processes could be improved. No action shall be required until the equipment or process exceeds the "fit for use limits" specified in this section.
- (2) <u>Control Charts for Individual Test Lanes</u>. In general, control charts for individual test lanes shall include parameters that will allow the cause for abnormal performance of a test lane to be pinpointed to individual systems or components. Test lane control charts shall include at a minimum:

- (i) Difference between theoretical and measured coast-down times
- (ii) Difference between theoretical and measured CVS flow
- (iii) Up-scale span change from last up-scale span (not required if software corrections are tracked)
- (iv) Mathematical or software correction to the calibration curve as a result of an up-scale span change (if used)
- (v) Difference between the analyzer response to the daily cross-check, and the test gas concentration
- (vi) The system response time
- (vii) FID CH₄ response ratio
- (viii) Difference between theoretical or measured values for other parameters measured during quality assurance procedures
- (3) <u>Control Charts for Individual Facilities</u>. Control charts for individual facilities shall consist of the test lane control charts for each test lane at the facility.
- (4) <u>Control Charts of Individual Inspectors</u>. Control charts for individual inspectors shall include parameters that will allow the cause for abnormal performance to be evaluated, such as technician IM240 driving quality.

§85.2235 Evaporative Test Quality Control Requirements

(a) General Requirements

- (1) <u>Manufacturers' Recommendations</u>. Manufacturers' recommendations for equipment installation, calibration, and maintenance shall be followed.
- (2) <u>Statistical Process Control</u>. SPC tracking methods shall be established for appropriate equipment checks and custom diagnostic or verification tests.
- (3) <u>Modifications to Quality Control Requirements</u>. Changes to the type or frequency of the quality checks are permitted provided they are based on SPC analysis, or data from experimental studies.

(b) Evaporative System Pressure Checks

- (1) <u>Daily Checks</u>. The pressure check system shall be pressurized to 28±1 inch of WC and monitored for a loss of pressure. Pressure testing shall be stopped and corrective action shall be taken to repair the system if a loss of pressure of more than 0.4 inches of WC is observed over a 15 second period.
- (2) <u>Bi-Weekly Check</u>. Pressure gauges or measurement devices shall be checked on a bi-weekly basis against a reference gauge or device equal to or better than the specified performance requirements. Deviations exceeding the specified accuracy shall require corrective action.

(c) Evaporative System Gas Cap Checks

- (1) <u>Gas Cap Tester</u>.
 - (i) <u>Daily Checks</u>. The tester shall be verified daily by testing and correctly identifying passing and failing reference gas caps or flow orifices as specified in §85.2227(d)(2)(v). Reference caps and orifices shall be stored in a dirt and dust free manner to prevent clogging and changes in flow rates. Reference caps and orifices shall be stored at the same temperature as the cap tester to provide accurate flow reference.
 - (ii) <u>Corrective Action</u>. Gas cap testing shall be stopped and corrective action taken to repair the tester if passing and failing reference gas caps or flow orifices cannot be correctly identified.
 - (iii) <u>Reference Caps or Orifices Flow Checks</u>. Independent flow bench verification of the reference gas caps and flow orifices shall be conducted before initial usage, and at six month intervals, or as recommended by the cap tester manufacturer or as suggested by analysis of quality control data. The bench flow verification results shall be traceable to NIST.
 - (iv) <u>Comparator Orifices Flow Checks</u>. Internal flow standard orifices for direct flow measurement methods, or flow comparator methods, shall be traceable to a NIST reference.
- (2) <u>Gas Cap Adapters</u>.
 - (i) <u>Leak Checks</u>. The gas cap adapters shall be checked for visual damage daily and leak checked weekly, or by following the recommendations of the gas cap adapters supplier.

§85.2239 Test Report

(a) General Test Report Information

- (1) <u>Vehicle Description</u>.
 - (i) License plate number
 - (ii) Vehicle identification number
 - (iii) Weight class
 - (iv) Odometer reading
- (2) <u>Date and Time</u>. Date and end time of the tailpipe emission measurement test.
- (3) <u>Identification Information</u>. Name or identification number of the individual performing the test and the location of the test station and lane.
- (4) <u>Warranty Provisions</u>. For failed vehicles, a statement indicating the availability of warranty coverage as provided in Section 207 of the Clean Air Act.
- (5) <u>Certification</u>. A statement certifying that the short tests were performed in accordance with applicable regulations.

(b) Tests and Results

- (1) <u>Test Types and Standards</u>. The test report shall indicate the types of tests performed on the vehicle and the test standards for each. Test standards shall be displayed to the appropriate number of significant digits as in §85.2205(a). For the IM240 the reported standards shall be the composite test standards.
- (2) <u>Test Scores</u>. The test report shall show the scores for each test performed. Test scores shall be displayed to the same number of significant digits as the standards.
- (3) <u>IM240 Scores</u>. The reported score for the IM240 shall be in units of grams per mile and shall be selected based upon the following:
 - (i) <u>Passing Scores Composite IM240</u>. If the emissions of any exhaust component on the composite IM240 are below the applicable standard in §85.2205(a), then the vehicle shall pass for that constituent and the composite score shall be reported.
 - (ii) <u>Passing Scores Phase 2</u>. If the emissions of any exhaust component on the composite IM240 exceed the applicable standard in §85.2205(a) but are below the Phase 2 standard, then the vehicle shall pass for that component and the Phase 2 score shall be reported.
 - (iii) <u>Failing Scores</u>. If the emissions of any exhaust component on the composite IM240 exceed the applicable standard in §85.2205(a)(2) through §85.2205(a)(4) and exceed the Two Ways to Pass Standard as described in §85.2205(a)(1), then the vehicle shall fail for that component and the composite score shall be reported.
 - (iv) <u>Emission Reporting</u>. If a passing decision is made for all three exhaust components on the IM240 before the end of the full driving cycle according to the criteria described in §85.2205(a)(4), the passing results and reported emissions levels shall be those obtained at the time the test is terminated. Emission levels for the IM240 shall be reported in grams per mile calculated using the full IM240 mileage (not actual

mileage). The emission standards reported shall be the composite standards (i.e., not the fast-pass standards).

- (4) <u>Pressure Test Scores</u>. The score(s) for the pressure test(s) shall be reported as a change in pressure expressed in inches of water.
- (5) <u>Test Results</u>. The test report shall indicate the pass/fail result for each test performed and the overall result. In the case of exhaust emission tests, the report shall indicate the pass/fail status for each component for which standards apply.
- (6) <u>Second-by-Second Measurements</u>. For vehicles failing the IM240, a graph showing the secondby-second emission levels (see following example), for each exhaust component in grams per mile equivalent. The plots of HC, CO, NOx, and CO2 are expressed in units of "gram per mile equivalent," or:

 $Y = (X)^{*}(239 \text{ seconds})/(1.959 \text{ miles})$

Where: Y = Grams per mile equivalent calculated on a second by second basis

X = Grams of HC, CO, NOx, or CO2 calculated during the one second interval

(c) Recommended IM240 Second-By-Second Emissions Report

Model Year	1988	Test Weight	3000	Emission	<u>Actual</u>	<u>Cut</u> point
Make	XXXX	TRLHP	14.7	HC (gpm)	2.45	0.80
Model	YYYY	Traction Control	No	CO (gpm)	23.1	15.0
Cylinders	4	ABS	No	NOx (gpm)	0.71	2.00
Transmission	Auto	Gas Cap Test	Yes	CO2 (gpm)	279	n/a
Vehicle Type	LDGV	Press Test	Yes			

Test Number 4719

The following figures provide illustrations of the recommended second-by-second emissions output.



.2271		I CI IIIS	
	(1)	ALVW:	Adjusted Loaded Vehicle Weight: (VCW + GVWR)/2
	(2)	CFV:	Critical Flow Venturi
	(3)	CH ₄ :	Methane
	(4)	CO_2 :	Carbon dioxide
	(5)	CO:	Carbon monoxide
	(6)	CRM:	Certified Reference Material
	(7)	CVS:	Constant Volume Sampler
	(8)	ETW:	Equivalent Test Weight
	(9)	FID:	Flame Ionization Detector
	(10)	gpm:	Grams per mile
	(11)	GVWR:	Gross Vehicle Weight Rating
	(12)	HC:	Hydrocarbons
	(13)	HDGT:	Heavy-Duty Gasoline-powered Truck greater than 8500 pounds GVWR
	(14)	hp:	Horsepower
	(15)	Hz:	Cycles per Second (Hertz)
	(16)	I/M:	Inspection and Maintenance
	(17)	IW:	Inertia Weight
	(18)	LDGV:	Light-Duty Gasoline-powered Vehicle
	(19)	LVW:	Loaded Vehicle Weight: VCW + 300 pounds
	(20)	mph:	Miles per hour
	(21)	NDIR:	Non-Dispersive Infrared
	(22)	NIST:	National Institute for Standards and Technology
	(23)	NO ₂ :	Nitrogen Dioxide
	(24)	NO:	Nitrogen Oxide
	(25)	NO _X :	Oxides of Nitrogen
	(26)	NVFEL:	National Vehicle and Fuel Emissions Laboratory
	(27)	Obmph:	Observed dynamometer speed in mph of the loading roller, if rolls are not coupled
	(28)	PLHP:	Parasitic horsepower loss at the observed dynamometer speed in mph
	(29)	ppm:	parts per million by volume
	(30)	ppmC:	parts per million, carbon
	(31)	psi:	Pounds per square inch
	(32)	RFP:	Request for Proposal
	(33)	RLHP	Road Load Horsepower
	(34)	rpm:	revolutions per minute
	(35)	SCFM:	Standard cubic feet per minute
	(36)	SPC:	Statistical Process Control
	(37)	SRM:	Standard Reference Material
	(38)	SSV:	Subsonic venturi
	(39)	TRLHP:	Track Road-Load Horsepower
	(40)	VCW:	Vehicle Curb Weight: Actual vehicle weight with standard equipment and 100% fuel fill
	(41)	WC:	Pressure in inches of water column

§85.2241

Terms

Appendix A

Guidance on the Use of Fast-Pass IM240 Standards

Guidance on the Use of Fast-Pass IM240 Standards

A fast-pass decision is made by measuring the vehicle's cumulative emissions of each pollutant in each second, and comparing them to cumulative emission fast-pass standards for each pollutant for the second of the test under consideration. In general, if the vehicle's cumulative emissions are below a given level for all pollutants the vehicle passes. Testing continues until decisions are made for each pollutant. Measurements of all constituents shall continue to be taken as long as the test continues, including those constituents for which a decision has already been made.

These fast-pass standards are derived from an Arizona IM240 data set which included 3,718 tests. Fast-pass standards for each second represent the tenth lowest cumulative emission levels in that second obtained for vehicles failing the IM240 using the two-ways-to-pass criteria. Hence, vehicles that fall below this level are showing lower cumulative emissions at that point in the test than the cleanest vehicles failing the full test and therefore pass. Fast-pass determinations begin at second 30 of the IM240 cycle.

Beginning at second 109, fast pass decisions for HC and CO are based upon analysis of cumulative emissions in phase 2, the portion of the test beginning at second 94, as well as emission levels accumulated from the beginning of the test (the "composite" test). Fast-pass standards are derived for phase 2 of the test as described above. Since the phase 2 standards for NO_x are the same as the composite, the phase 2 NO_x fast-pass standards are also the same as the composite.

Scores

 HC_t = cumulative composite HC at time = t seconds

 CO_t = cumulative composite CO at time = *t* seconds

 $NOx_t = cumulative composite NOx at time = t seconds$

 HC_{ht} = cumulative Phase 2 HC at time = t seconds

 CO_{bt} = cumulative Phase 2 CO at time = t seconds

 NOx_{ht} = cumulative Phase 2 NOx at time = t seconds

Cumulative composite scores represent the cumulative grams of emissions from t = 0 seconds Cumulative Phase 2 scores represent the cumulative grams of emissions from t = 109 seconds

Fast-Pass Standards

 $HC_{pt} = composite HC fast-pass standard at time = t seconds$ $CO_{pt} = composite CO fast-pass standard at time = t seconds$ $NOx_{pt} = composite NOx fast-pass standard for failing vehicles at time = t seconds$ $HC_{pbt} = Phase 2 HC fast-pass standard at time = t seconds$ $CO_{pbt} = Phase 2 CO fast-pass standard at time = t seconds$ $NOx_{pbt} = Phase 2 NOx fast-pass standard at time = t seconds$

Fast-Pass Conditions

For t > 30 seconds, the vehicle shall pass if:

 $HC_t < HC_{pt}$ and $CO_t < CO_{pt}$, $NOx_t < NOx_{pt}$;

additionally, for t > 109 seconds, the vehicle shall pass if:

 $HC_{bt} < HC_{pbt}$ and $CO_{bt} < CO_{pbt}$ and $NOx_{bt} < NOx_{pbt}$ or

 $HC_t < HC_{pt}$ and $CO_{bt} < CO_{pbt}$ and $NOx_{bt} < NOx_{pbt}$ or

 $HC_t < HC_{pt}$ and $CO_t < CO_{pt}$ and $NOx_{bt} < NOx_{pbt}$ or

 $HC_{bt} < HC_{pbt}$ and $CO_t < CO_{pt}$ and $NOx_{bt} < NOx_{pbt}$ or

 $HC_{bt} < HC_{pbt}$ and $CO_t < CO_{pt}$ and $NOx_t < NOx_{pt}$ or

 $HC_{bt} < HC_{pbt}$ and $CO_{bt} < CO_{pbt}$ and $NOx_t < NOx_{pt}$

IM240 FAST-PASS EMISSION STANDARDS

(grams)

	Hydrocarbons						Carbon Monoxide							Oxide	
Sec	Composite		Composite		Composite		Composite		Composite		Composite			Nitrog	gen
	0.80	2 0.50	1.25	2 0.75	2.00	2 1.25	15.0	2 12.0	20.0	2 16.0	30.0	2 24.0	2.0	2.5	3.0
30	0.124		0.247		0.407		0.693		1.502		3.804		2.0 0.167	0.262	0.419
		n/a		n/a		n/a		n/a		n/a		n/a			
31	0.126	n/a	0.253	n/a	0.415	n/a	0.773	n/a	1.546	n/a	3.985	n/a	•••••	0.275	
32	0.129	n/a	0.258	n/a	0.423	n/a	0.837	n/a	1.568	n/a	4.215	n/a	•••••	0.301	
33	0.135	n/a	0.263	n/a	0.436	n/a	0.851	n/a	1.582	n/a	4.440	n/a	•••••	0.317	
34	0.140	n/a	0.268	n/a	0.451	n/a	0.853	n/a	1.593	n/a	4.579	n/a		0.327	
35	0.146	n/a	0.277	n/a	0.464	n/a	0.857	n/a	1.602	n/a	4.688	n/a	•••••	0.330	
36	0.150	n/a	0.283	n/a	0.468	n/a	0.900	n/a	1.621	n/a	4.749	n/a	•••••	0.332	
37	0.153	n/a	0.293	n/a	0.475	n/a	0.960	n/a	1.631	n/a	4.783	n/a	•••••	0.334	
38	0.156	n/a	0.297	n/a	0.487	n/a	1.034	n/a	1.702	n/a	4.813	n/a	•••••	0.336	
39	0.160	n/a	0.298	n/a	0.506	n/a	1.070	n/a	1.784	n/a	4.876	n/a	•••••	0.337	
40	0.165	n/a	0.313	n/a	0.530	n/a	1.076	n/a	1.879	n/a	5.104	n/a	•••••	0.354	
41	0.169	n/a	0.320	n/a	0.549	n/a	1.083	n/a	2.162	n/a	5.217	n/a		0.366	
42	0.172	n/a	0.327	n/a	0.569	n/a	1.102	n/a	2.307	n/a	5.383	n/a	•••••	0.410	
43	0.173	n/a	0.342	n/a	0.588	n/a	1.111	n/a	2.343	n/a	5.571	n/a		0.414	
44	0.177	n/a	0.360	n/a	0.609	n/a	1.114	n/a	2.376	n/a	5.888	n/a	•••••	0.438	
45	0.197	n/a	0.376	n/a	0.621	n/a	1.157	n/a	2.406	n/a	6.199	n/a		0.477	
46	0.200	n/a	0.389	n/a	0.636	n/a	1.344	n/a	2.433	n/a	6.245	n/a		0.506	
47	0.208	n/a	0.408	n/a	0.649	n/a	1.482	n/a	2.458	n/a	6.318	n/a	0.373	0.518	0.716
48	0.221	n/a	0.423	n/a	0.666	n/a	1.530	n/a	2.483	n/a	6.418	n/a	0.383	0.522	0.735
49	0.232	n/a	0.434	n/a	0.679	n/a	1.542	n/a	2.774	n/a	6.540	n/a	0.385	0.526	0.765
50	0.235	n/a	0.444	n/a	0.696	n/a	1.553	n/a	2.844	n/a	6.690	n/a	0.400	0.554	0.802
51	0.238	n/a	0.454	n/a	0.712	n/a	1.571	n/a	2.900	n/a	6.875	n/a	0.410	0.574	0.836
52	0.240	n/a	0.465	n/a	0.727	n/a	1.595	n/a	2.936	n/a	7.029	n/a	0.434	0.587	0.868
53	0.242	n/a	0.472	n/a	0.745	n/a	1.633	n/a	3.133	n/a	7.129	n/a	0.464	0.601	0.890
54	0.246	n/a	0.478	n/a	0.760	n/a	1.685	n/a	3.304	n/a	7.359	n/a	0.472	0.615	0.918
55	0.249	n/a	0.485	n/a	0.776	n/a	1.689	n/a	3.407	n/a	7.722	n/a	0.480	0.629	0.936
56	0.252	n/a	0.493	n/a	0.797	n/a	1.693	n/a	3.456	n/a	8.017	n/a	0.491	0.643	0.947
57	0.261	n/a	0.500	n/a	0.814	n/a	1.700	n/a	3.480	n/a	8.249	n/a	0.500	0.667	0.958
58	0.271	n/a	0.505	n/a	0.826	n/a	1.723	n/a	3.518	n/a	8.425	n/a	0.506	0.678	0.970
59	0.276	n/a	0.514	n/a	0.837	n/a	1.852	n/a	3.560	n/a	8.563	n/a	0.509	0.683	0.982
60	0.278	n/a	0.537	n/a	0.849	n/a	1.872	n/a	3.593	n/a	8.686	n/a	0.512	0.686	0.994
61	0.280	n/a	0.540	n/a	0.862	n/a	1.872	n/a	3.628	n/a	8.804	n/a	0.516	0.693	1.019
62	0.282	n/a	0.543	n/a	0.872	n/a	1.872	n/a	3.641	n/a	8.916	n/a	0.519	0.699	1.042
63	0.283	n/a	0.546	n/a	0.887	n/a	1.900	n/a	3.655	n/a	9.025	n/a		0.703	
64	0.284	n/a	0.551	n/a	0.895	n/a	1.917	n/a	3.680	n/a	9.138	n/a	0.529	0.707	1.058
65	0.285	n/a	0.559	n/a	0.903	n/a	1.944	n/a	3.700	n/a	9.250	n/a	0.533	0.711	1.062
66	0.286	n/a	0.567	n/a	0.925	n/a	2.000	n/a	3.728	n/a	9.354	n/a	0.535	0.716	1.064
67	0.288	n/a	0.575	n/a	0.933	n/a	2.060	n/a	3.857	n/a	9.457	n/a		0.721	
68	0.291	n/a	0.588	n/a	0.945	n/a	2.064	n/a	3.894	n/a	9.575	n/a	•••••	0.726	
69	0.294	n/a	0.595	n/a	0.959	n/a	2.076	n/a	3.943	n/a	9.728	n/a		0.742	
70	0.294	n/a	0.601	n/a	0.959	n/a	2.070	n/a	3.983	n/a	9.938	n/a		0.759	
71	0.298	n/a	0.606	n/a	0.980	n/a	2.104	n/a	4.009	n/a	10.140	n/a	•••••	0.773	
72	0.200	n/a	0.610	n/a	0.988	n/a	2.117	n/a	4.023	n/a	10.140	n/a	•••••	0.784	
72	0.300	n/a	0.617	n/a	0.988	n/a	2.125	n/a	4.023	n/a	10.222	n/a	•••••	0.790	
73	0.302		0.631		1.022		2.130		4.025	••••••	••••••			0.790	
l′. *	0.304	n/a	0.031	n/a	1.044	n/a	2.130	n/a	4.033	n/a	10.278	n/a	0.004	0.774	1.131

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$.799 1.141	0.613	n/a	10.290	n/a	4.063	n/a	2.152	n/a	1.037	n/a	0.643	n/a	0.307	75
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	•••••	•••••	n/a		n/a			2.508			••••••	••••••		• • • • • • • • • • • • • • • • • • • •	99
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$.941 1.405	0.789	n/a	•••••	n/a	4.957	n/a	2.660	n/a	1.365	n/a	0.810	n/a	0.410	101
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$.970 1.466	0.822	n/a	•••••	n/a	5.104	n/a	2.749	n/a	1.378	n/a	0.823	n/a	0.411	102
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$.027 1.485	0.867	n/a	13.472	n/a	5.340	n/a	2.913	n/a	1.397	n/a	0.836	n/a	0.412	103
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$.093 1.546	0.905	n/a	14.405	n/a	5.496	n/a	3.162	n/a	1.420	n/a	0.853	n/a	0.413	104
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$.155 1.623	0.925	n/a	14.808	n/a	5.625	n/a	3.170	n/a	1.445	n/a	0.871	n/a	0.421	105
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$.234 1.699	0.955	n/a	14.965	n/a	5.815	n/a	3.197	n/a	1.470	n/a	0.887	n/a	0.428	106
109 0.459 0.015 0.947 0.040 1.517 0.151 3.587 0.168 7.419 0.246 15.530 1.113 0.995 1.320 110 0.462 0.017 0.957 0.047 1.528 0.159 3.595 0.173 7.643 0.257 15.687 1.213 0.996 1.332 111 0.464 0.021 0.965 0.052 1.542 0.172 3.640 0.237 7.759 0.286 16.018 1.344 1.010 1.346 112 0.466 0.024 0.971 0.056 1.559 0.186 3.740 0.266 7.824 0.379 16.527 1.399 1.028 1.358 113 0.468 0.024 0.977 0.061 1.578 0.199 3.868 0.280 7.889 0.425 16.810 1.520 1.034 1.378 114 0.471 0.025 0.983 0.064 1.594 0.207 3.877 0.291 7.9	.275 1.760	0.985	n/a	15.121	n/a	6.473	n/a	3.288	n/a	1.491	n/a	0.899	n/a	0.430	107
110 0.462 0.017 0.957 0.047 1.528 0.159 3.595 0.173 7.643 0.257 15.687 1.213 0.996 1.332 111 0.464 0.021 0.965 0.052 1.542 0.172 3.640 0.237 7.759 0.286 16.018 1.344 1.010 1.346 112 0.466 0.024 0.971 0.056 1.559 0.186 3.740 0.266 7.824 0.379 16.527 1.399 1.028 1.358 113 0.468 0.024 0.977 0.061 1.578 0.199 3.868 0.280 7.889 0.425 16.810 1.520 1.034 1.378 114 0.471 0.025 0.983 0.064 1.594 0.207 3.877 0.291 7.960 0.457 16.961 1.640 1.044 1.406 115 0.488 0.026 1.003 0.072 1.605 0.216 3.934 0.314 8.0	.305 1.788	0.993	n/a	15.372	n/a	7.037	n/a	3.419	n/a	1.506	n/a	0.931	n/a	0.455	108
111 0.464 0.021 0.965 0.052 1.542 0.172 3.640 0.237 7.759 0.286 16.018 1.344 1.010 1.346 112 0.466 0.024 0.971 0.056 1.559 0.186 3.740 0.266 7.824 0.379 16.527 1.399 1.028 1.358 113 0.468 0.024 0.977 0.061 1.578 0.199 3.868 0.280 7.889 0.425 16.810 1.520 1.034 1.378 114 0.471 0.025 0.983 0.064 1.594 0.207 3.877 0.291 7.960 0.457 16.961 1.640 1.044 1.406 115 0.488 0.026 1.003 0.072 1.605 0.216 3.934 0.314 8.024 0.477 17.120 1.684 1.059 1.426 116 0.513 0.029 1.030 0.081 1.615 0.229 4.015 0.331 8.0	.320 1.798	0.995	1.113	15.530	0.246	7.419	0.168	3.587	0.151	1.517	0.040	0.947	0.015	0.459	109
112 0.466 0.024 0.971 0.056 1.559 0.186 3.740 0.266 7.824 0.379 16.527 1.399 1.028 1.358 113 0.468 0.024 0.977 0.061 1.578 0.199 3.868 0.280 7.889 0.425 16.810 1.520 1.034 1.378 114 0.471 0.025 0.983 0.064 1.594 0.207 3.877 0.291 7.960 0.457 16.961 1.640 1.044 1.406 115 0.488 0.026 1.003 0.072 1.605 0.216 3.934 0.314 8.024 0.477 17.120 1.684 1.059 1.426 116 0.513 0.029 1.030 0.081 1.615 0.229 4.015 0.331 8.076 0.494 17.135 1.693 1.075 1.438 117 0.538 0.032 1.041 0.082 1.625 0.235 4.061 0.345 8.1	.332 1.842	0.996	1.213	15.687	0.257	7.643	0.173	3.595	0.159	1.528	0.047	0.957	0.017	0.462	110
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113 0.468 0.024 0.977 0.061 1.578 0.199 3.868 0.280 7.889 0.425 16.810 1.520 1.034 1.378 114 0.471 0.025 0.983 0.064 1.594 0.207 3.877 0.291 7.960 0.457 16.961 1.640 1.044 1.406 115 0.488 0.026 1.003 0.072 1.605 0.216 3.934 0.314 8.024 0.477 17.120 1.684 1.059 1.426 116 0.513 0.029 1.030 0.081 1.615 0.229 4.015 0.331 8.076 0.494 17.135 1.693 1.075 1.438 117 0.538 0.032 1.041 0.082 1.625 0.235 4.061 0.345 8.111 0.504 17.249 1.786 1.080 1.448 118 0.561 0.035 1.050 0.083 1.642 0.240 4.063 0.350 8.1	.358 1.888	1.028	1.399	16.527	0.379	7.824	0.266	3.740		1.559	0.056	0.971	0.024	0.466	112
1140.4710.0250.9830.0641.5940.2073.8770.2917.9600.45716.9611.6401.0441.4061150.4880.0261.0030.0721.6050.2163.9340.3148.0240.47717.1201.6841.0591.4261160.5130.0291.0300.0811.6150.2294.0150.3318.0760.49417.1351.6931.0751.4381170.5380.0321.0410.0821.6250.2354.0610.3458.1110.50417.2491.7861.0801.4481180.5610.0351.0500.0831.6420.2404.0630.3508.1300.51217.4512.0071.0801.460	.378 1.905	1.034	1.520	16.810	0.425	7.889	0.280	3.868	0.199	1.578	0.061	0.977	0.024	0.468	
1150.4880.0261.0030.0721.6050.2163.9340.3148.0240.47717.1201.6841.0591.4261160.5130.0291.0300.0811.6150.2294.0150.3318.0760.49417.1351.6931.0751.4381170.5380.0321.0410.0821.6250.2354.0610.3458.1110.50417.2491.7861.0801.4481180.5610.0351.0500.0831.6420.2404.0630.3508.1300.51217.4512.0071.0801.460	.406 1.920	1.044	1.640	16.961	0.457	7.960	0.291	3.877	0.207	1.594	0.064	0.983	0.025	0.471	
116 0.513 0.029 1.030 0.081 1.615 0.229 4.015 0.331 8.076 0.494 17.135 1.693 1.075 1.438 117 0.538 0.032 1.041 0.082 1.625 0.235 4.061 0.345 8.111 0.504 17.249 1.786 1.080 1.448 118 0.561 0.035 1.050 0.083 1.642 0.240 4.063 0.350 8.130 0.512 17.451 2.007 1.080 1.460	.426 1.926	1.059	1.684	17.120	0.477	8.024	0.314	3.934	0.216	1.605	0.072	1.003	0.026	0.488	
117 0.538 0.032 1.041 0.082 1.625 0.235 4.061 0.345 8.111 0.504 17.249 1.786 1.080 1.448 118 0.561 0.035 1.050 0.083 1.642 0.240 4.063 0.350 8.130 0.512 17.451 2.007 1.080 1.460	.438 1.939	1.075	1.693	17.135	0.494	8.076	0.331	4.015	0.229	1.615	0.081	1.030	0.029	0.513	116
118 0.561 0.035 1.050 0.083 1.642 0.240 4.063 0.350 8.130 0.512 17.451 2.007 1.080 1.460			1.786	17.249	0.504	8.111	0.345	4.061	0.235	1.625	0.082	1.041	0.032	0.538	117
	.460 1.972	1.080	2.007	17.451	0.512	8.130	0.350	4.063	0.240	1.642	0.083	1.050	0.035	0.561	
119 0.577 0.035 1.052 0.092 1.670 0.245 4.079 0.356 8.148 0.519 17.509 2.084 1.081 1.462	.462 1.981	1.081	2.084	17.509	0.519	8.148	0.356	4.079	0.245	1.670	0.092	1.052	0.035	0.577	119
120 0.580 0.036 1.055 0.094 1.694 0.261 4.140 0.367 8.211 0.529 17.605 2.179 1.091 1.467			2.179	17.605	0.529	8.211	0.367	4.140	0.261	1.694	0.094	1.055	0.036	0.580	120
121 0.586 0.038 1.061 0.097 1.705 0.267 4.185 0.388 8.478 0.529 17.734 2.264 1.096 1.476			2.264	17.734	0.529	8.478	0.388	4.185	0.267	1.705	0.097	1.061	0.038	0.586	121
122 0.594 0.040 1.071 0.100 1.717 0.277 4.199 0.407 8.548 0.530 18.049 2.328 1.111 1.494	.494 1.996	1.111	2.328	18.049	0.530	8.548	0.407	4.199	0.277	1.717	0.100	1.071	0.040	0.594	122
123 0.603 0.041 1.081 0.103 1.732 0.287 4.205 0.463 8.561 0.531 18.447 2.375 1.122 1.505	.505 2.012	1.122	2.375	18.447	0.531	8.561	0.463	4.205	0.287	1.732	0.103	1.081	0.041	0.603	123
124 0.610 0.042 1.091 0.106 1.747 0.298 4.212 0.480 8.568 0.532 18.592 2.437 1.135 1.517	.517 2.040	1.135	2.437	18.592	0.532	8.568	0.480	4.212	0.298	1.747	0.106	1.091	0.042	0.610	124
125 0.615 0.042 1.102 0.108 1.763 0.308 4.232 0.506 8.572 0.533 18.657 2.543 1.138 1.546			2.543	18.657	0.533	8.572	0.506	4.232	0.308	1.763	0.108	1.102	0.042	0.615	125
126 0.624 0.042 1.110 0.110 1.779 0.316 4.298 0.518 8.584 0.548 18.796 2.593 1.139 1.569	.569 2.069	1.139	2.593	18.796	0.548	8.584	0.518	4.298	0.316	1.779	0.110	1.110	0.042	0.624	126
	.586 2.092		2.641	18.952	0.610	8.592	0.522	4.344	0.322	1.795	0.112	1.116	0.045	0.628	127

128	0.632	0.046	1.121	0.114	1.810	0.329	4.361	0.525	8.596	0.614	19.137	2.663	1.139 1.596 2.114
129	0.637	0.046	1.125	0.116	1.823	0.338	4.366	0.528	8.597	0.622	19.329	2.672	1.139 1.603 2.132
130	0.641	0.049	1.128	0.118	1.835	0.346	4.369	0.530	8.601	0.631	19.519	2.676	1.139 1.605 2.144
131	0.643	0.050	1.130	0.120	1.845	0.354	4.372	0.530	8.605	0.640	19.707	2.683	1.139 1.606 2.152
132	0.644	0.052	1.132	0.122	1.854	0.356	4.435	0.534	8.608	0.646	19.882	2.817	1.139 1.607 2.157
133	0.645	0.054	1.134	0.123	1.862	0.357	4.523	0.550	8.626	0.650	19.905	2.992	1.139 1.607 2.160
134	0.647	0.054	1.135	0.124	1.870	0.359	4.524	0.554	8.650	0.652	20.049	3.111	1.139 1.608 2.163
135	0.651	0.054	1.143	0.127	1.883	0.362	4.525	0.590	8.660	0.738	20.460	3.234	1.139 1.614 2.165
136	0.658	0.055	1.147	0.130	1.888	0.364	4.531	0.616	8.767	0.754	20.746	3.304	1.160 1.616 2.168
137	0.663	0.055	1.156	0.134	1.896	0.368	4.534	0.639	9.029	0.780	21.068	3.310	1.174 1.631 2.171
138	0.666	0.056	1.163	0.139	1.911	0.378	4.542	0.653	9.238	0.795	21.380	3.320	1.183 1.643 2.186
139	0.668	0.059	1.186	0.146	1.928	0.391	4.553	0.662	9.389	0.804	21.748	3.354	1.197 1.656 2.235
140	0.670	0.061	1.253	0.149	1.949	0.402	4.554	0.683	9.493	0.810	22.046	3.436	1.223 1.673 2.298
141	0.672	0.061	1.262	0.151	1.969	0.408	4.554	0.696	9.583	0.815	22.348	3.443	1.255 1.703 2.333
142	0.675	0.061	1.271	0.153	1.982	0.422	4.554	0.708	9.626	0.818	22.397	3.452	1.272 1.739 2.373
143	0.678	0.063	1.277	0.155	1.999	0.428	4.554	0.721	9.669	0.821	22.407	3.490	1.286 1.767 2.406
144	0.681	0.064	1.283	0.157	2.011	0.432	4.554	0.739	9.716	0.825	22.417	3.552	1.304 1.774 2.416
145	0.684	0.065	1.291	0.162	2.022	0.434	4.554	0.742	9.763	0.840	22.922	3.588	1.307 1.785 2.420
146	0.686	0.066	1.294	0.164	2.035	0.439	4.554	0.743	9.809	0.847	22.951	3.600	1.312 1.806 2.424
147	0.688	0.067	1.296	0.166	2.043	0.450	4.554	0.745	9.852	0.855	22.976	3.616	1.317 1.830 2.435
148	0.690	0.068	1.298	0.168	2.049	0.460	4.554	0.748	9.885	0.865	23.017	3.627	1.321 1.844 2.455
149	0.692	0.069	1.303	0.169	2.063	0.467	4.554	0.751	9.932	0.874	23.073	3.636	1.325 1.845 2.471
150	0.694	0.070	1.316	0.170	2.085	0.472	4.554	0.762	9.986	0.891	23.161	3.676	1.328 1.846 2.484
151	0.696	0.071	1.330	0.171	2.104	0.480	4.556	0.789	10.039	0.914	23.218	3.882	1.332 1.852 2.495
152	0.698	0.072	1.342	0.172	2.117	0.491	4.556	0.790	10.072	0.929	23.253	4.011	1.338 1.868 2.509
153	0.700	0.073	1.348	0.173	2.127	0.503	4.565	0.794	10.090	0.937	23.337	4.047	1.344 1.877 2.522
154	0.702	0.073	1.353	0.175	2.138	0.505	4.612	0.799	10.105	0.942	23.425	4.067	1.350 1.879 2.533
155	0.704	0.074	1.362	0.178	2.152	0.515	4.834	0.805	10.146	0.949	23.534	4.081	1.357 1.886 2.541
156	0.706	0.077	1.365	0.180	2.168	0.522	5.702	0.842	10.245	1.375	23.652	4.116	1.365 1.900 2.552
157	0.708	0.079	1.366	0.189	2.186	0.527	5.841	0.990	10.397	1.576	23.739	4.251	1.379 1.910 2.589
158	0.710	0.082	1.373	0.198	2.205	0.537	6.170	1.038	10.923	1.943	24.606	5.099	1.414 1.936 2.631
159	0.712	0.082	1.397	0.203	2.224	0.549	6.670	1.357	11.970	2.820	25.615	5.383	1.466 1.954 2.704
160	0.716	0.086	1.423	0.207	2.242	0.568	7.425	1.455	13.421	3.281	26.073	6.362	1.514 1.986 2.758
161	0.750	0.095	1.440	0.214	2.268	0.586	8.379	1.546	15.289	3.483	28.496	7.926	1.559 2.050 2.802
162	0.784	0.107	1.452	0.221	2.308	0.610	9.648	1.824	15.912	3.620	29.772	8.429	1.591 2.131 2.904
163	0.805	0.115	1.465	0.229	2.352	0.648	10.918	2.746	16.530	4.168	31.056	9.201	1.641 2.235 2.960
164	0.840	0.122	1.509	0.247	2.406	0.677	12.157	3.073	17.622	4.338	33.351	10.825	1.719 2.320 3.027
165	0.853	0.127	1.533	0.274	2.421	0.699	12.731	3.633	18.366	4.682		12.291	
166	0.874	0.159	1.555	0.309	2.435	0.720	12.831	4.505	19.869	5.633	35.937	13.366	1.832 2.488 3.187
167	0.903	0.186	1.576	0.318	2.470	0.738	12.892	4.952	20.711	6.137	37.012	14.428	1.919 2.563 3.306
168	0.910	0.189	1.598	0.322	2.501	0.767	12.932	5.254	22.319	6.853	37.892	15.318	1.972 2.645 3.384
169	0.914	0.200	1.618	0.333	2.537	0.828	13.702	5.730	23.751	7.136	39.028	15.699	2.013 2.746 3.467
170	0.916	0.220	1.636	0.343	2.571	0.855	14.139	6.051	24.842	7.320	40.406	16.073	2.100 2.778 3.565
171	0.919	0.236	1.666	0.356	2.625	0.869	14.964	6.333	25.410	7.685	41.379	16.475	2.200 2.792 3.640
172	0.931	0.247	1.685	0.385	2.657	0.885	15.704	6.490	25.798	8.052	42.033	17.158	2.251 2.810 3.718
173	0.948	0.257	1.726	0.409	2.683	0.900	16.253	6.796	26.122	8.344	42.432	17.532	2.270 2.847 3.781
174	0.983	0.267	1.742	0.433	2.701	0.941	16.907	7.205	26.353	8.602	42.742	17.965	2.301 2.874 3.827
175	1.018	0.283	1.756	0.453	2.717	0.979	17.655	8.151	26.638	8.898	43.399	18.242	2.318 2.905 3.852
176	1.027	0.295	1.769	0.463	2.732	1.002	18.020	8.230	27.219	9.251	43.895	18.283	2.335 2.950 3.903
177	1.035	0.312	1.784	0.507	2.756	1.025	18.349	8.584	27.279	10.253	44.227	18.480	2.349 3.001 3.930
178	1.051	0.318	1.802	0.523	2.781	1.047	18.671	8.800	27.320	10.828	44.926	19.576	2.387 3.047 3.970
179	1.074	0.323	1.822	0.528	2.811	1.065	18.972	8.847	27.352	10.933	45.256	20.015	2.423 3.104 4.015
180	1.084	0.337	1.843	0.541	2.853	1.089	19.228	8.913	27.822	11.060	45.553	20.203	2.462 3.173 4.074
۰ ا	••••••	••••••	•••••	•••••	••••••		••••••	•••••			• • • • • • • • • • • • • • • • • • • •		

181	1.099	0.345	1.864	0.549	2.898	1.109	20.123	9.122	28.763	11.188	45.753	20.433	2.503	3.238	4.159
182	1.121	0.350	1.884	0.559	2.946	1.133	20.405	9.532	29.402	11.345	46.210	21.025	2.545	3.302	4.230
183	1.132	0.359	1.896	0.571	2.988	1.158	20.754	10.256	29.971	11.733	47.017	21.882	2.586	3.372	4.286
184	1.152	0.387	1.915	0.584	3.023	1.184	21.684	10.862	30.276	12.598	48.185	22,204	2.627	3.452	4.334
185	1.161	0.398	1.940	0.598	3.057	1.209	21.955	10.996	30.988	12.953	48.741	22.859	2.673	3.545	4.388
186	1.168	0.400	1.958	0.613	3.076	1.222	22.650	11.206	31.095	13.213	49.462	23.533	2.749	3.648	4.447
187	1.175	0.402	1.972	0.624	3.101	1.231	22.989	11.514	31.314	14.131	50.313	24.281	2.804	3.701	4.505
188	1.181	0.405	1.985	0.629	3.120	1.239	23.535	11.894	31.833	14.839	51.285	25.078	2.851	3.759	4.561
189	1.188	0.418	1.991	0.629	3.136	1.254	23.876	12.019	32.239	15.137	52.076	25.276	2.894	3.821	4.625
190	1.203	0.429	1.993	0.638	3.151	1.278	24.018	12.170	32.547	15.138	52.857	25.578	2.931	3.870	4.696
191	1.219	0.442	1.995	0.648	3.163	1.300	24.464	12.517	32.855	15.141	52.876	25.859	2.971	•••••	
192	1.233	0.457	2.001	0.659	3.209	1.313	24.685	12.598	33.153	15.595	53.067	25.985	3.020	•••••	
193	1.251	0.473	2.015	0.663	3.223	1.324	24.931	12.625	33.444	15.658	53.777	26.153	3.077	•••••	
194	1.255	0.487	2.031	0.671	3.237	1.340	25.188	12.653	33.482	15.704	54.242	26.582	3.132	•••••	
195	1.258	0.501	2.047	0.681	3.263	1.367	25.468	12.777	33.516	15.729	54.489	27.067	3.185	•••••	
196	1.265	0.510	2.063	0.693	3.302	1.387	25.627	12.906	33.549	16.058	54.601	27.456	3.219	•••••	
197	1.205	0.510	2.005	0.709	3.338	1.402	25.746	12.989	33.653	16.987	54.912	27.805	3.268		
198	1.200	0.512	2.075	0.705	3.372	1.417	25.850	13.060	33.973	17.064	55.588	28.070	3.299	•••••	
199								13.165					3.350	•••••	
	1.301	0.516	2.109	0.740	3.390	1.432	25.974		34.159	17.073	56.266	28.590			
200	1.313	0.518	2.122	0.754	3.428	1.446	26.141	13.242	34.191	17.153	56.617	28.914	3.406		
201	1.324	0.527	2.130	0.767	3.470	1.460	26.225	13.412	34.250	17.332	56.863	29.063	3.466	•••••	
202	1.332	0.540	2.137	0.775	3.493	1.477	26.338	13.662	34.469	17.406	57.204	29.502	3.497		
203	1.341	0.547	2.157	0.787	3.509	1.492	26.547	13.773	34.716	17.641	57.371	29.697	3.514		
204	1.357	0.553	2.172	0.795	3.522	1.501	26.818	13.942	34.969	17.922	57.487	29.713	3.517		
205	1.375	0.559	2.194	0.803	3.533	1.510	27.052	14.090	35.144	18.484	57.728	29.783	3.519		
206	1.392	0.563	2.222	0.854	3.550	1.522	27.393	14.224	35.418	18.553	58.097	29.942	3.523		
207	1.408	0.567	2.245	0.859	3.578	1.561	27.501	14.426	35.766	18.658	58.572	30.284	3.545		
208	1.422	0.571	2.268	0.872	3.607	1.585	27.632	14.498	35.949	18.953	59.024	30.755	3.570		
209	1.433	0.575	2.279	0.892	3.630	1.597	27.803	14.776	36.010	19.266	59.321	31.287	3.600	•••••	
210	1.443	0.579	2.288	0.896	3.658	1.607	27.953	14.907	36.548	19.309	59.715	31.549	3.619		
211	1.453	0.595	2.301	0.903	3.701	1.627	28.205	14.916	37.179	19.731	60.045	31.820	3.639	4.638	5.657
212	1.463	0.605	2.316	0.924	3.745	1.645	28.543	15.014	37.651	19.902	60.453	32.250	3.686	•••••	
213	1.468	0.614	2.332	0.938	3.778	1.656	28.997	15.221	38.041	20.012	60.935	32.546	3.732	•••••	
214	1.470	0.622	2.345	0.941	3.814	1.663	29.000	15.472	38.591	20.260	61.307	32.808	3.791	•••••	
215	1.474	0.627	2.354	0.951	3.825	1.669	29.005	15.555	38.852	20.739	61.666	33.060	3.833		
216	1.478	0.638	2.362	0.966	3.835	1.674	29.081	15.652	38.861	21.346	62.148	33.204	3.890	4.931	5.884
217	1.481	0.643	2.368	0.979	3.844	1.685	29.281	15.969	38.926	21.810	62.532	33.341		4.960	5.908
218	1.484	0.643	2.376	0.980	3.853	1.700	29.483	16.028	39.194	22.001	62.546	33.414	3.960	4.963	5.921
219	1.487	0.645	2.384	0.981	3.864	1.704	29.734	16.375	39.474	22.290	62.559	33.514	3.997	4.965	5.931
220	1.490	0.651	2.391	1.005	3.874	1.706	29.803	16.487	39.668	22.324	62.570	33.640	4.013	4.968	5.939
221	1.493	0.655	2.395	1.016	3.891	1.709	29.821	16.524	39.781	22.343	62.846	33.692	4.035	4.971	5.947
222	1.504	0.663	2.400	1.022	3.928	1.711	29.847	16.578	39.890	22.522	63.097	33.711	4.038	4.974	5.952
223	1.522	0.671	2.405	1.028	3.966	1.714	29.862	16.684	39.954	22.661	63.150	33.733	4.050	4.977	5.955
224	1.547	0.675	2.409	1.035	4.008	1.718	29.873	16.755	39.984	22.666	63.150	33.770	4.066	4.979	5.957
225	1.549	0.684	2.413	1.041	4.010	1.721	30.008	16.770	39.989	22.667	63.150	33.796	4.070	4.980	5.959
226	1.562	0.694	2.415	1.045	4.012	1.723	30.126	16.805	39.990	22.668	63.150	33.810	4.072	4.981	5.961
227	1.574	0.701	2.417	1.051	4.016	1.726	30.127	16.865	39.990	22.669	63.150	33.821	4.072	4.982	5.963
228	1.579	0.702	2.419	1.055	4.019	1.729	30.127	16.960	39.990	22.670	63.150	33.839	4.073	4.983	5.966
229	1.584	0.708	2.420	1.059	4.057	1.731	30.208	16.960	39.991	22.671	63.150	33.865	4.073	4.984	5.971
230	1.589	0.708	2.421	1.062	4.065	1.733	30.314	16.962	40.012	22.671	63.150	33.894	4.073	4.985	5.977
231	1.590	0.709	2.423	1.063	4.071	1.735	30.323	16.988	40.061	22.672	63.150	33.918	4.073	4.986	5.984
232	1.596	0.710	2.425	1.063	4.073	1.743	30.325	17.072	40.116	22.673	63.150	33.944	4.074	4.987	
233	1.598	0.710	2.427	1.063	4.075	1.749	30.368	17.094	40.249	22.673	63.150	33.985			
• 			••••••		••••••		L	•••••	••••••		•••••		.	•••••	••••••

234	1.604	0.711	2.429	1.064	4.077	1.753	30.411	17.184	40.253	22.673	63.153	34.014	4.075	4.989	6.004
235	1.610	0.712	2.430	1.064	4.079	1.757	30.416	17.187	40.290	22.674	63.159	34.032	4.075	4.990	6.012
236	1.612	0.712	2.431	1.066	4.081	1.762	30.428	17.188	40.385	22.675	63.173	34.051	4.076	4.991	6.024
237	1.613	0.712	2.432	1.069	4.083	1.767	30.430	17.189	40.488	22.675	63.193	34.067	4.076	4.992	6.037
238	1.614	0.713	2.433	1.072	4.084	1.772	30.452	17.241	40.720	22.675	63.214	34.079	4.076	4.993	6.049
239	1.615	0.716	2.434	1.075	4.085	1.776	30.488	17.370	40.763	22.677	63.233	34.085	4.076	4.994	6.060

Appendix B Alternative Fast-Pass IM240 Standards

Alternative Fast-Pass IM240 Standards Corresponding to Composite Start-up Emission Standards in §85.2205(a)(2)(i) and §85.2205(a)(2)(ii) Light Duty Vehicles

]	Low Al	titude	Lov	v Altitu	ıde	Lov	v Altitu	ıde	High Al	titude
Sec		1981-	1982		1983-	1990		1991·	1995		1982	
	HC	СО	NOx	HC	CO	NOx	HC	CO	NOx	HC	CO	NOx
30	0.330	4.189	0.250	0.330	1.941	0.251	0.174	1.307	0.222	0.330	7.391	0.250
31	0.342	4.278	0.267	0.342	1.983	0.268	0.179	1.329	0.246	0.342	7.667	0.267
32	0.353	4.366	0.283	0.353	2.025	0.285	0.184	1.350	0.270	0.353	7.944	0.283
33	0.364	4.455	0.300	0.365	2.067	0.302	0.189	1.372	0.294	0.364	8.220	0.300
34	0.375	4.544	0.316	0.376	2.108	0.320	0.194	1.394	0.318	0.375	8.497	0.316
35	0.386	4.633	0.333	0.388	2.150	0.337	0.199	1.416	0.342	0.386	8.773	0.333
36	0.398	4.728	0.336	0.399	2.230	0.339	0.201	1.453	0.345	0.398	9.011	0.336
37	0.409	4.823	0.339	0.410	2.310	0.342	0.203	1.490	0.348	0.409	9.249	0.339
38	0.420	4.917	0.342	0.420	2.390	0.344	0.205	1.527	0.350	0.420	9.488	0.342
39	0.431	5.012	0.345	0.431	2.471	0.347	0.207	1.565	0.353	0.431	9.726	0.345
40	0.443	5.107	0.348	0.442	2.551	0.349	0.209	1.602	0.356	0.443	9.964	0.348
41	0.458	5.429	0.371	0.458	2.738	0.373	0.214	1.642	0.373	0.458	10.527	0.371
42	0.474	5.751	0.394	0.473	2.926	0.397	0.219	1.682	0.390	0.474	11.090	0.394
43	0.489	6.073	0.418	0.489	3.114	0.422	0.224	1.722	0.407	0.489	11.652	0.418
44	0.505	6.395	0.441	0.505	3.302	0.446	0.228	1.763	0.425	0.505	12.215	0.441
45	0.521	6.717	0.465	0.520	3.489	0.470	0.233	1.803	0.442	0.521	12.778	0.465
46	0.535	6.985	0.480	0.536	3.589	0.486	0.238	1.867	0.465	0.535	13.265	0.480
47	0.550	7.254	0.496	0.552	3.688	0.501	0.244	1.932	0.487	0.550	13.751	0.496
48	0.565	7.522	0.512	0.568	3.787	0.517	0.250	1.997	0.510	0.565	14.238	0.512
49	0.580	7.791	0.527	0.584	3.887	0.533	0.255	2.061	0.533	0.580	14.724	0.527
50	0.594	8.060	0.543	0.600	3.986	0.549	0.261	2.126	0.555	0.594	15.211	0.543
51	0.611	8.511	0.567	0.617	4.029	0.571	0.268	2.152	0.573	0.611	15.550	0.567
52	0.628	8.962	0.590	0.633	4.072	0.594	0.275	2.179	0.590	0.628	15.889	0.590
53	0.644	9.413	0.613	0.649	4.115	0.616	0.282	2.205	0.608	0.644	16.228	0.613
54	0.661	9.865	0.637	0.665	4.157	0.638	0.290	2.232	0.625	0.661	16.567	0.637
55	0.678	10.316	0.660	0.681	4.200	0.661	0.297	2.258	0.643	0.678	16.907	0.660
56	0.691	10.818	0.675	0.696	4.263	0.676	0.302	2.348	0.654	0.691	17.199	0.675
57	0.705	11.320	0.689	0.710	4.326	0.691	0.306	2.437	0.666	0.705	17.492	0.689
58		11.822								0.718	17.785	0.703
59	0.731									0.731	18.078	0.718
60	0.745	12.827	0.732	0.754	4.514	0.737	0.320	2.705	0.700	0.745	18.371	0.732
61	0.758	13.228	0.743	0.767	4.589	0.748	0.323	2.726	0.707	0.758	18.609	0.743
62	0.772	13.629	0.754	0.780	4.664	0.758	0.326	2.746	0.714	0.772	18.847	0.754
63	0.786	14.029	0.764	0.794	4.740	0.769	0.329	2.767	0.722	0.786	19.085	0.764
64	0.799	14.430	0.775	0.807	4.815	0.780	0.332	2.787	0.729	0.799	19.323	0.775
65	0.813	14.831	0.786	0.820	4.891	0.790	0.335	2.808	0.736	0.813	19.562	0.786
66	0.827	15.046	0.794	0.833	4.945	0.799	0.340	2.812	0.742	0.827	19.887	0.794
67	0.841	15.261	0.803	0.846	4.999	0.808	0.345	2.816	0.747	0.841	20.213	0.803

68	0.855 15.476 0.811	0.859 5.053 0.817	0.350 2.820 0.753	0.855 20.539 0.811
<u>69</u>		0.872 5.107 0.826	••••••••••••	
70	0.883 15.907 0.828	0.885 5.162 0.835	0.360 2.829 0.764	0.883 21.191 0.828
71	0.894 16.118 0.838	0.896 5.226 0.846	•••••••••	0.894 21.396 0.838
72	0.905 16.330 0.848	0.906 5.291 0.857	0.367 2.865 0.802	
73	0.917 16.542 0.858	0.917 5.356 0.868	0.371 2.884 0.822	0.917 21.808 0.858
74	0.928 16.753 0.868	0.928 5.421 0.878	0.375 2.902 0.841	0.928 22.013 0.868
75	0.939 16.965 0.878	0.939 5.486 0.889	0.378 2.921 0.860	0.939 22.219 0.878
76	0.953 17.199 0.891	0.952 5.553 0.900	0.387 2.982 0.874	0.953 22.685 0.891
77	0.967 17.432 0.904	0.965 5.620 0.911	0.396 3.044 0.888	
78	0.981 17.666 0.917	0.978 5.687 0.922	0.405 3.106 0.902	0.981 23.617 0.917
79	0.994 17.900 0.930	0.991 5.754 0.933	0.414 3.167 0.916	0.994 24.083 0.930
80	1.008 18.133 0.944	1.004 5.821 0.944	0.423 3.229 0.930	1.008 24.549 0.944
81	1.019 18.182 0.951	1.015 5.842 0.951	0.428 3.240 0.945	1.019 24.570 0.951
82	1.031 18.231 0.958	1.026 5.863 0.959	0.432 3.250 0.959	1.031 24.591 0.958
83	1.042 18.280 0.965	1.037 5.883 0.966	0.437 3.261 0.973	1.042 24.612 0.965
84	1.053 18.329 0.972	1.048 5.904 0.973	0.441 3.271 0.987	1.053 24.633 0.972
85	1.065 18.378 0.979	1.059 5.925 0.980	0.445 3.281 1.002	1.065 24.654 0.979
86	1.072 18.393 0.980	1.067 5.970 0.981	0.448 3.290 1.003	1.072 24.666 0.980
87	1.079 18.408 0.981	1.075 6.015 0.982	0.452 3.298 1.004	1.079 24.678 0.981
88	1.086 18.423 0.982	1.083 6.060 0.982	0.455 3.306 1.005	1.086 24.690 0.982
89	1.093 18.438 0.983	1.091 6.105 0.983	0.458 3.315 1.006	1.093 24.703 0.983
90	1.099 18.453 0.983	1.099 6.151 0.984	0.462 3.323 1.007	1.099 24.715 0.983
91	1.107 18.467 0.984	1.106 6.185 0.985	0.463 3.360 1.008	1.107 24.737 0.984
92	1.114 18.481 0.985	1.114 6.219 0.986	0.464 3.397 1.008	1.114 24.758 0.985
93	1.121 18.495 0.985	1.122 6.253 0.986	0.465 3.434 1.009	1.121 24.780 0.985
94	1.128 18.509 0.986	1.129 6.287 0.987	0.466 3.470 1.009	1.128 24.801 0.986
95	1.135 18.523 0.986	1.137 6.321 0.988	0.468 3.507 1.010	1.135 24.823 0.986
96	1.149 18.681 0.992	1.150 6.489 0.993	0.472 3.536 1.011	1.149 25.193 0.992
97	1.162 18.840 0.997	1.163 6.657 0.999	0.477 3.565 1.012	1.162 25.563 0.997
98	1.176 18.998 1.002	1.176 6.825 1.004	0.481 3.594 1.013	1.176 25.933 1.002
99	1.189 19.157 1.008	1.189 6.992 1.009	0.486 3.623 1.014	1.189 26.303 1.008
100	1.203 19.315 1.013	1.202 7.160 1.014	0.490 3.651 1.015	1.203 26.672 1.013
101	1.223 20.090 1.049	1.224 7.269 1.049	0.499 3.685 1.042	1.223 27.821 1.049
102	1.244 20.864 1.085	1.245 7.378 1.084	0.509 3.719 1.069	1.244 28.969 1.085
103	1.264 21.639 1.121	1.266 7.487 1.119	0.518 3.753 1.097	1.264 30.117 1.121
104	1.285 22.414 1.157	1.287 7.596 1.154	0.527 3.787 1.124	1.285 31.265 1.157
105	1.305 23.189 1.193	1.309 7.705 1.189		1.305 32.414 1.193
106	1.319 23.461 1.224	1.323 7.835 1.215	0.541 3.842 1.194	1.319 33.103 1.224
107	1.333 23.733 1.255	1.338 7.965 1.241	0.545 3.863 1.237	1.333 33.792 1.255
108	1.346 24.006 1.286	1.352 8.095 1.267	0.548 3.884 1.280	
109	1.360 24.278 1.317	1.367 8.225 1.293	0.552 3.904 1.323	1.360 35.170 1.317
110	1.374 24.550 1.348	1.382 8.355 1.319	0.556 3.925 1.366	1.374 35.859 1.348
111	1.385 24.846 1.356			••••••
112	1.396 25.141 1.363	1.406 8.472 1.336	0.568 3.937 1.371	1.396 36.495 1.363

113	1.407 25.437 1.371	1.418 8.531 1.345	0.574 3.943 1.374	1.407 36.813 1.371
114			0.580 3.949 1.377	
115	1.428 26.028 1.386	1.442 8.649 1.363		
116	1.437 26.045 1.388	1.451 8.735 1.364	•••••••	•••••••••••••••••••••••••••••••••••••••
117	1.446 26.062 1.389	1.460 8.821 1.365		••••••
118	1.455 26.079 1.391	1.469 8.907 1.366		1.455 37.761 1.391
119	1.464 26.096 1.393	1.479 8.992 1.368	•••••••••••••••••••••••••••••••••••••••	1.464 37.865 1.393
120	1.472 26.114 1.394	1.488 9.078 1.369	0.604 4.055 1.383	1.472 37.969 1.394
121	1.488 26.293 1.408	1.501 9.152 1.385	0.610 4.152 1.400	1.488 38.310 1.408
122	1.503 26.472 1.422	1.514 9.227 1.401	0.615 4.250 1.417	1.503 38.650 1.422
123	1.518 26.651 1.435	1.527 9.301 1.417	0.621 4.348 1.433	1.518 38.990 1.435
124	1.534 26.830 1.449	1.540 9.375 1.434	0.627 4.445 1.450	1.534 39.330 1.449
125	1.549 27.010 1.463	1.553 9.449 1.450	0.632 4.543 1.466	1.549 39.671 1.463
126	1.559 27.151 1.471	1.563 9.519 1.458	0.636 4.567 1.470	1.559 39.865 1.471
127	1.569 27.292 1.479	1.572 9.590 1.467	0.639 4.592 1.473	1.569 40.059 1.479
128	1.579 27.433 1.487	1.582 9.661 1.475	0.642 4.617 1.476	1.579 40.254 1.487
129	1.590 27.575 1.495	1.592 9.731 1.484	0.645 4.641 1.479	1.590 40.448 1.495
130	1.600 27.716 1.502	1.601 9.802 1.492	0.648 4.666 1.482	1.600 40.642 1.502
131	1.612 27.878 1.506	1.615 9.849 1.496	0.653 4.685 1.483	1.612 40.790 1.506
132	1.624 28.040 1.509	1.628 9.895 1.500	0.657 4.704 1.485	1.624 40.937 1.509
133	1.635 28.202 1.512	1.642 9.942 1.504	0.661 4.724 1.486	1.635 41.084 1.512
134	1.647 28.365 1.515	1.655 9.989 1.508	0.666 4.743 1.488	1.647 41.231 1.515
135	1.659 28.527 1.519	1.669 10.035 1.512	0.670 4.762 1.489	1.659 41.379 1.519
136	1.676 28.833 1.542	1.685 10.104 1.534	0.678 4.785 1.507	1.676 42.023 1.542
137	1.693 29.140 1.566	1.700 10.173 1.557	0.685 4.807 1.524	1.693 42.668 1.566
138	1.709 29.446 1.589	1.716 10.241 1.580	0.693 4.830 1.541	1.709 43.312 1.589
139	1.726 29.753 1.613	1.732 10.310 1.603	•••••	••••••
140	1.743 30.060 1.636	1.747 10.378 1.626	•••••	1.743 44.602 1.636
141	1.756 30.160 1.651	1.762 10.506 1.640	••••••	1.756 45.010 1.651
142	1.770 30.260 1.666	1.777 10.633 1.655	•••••	•••••
143	1.783 30.361 1.681	1.791 10.761 1.669		
144	1.797 30.461 1.696		0.738 4.918 1.640	
145	1.810 30.562 1.711	1.821 11.016 1.699		
146	1.822 30.592 1.720	1.830 11.101 1.709		
147	1.834 30.622 1.730	1.840 11.187 1.720	•••••	1.834 47.244 1.730
148	1.846 30.653 1.740	1.850 11.273 1.730	0.760 5.004 1.679	1.846 47.544 1.740
149	1.858 30.683 1.750	1.860 11.359 1.741 1.869 11.445 1.752	0.765 5.029 1.687	1.858 47.843 1.750
150	1.869 30.713 1.760			1.869 48.143 1.760
151 152	1.880 30.741 1.767 1.890 30.768 1.775	1.879 11.504 1.759 1 890 11 564 1 767	0.775 5.060 1.711	1.880 48.423 1.767 1.890 48.704 1.775
· · · · · · · · · · · ·	1.890 30.768 1.775 1.900 30.796 1.783	1.890 11.564 1.767 1.900 11.624 1.775	0.780 5.065 1.727	1.890 48.704 1.775 1 900 48 984 1 783
153 154	1.90030.7961.7831.91030.8231.791	1.900 11.024 1.775 1.910 11.683 1.783	0.785 5.070 1.743 0.791 5.075 1.760	1.900 48.984 1.783 1.910 49.265 1.791
· · · · · · · · · · · · ·		1.910 11.085 1.785 1.920 11.743 1.790		
155	1.920 30.850 1.798 1.940 32.415 1.828	1.920 11.743 1.790 1.945 12.434 1.821	0.796 5.080 1.776 0.819 5.150 1.813	••••••
156	1.949 32.415 1.828 1.977 33.980 1.858			• • • • • • • • • • • • • • • • • • • •
157	1.977 33.980 1.858	1.971 13.125 1.852	0.842 5.220 1.850	1.977 51.489 1.858

158	2.006 35.545 1.888	1 996 13 816 1 883	0.865 5.290 1.887	2.006 52.461 1.888
159	2.034 37.110 1.918	2.022 14.507 1.913		
160	2.063 38.674 1.948	2.047 15.198 1.944		
161	2.105 41.040 2.043	2.092 16.627 2.038		•••••••••••••••••••••••••••••••••••••••
162	2.147 43.405 2.138	2.137 18.056 2.133	•••••	• • • • • • • • • • • • • • • • • • • •
163	2.190 45.770 2.234	2.182 19.485 2.227	1.032 10.276 2.168	2.190 60.026 2.234
164	2.232 48.136 2.329	2.227 20.914 2.321	1.073 11.891 2.237	
165	2.275 50.501 2.424	2.272 22.343 2.415	1.113 13.506 2.306	•••••
166	2.304 52.979 2.509	2.300 23.672 2.502	1.163 14.131 2.357	2.304 65.726 2.509
167	2.333 55.458 2.593	2.328 25.002 2.589	1.213 14.755 2.409	2.333 67.678 2.593
168	2.362 57.937 2.678	2.356 26.331 2.676	1.263 15.380 2.460	2.362 69.631 2.678
169	2.391 60.415 2.762	2.385 27.660 2.763	1.313 16.004 2.512	2.391 71.584 2.762
170	2.420 62.894 2.847	2.413 28.989 2.849	1.363 16.628 2.564	2.420 73.536 2.847
171	2.451 63.874 2.890	2.442 29.484 2.892	1.386 16.692 2.603	2.451 75.553 2.890
172	2.481 64.855 2.933	2.472 29.978 2.934	1.410 16.756 2.643	2.481 77.570 2.933
173	2.512 65.835 2.976	2.502 30.473 2.976	1.433 16.820 2.683	2.512 79.587 2.976
174	2.542 66.815 3.019	2.532 30.967 3.019	1.457 16.883 2.723	2.542 81.604 3.019
175	2.573 67.796 3.062	2.562 31.462 3.061	1.480 16.947 2.762	2.573 83.621 3.062
176	2.598 68.919 3.122	2.588 32.216 3.119	1.494 17.044 2.809	2.598 85.074 3.122
177	2.623 70.042 3.181	2.615 32.970 3.178	1.508 17.141 2.856	2.623 86.528 3.181
178	2.648 71.165 3.240	2.641 33.725 3.236	1.522 17.238 2.903	2.648 87.981 3.240
179	2.674 72.287 3.300	2.668 34.479 3.295	1.536 17.335 2.949	2.674 89.434 3.300
180	2.699 73.410 3.359	2.694 35.233 3.353	1.550 17.431 2.996	2.699 90.888 3.359
181	2.726 74.714 3.432	2.718 35.950 3.424	1.565 17.453 3.040	2.726 92.421 3.432
182	2.753 76.017 3.504	2.743 36.666 3.495	1.580 17.475 3.084	2.753 93.953 3.504
183	2.780 77.320 3.576	2.767 37.382 3.567	1.595 17.497 3.129	2.780 95.486 3.576
184	2.807 78.623 3.648	2.791 38.099 3.638	1.610 17.519 3.173	2.807 97.019 3.648
185	2.834 79.927 3.720	2.816 38.815 3.709	1.624 17.540 3.217	2.834 98.552 3.720
186	2.861 81.488 3.804	2.843 39.562 3.795	1.639 17.816 3.277	2.861 100.583 3.804
187	2.888 83.049 3.889	2.869 40.309 3.880	1.654 18.091 3.337	2.888 102.615 3.889
188	2.915 84.611 3.973	2.896 41.056 3.965	1.668 18.366 3.397	2.915 104.646 3.973
189	2.942 86.172 4.057	2.923 41.803 4.051	1.683 18.641 3.457	2.942 106.677 4.057
190	2.969 87.733 4.141	2.950 42.550 4.136	1.697 18.916 3.518	2.969 108.709 4.141
191	2.994 88.668 4.196	2.975 43.279 4.190	1.711 19.891 3.565	2.994 110.057 4.196
192	3.019 89.603 4.250	3.001 44.008 4.243		
193	3.044 90.538 4.304	3.027 44.737 4.297	1.737 21.840 3.658	3.044 112.753 4.304
194	3.070 91.473 4.358	3.052 45.466 4.351	1.750 22.815 3.705	3.070 114.101 4.358
195	3.095 92.407 4.412	3.078 46.195 4.404	1.763 23.790 3.752	3.095 115.449 4.412
196	3.120 93.768 4.485	3.105 46.747 4.477	1.778 24.992 3.794	
197	3.145 95.129 4.558	3.132 47.299 4.549	1.793 26.194 3.836	3.145 117.674 4.558
198	3.169 96.490 4.630	3.159 47.852 4.622	1.808 27.396 3.877	••••••
199	3.194 97.851 4.703	3.186 48.404 4.694	1.823 28.597 3.919	3.194 119.899 4.703
200	3.219 99.212 4.775	3.213 48.957 4.767	1.838 29.799 3.960	3.219 121.011 4.775
201	3.242 99.878 4.821	3.234 49.204 4.812		
202	3.266 100.544 4.867	3.255 49.451 4.858	1.877 30.152 4.047	3.266 122.378 4.867

203	3.289 101.210 4.914	3.277 49.698 4.904	1.897 30.328 4.090	3.289 123.062 4.914
204				3.312 123.745 4.960
205	3.335 102.542 5.006	3.320 50.192 4.996	1.936 30.680 4.176	3.335 124.429 5.006
206			1.948 30.747 4.193	
207	3.388 104.472 5.069	3.373 51.205 5.063	1.961 30.813 4.209	3.388 126.769 5.069
208	3.415 105.437 5.101	3.399 51.711 5.097	1.973 30.879 4.225	3.415 127.939 5.101
209	3.441 106.402 5.132	3.426 52.218 5.130	1.986 30.946 4.241	3.441 129.109 5.132
210	3.468 107.366 5.164	3.452 52.724 5.164	1.998 31.012 4.257	3.468 130.279 5.164
211	3.488 108.519 5.234	3.472 53.327 5.233	2.006 32.744 4.311	3.488 132.009 5.234
212	3.509 109.671 5.304	3.492 53.931 5.303	2.015 34.476 4.365	3.509 133.740 5.304
213	3.530 110.823 5.374	3.513 54.534 5.372	2.023 36.207 4.419	3.530 135.470 5.374
214	3.550 111.976 5.444	3.533 55.137 5.442	2.031 37.939 4.473	3.550 137.201 5.444
215	3.571 113.128 5.514	3.553 55.740 5.511	2.039 39.671 4.527	3.571 138.931 5.514
216	3.591 113.763 5.564	3.571 56.057 5.559	2.044 39.822 4.565	3.591 140.070 5.564
217	3.612 114.398 5.613	3.589 56.373 5.606	2.048 39.973 4.602	3.612 141.208 5.613
218	3.632 115.033 5.663	3.608 56.689 5.654	2.053 40.125 4.640	3.632 142.347 5.663
219	3.652 115.668 5.713	3.626 57.005 5.701	2.058 40.276 4.677	3.652 143.485 5.713
220	3.672 116.304 5.763	3.644 57.321 5.749	2.062 40.427 4.715	3.672 144.624 5.763
221	3.693 116.644 5.775	3.669 57.474 5.761	2.076 40.526 4.724	3.693 144.903 5.775
222	3.714 116.984 5.787	3.693 57.626 5.773	2.089 40.626 4.732	3.714 145.182 5.787
223	3.736 117.324 5.799	3.717 57.779 5.785	2.103 40.725 4.741	3.736 145.462 5.799
224	3.757 117.663 5.811	3.741 57.931 5.797	2.117 40.825 4.750	3.757 145.741 5.811
225	3.778 118.003 5.823	3.766 58.084 5.809	2.130 40.924 4.759	3.778 146.020 5.823
226	3.795 118.158 5.828	3.782 58.158 5.814	2.160 40.962 4.764	3.795 146.177 5.828
227	3.811 118.312 5.833	3.798 58.232 5.820	2.190 41.000 4.770	3.811 146.334 5.833
228	3.828 118.466 5.838	3.815 58.307 5.825	2.219 41.038 4.775	3.828 146.491 5.838
229	3.845 118.621 5.842	3.831 58.381 5.830	2.249 41.076 4.781	3.845 146.648 5.842
230	3.862 118.775 5.847	3.848 58.455 5.835	2.278 41.114 4.786	3.862 146.805 5.847
231	3.873 118.885 5.852	3.858 58.534 5.840	2.285 41.142 4.790	3.873 147.057 5.852
232	3.884 118.995 5.856	3.868 58.612 5.845	2.292 41.171 4.794	3.884 147.308 5.856
233	3.896 119.105 5.860			
234	3.907 119.215 5.865	3.889 58.769 5.855	2.306 41.228 4.801	3.907 147.812 5.865
235	3.918 119.325 5.869	3.900 58.847 5.860	2.313 41.256 4.805	3.918 148.064 5.869
236	3.924 119.407 5.874	3.907 58.990 5.865	2.315 41.285 4.808	3.924 148.450 5.874
237	3.930 119.488 5.878	3.913 59.132 5.869	2.318 41.313 4.812	3.930 148.837 5.878
238	3.935 119.570 5.883		•••••	
239	3.941 119.651 5.887	••••••••••••••••	•••••	
240	3.947 119.733 5.892	3.934 59.560 5.883	2.325 41.397 4.822	3.947 149.996 5.892

Alternative Fast-Pass IM240 Standards Corresponding to Composite Start-up Emission Standards in §85.2205(a)(2)(iv)

Light Duty Truck 1&2

		1982-	1983		1984-	1987		1988-	1990		1991	
Sec	HC	CO	NOx	HC	CO	NOx	HC	СО	NOx	HC	CO	NOx
30	1.064	14.776	0.562	0.585	10.661	0.513	0.585	10.661	0.298	0.477	5.069	0.254
31	1.091	15.338	0.610	0.609	11.033	0.551	0.609	11.033	0.319	0.494	5.129	0.270
32	1.118	15.900	0.657	0.633	11.405	0.590	0.633	11.405	0.340	0.512	5.189	0.285
33	1.145	16.462	0.705	0.657	11.777	0.629	0.657	11.777	0.361	0.529	5.249	0.300
34	1.172	17.023	0.752	0.681	12.149	0.667	0.681	12.149	0.382	0.547	5.309	0.316
35	1.199	17.585	0.800	0.705	12.521	0.706	0.705	12.521	0.403	0.564	5.369	0.331
36	1.237	17.834	0.804	0.730	12.895	0.711	0.730	12.895	0.407	0.582	5.562	0.334
37	1.275	18.084	0.808	0.754	13.269	0.716	0.754	13.269	0.410	0.601	5.755	0.336
38	1.313	18.333	0.813	0.779	13.643	0.721	0.779	13.643	0.414	0.619	5.948	0.339
39	1.351	18.582	0.817	0.803	14.018	0.727	0.803	14.018	0.418	0.637	6.142	0.341
40	1.389	18.832	0.822	0.828	14.392	0.732	0.828	14.392	0.422	0.656	6.335	0.344
41	1.459	19.867	0.869	0.854	15.098	0.796	0.854	15.098	0.451	0.681	6.890	0.368
42	1.529	20.902	0.915	0.880	15.805	0.861	0.880	15.805	0.479	0.707	7.445	0.392
43	1.599	21.937	0.962	0.907	16.511	0.925	0.907	16.511	0.508	0.732	7.999	0.416
44	1.669	22.972	1.009	0.933	17.217	0.989	0.933	17.217	0.536	0.758	8.554	0.440
45	1.738	24.008	1.056	0.959	17.924	1.053	0.959	17.924	0.565	0.783	9.109	0.464
46	1.784	24.572	1.098	0.989	18.458	1.096	0.989	18.458	0.587	0.799	9.593	0.480
47	1.830	25.136	1.140	1.019	18.992	1.138	1.019	18.992	0.609	0.816	10.076	0.496
48	1.876	25.701	1.182	1.050	19.526	1.180	1.050	19.526	0.631	0.832	10.560	0.512
49	1.922	26.265	1.224	1.080	20.060	1.223	1.080	20.060	0.652	0.848	11.044	0.528
50	1.968	26.830	1.266	1.110	20.594	1.265	1.110	20.594	0.674	0.864	11.527	0.543
51	2.020	27.642	1.305	1.146	21.719	1.294	1.146	21.719	0.701	0.891	12.038	0.563
52	2.072	28.454	1.343	1.182	22.845	1.324	1.182	22.845	0.728	0.917	12.549	0.582
53	2.124	29.266	1.381	1.218	23.970	1.353	1.218	23.970	0.755	0.943	13.059	0.601
54	2.176	30.079	1.420	1.254	25.095	1.382	1.254	25.095	0.782	0.969	13.570	0.621
55	2.228	30.891	1.458	1.290	26.221	1.411	1.290	26.221	0.809	0.995	14.081	0.640
56	2.265	31.485	1.490	1.310	26.449	1.449	1.310	26.449	0.826	1.015	14.438	0.653
57	2.302	32.078	1.522	1.330	26.677	1.486	1.330	26.677	0.842	1.035	14.796	0.666
58	2.340	32.672	1.555	1.350	26.905	1.523	1.350	26.905	0.859	1.055	15.154	0.679
59	2.377	33.266	1.587	1.370	27.133	1.560	1.370	27.133	0.876	1.075	15.512	0.692
60	2.415	33.860	1.619	1.390	27.361	1.597	1.390	27.361	0.892	1.095	15.870	0.705
61	2.451	34.449	1.637	1.405	27.372	1.611	1.405	27.372	0.903	1.109	16.268	0.714
62	2.487	35.037	1.656	1.420	27.383	1.625	1.420	27.383	0.915	1.124	16.667	0.723
63	2.523	35.626	1.674	1.434	27.393	1.639	1.434	27.393	0.926	1.138	17.066	0.732
64	2.559	36.215	1.693	1.449	27.404	1.653	1.449	27.404	0.938	1.153	17.465	0.741
65	2.595	36.804		1.464	27.415	1.667		27.415			17.863	0.750
66	2.639	37.463	1.737	1.497	28.054	1.699	1.497	28.054	0.960	1.182	18.249	0.759
67	2.683	38.122	1.763	1.530	28.694	1.732	1.530	28.694	0.972	1.196	18.635	0.768
68	2.728	38.782	1.789	1.563	29.333	1.765	1.563	29.333	0.983	1.211	19.020	0.777

69	2.772 39.441 1.815	1.596 29.972 1.797	1.596 29.972 0.994	1.225 19.406 0.786
70	2.817 40.100 1.841	1.629 30.612 1.830	1.629 30.612 1.005	1.239 19.792 0.795
71	2.859 40.631 1.862	1.650 31.097 1.854	1.650 31.097 1.016	1.255 19.906 0.805
72	2.901 41.161 1.884	1.672 31.583 1.878	1.672 31.583 1.028	1.271 20.020 0.815
73	2.943 41.692 1.906	1.694 32.068 1.902	1.694 32.068 1.039	1.287 20.134 0.825
74	2.985 42.222 1.928	1.715 32.554 1.925	1.715 32.554 1.051	1.303 20.248 0.835
75	3.027 42.753 1.950	1.737 33.039 1.949	1.737 33.039 1.062	1.318 20.362 0.845
76	3.061 43.694 1.978	1.760 33.193 1.977	1.760 33.193 1.074	1.331 20.782 0.859
77	3.096 44.636 2.007	1.782 33.347 2.005	1.782 33.347 1.085	1.344 21.202 0.874
78	3.130 45.577 2.035	1.805 33.501 2.033	1.805 33.501 1.096	1.357 21.623 0.888
79	3.165 46.519 2.063	1.828 33.655 2.061	1.828 33.655 1.108	1.370 22.043 0.902
80	3.200 47.461 2.092	1.851 33.809 2.089	1.851 33.809 1.119	1.382 22.463 0.916
81	3.237 47.831 2.111	1.872 34.035 2.111	1.872 34.035 1.131	1.407 22.571 0.925
82	3.275 48.201 2.130	1.894 34.261 2.132	1.894 34.261 1.144	1.431 22.678 0.934
83	3.313 48.571 2.149	1.915 34.488 2.154	1.915 34.488 1.156	1.455 22.786 0.942
84	3.351 48.941 2.168	1.937 34.714 2.175	1.937 34.714 1.169	1.480 22.894 0.951
85	3.389 49.311 2.187	1.958 34.941 2.197	1.958 34.941 1.181	1.504 23.001 0.960
86	3.432 49.503 2.189	1.973 35.115 2.200	1.973 35.115 1.182	1.531 23.112 0.961
87	3.475 49.694 2.192	1.988 35.289 2.203	1.988 35.289 1.182	1.558 23.223 0.963
88	3.518 49.886 2.194	2.002 35.463 2.206	2.002 35.463 1.183	1.586 23.334 0.964
89	3.562 50.077 2.197	2.017 35.637 2.209	2.017 35.637 1.184	1.613 23.445 0.966
90	3.605 50.269 2.199	2.032 35.811 2.212	2.032 35.811 1.185	1.640 23.556 0.967
91	3.645 50.447 2.200	2.044 35.968 2.213	2.044 35.968 1.186	1.654 23.558 0.968
92	3.686 50.626 2.201	2.056 36.125 2.214	2.056 36.125 1.187	1.668 23.560 0.968
93	3.727 50.805 2.202	2.068 36.282 2.215	2.068 36.282 1.188	1.682 23.562 0.968
94	3.767 50.984 2.203	2.081 36.440 2.216	2.081 36.440 1.189	1.696 23.564 0.969
95	3.808 51.162 2.204	2.093 36.597 2.217	2.093 36.597 1.190	1.710 23.567 0.969
96	3.853 51.779 2.212	2.111 36.968 2.227	2.111 36.968 1.195	1.727 23.924 0.978
97	3.898 52.395 2.219	2.129 37.339 2.236	2.129 37.339 1.201	1.744 24.282 0.987
98	3.943 53.012 2.227	2.147 37.710 2.245	2.147 37.710 1.207	1.762 24.639 0.996
99	3.988 53.628 2.234	2.165 38.081 2.254	2.165 38.081 1.213	1.779 24.997 1.004
100	4.033 54.245 2.242	2.183 38.453 2.263	2.183 38.453 1.218	1.796 25.355 1.013
101	4.081 55.131 2.322	2.221 40.429 2.342	2.221 40.429 1.259	1.819 25.871 1.045
102	4.128 56.016 2.403	2.258 42.405 2.420	2.258 42.405 1.299	1.842 26.387 1.076
103	4.175 56.902 2.484	2.295 44.382 2.498	2.295 44.382 1.340	1.865 26.903 1.107
104	4.223 57.788 2.565	2.333 46.358 2.576	2.333 46.358 1.380	1.887 27.419 1.139
105	4.270 58.674 2.646	2.370 48.335 2.654	2.370 48.335 1.421	1.910 27.935 1.170
106	4.300 59.222 2.721	2.404 49.060 2.740	2.404 49.060 1.458	1.936 28.221 1.201
107	4.331 59.771 2.797	2.437 49.785 2.826	2.437 49.785 1.495	1.962 28.506 1.232
108	4.361 60.319 2.872	2.471 50.511 2.912	2.471 50.511 1.531	1.988 28.792 1.263
109	4.391 60.868 2.948	2.504 51.236 2.998	2.504 51.236 1.568	2.014 29.077 1.294
110	4.421 61.416 3.023	2.538 51.962 3.084	2.538 51.962 1.605	2.040 29.363 1.325
111	4.449 61.935 3.038	2.560 52.113 3.101	2.560 52.113 1.615	2.057 29.405 1.332
112	4.476 62.455 3.053	2.582 52.265 3.118	2.582 52.265 1.624	2.074 29.447 1.338
113	4.503 62.974 3.067	2.604 52.417 3.136	2.604 52.417 1.634	2.090 29.489 1.344

1 1 1 4 1	4.531 63.493 3.082	2.625 52.569 3.153	2.625 52.569 1.644	2 107 20 521 1 250
114				
115	4.558 64.013 3.097	2.647 52.721 3.170	2.647 52.721 1.653	2.124 29.573 1.357
116	4.600 64.559 3.099	2.673 52.723 3.173	2.673 52.723 1.656	2.152 29.865 1.359
117	4.642 65.105 3.102	2.698 52.724 3.175	2.698 52.724 1.658	2.179 30.157 1.361
118	4.684 65.651 3.105	2.723 52.726 3.178	2.723 52.726 1.661	2.207 30.449 1.363
119	4.726 66.197 3.108	2.749 52.728 3.181	2.749 52.728 1.663	2.234 30.741 1.365
120	4.768 66.743 3.111	2.774 52.729 3.184	2.774 52.729 1.666	2.262 31.033 1.368
121	4.804 67.600 3.134	2.799 53.168 3.206	2.799 53.168 1.684	2.276 31.230 1.383
122	4.840 68.458 3.156	2.824 53.606 3.229	2.824 53.606 1.703	2.290 31.428 1.399
123	4.876 69.315 3.179	2.850 54.044 3.251	2.850 54.044 1.722	2.304 31.625 1.415
124	4.911 70.173 3.202	2.875 54.483 3.274	2.875 54.483 1.741	2.318 31.823 1.431
125	4.947 71.030 3.224	2.900 54.921 3.296	2.900 54.921 1.759	2.332 32.020 1.446
126	4.983 71.729 3.241	2.920 55.078 3.310	2.920 55.078 1.770	2.355 32.099 1.453
127	5.019 72.427 3.257	2.941 55.236 3.323	2.941 55.236 1.780	2.377 32.178 1.460
128	5.055 73.126 3.274	2.961 55.393 3.337	2.961 55.393 1.790	2.399 32.256 1.468
129	5.091 73.825 3.290	2.981 55.551 3.350	2.981 55.551 1.800	2.422 32.335 1.475
130	5.126 74.523 3.307	3.001 55.708 3.364	3.001 55.708 1.811	2.444 32.413 1.482
131	5.178 75.331 3.311	3.027 55.921 3.370	3.027 55.921 1.813	2.464 32.638 1.484
132	5.230 76.139 3.316	3.052 56.134 3.376	3.052 56.134 1.816	2.485 32.862 1.487
133	5.282 76.947 3.321	3.078 56.346 3.382	3.078 56.346 1.819	2.505 33.086 1.490
134	5.334 77.755 3.326	3.103 56.559 3.388	3.103 56.559 1.822	2.525 33.310 1.492
135	5.386 78.563 3.331	3.129 56.771 3.394	3.129 56.771 1.825	2.545 33.534 1.495
136	5.468 79.372 3.365	3.167 57.854 3.432	3.167 57.854 1.851	2.573 34.147 1.520
137	5.549 80.181 3.398	3.206 58.937 3.469	3.206 58.937 1.877	2.600 34.760 1.546
138	5.630 80.990 3.431	3.244 60.020 3.507	3.244 60.020 1.903	2.628 35.373 1.571
139	5.712 81.798 3.464	3.283 61.102 3.544	3.283 61.102 1.929	2.655 35.985 1.596
140	5.793 82.607 3.498	3.322 62.185 3.582	3.322 62.185 1.955	2.682 36.598 1.622
141	5.825 83.486 3.536	3.342 62.366 3.639	3.342 62.366 1.977	2.702 36.880 1.639
141	5.856 84.365 3.575	3.363 62.548 3.697	3.363 62.548 1.999	2.722 37.162 1.656
143	5.888 85.245 3.613	3.383 62.729 3.754	3.383 62.729 2.021	2.742 37.444 1.673
144	5.920 86.124 3.652	3.404 62.910 3.811	3.404 62.910 2.043	2.762 37.727 1.691
145	5.951 87.003 3.690	3.425 63.091 3.869	3.425 63.091 2.065	2.782 38.009 1.708
145	5.975 87.915 3.718	3.453 63.539 3.892	3.453 63.539 2.074	2.782 38.609 1.708 2.797 38.632 1.717
140			3.482 63.987 2.082	
	5.998 88.827 3.745	3.482 63.987 3.916		
148	6.022 89.739 3.772	3.510 64.435 3.939	3.510 64.435 2.090	2.825 39.878 1.735
149	6.046 90.652 3.800	3.539 64.883 3.963	3.539 64.883 2.098	2.839 40.501 1.743
150	6.069 91.564 3.827	3.568 65.331 3.986	3.568 65.331 2.106	2.853 41.124 1.752
151	6.099 92.475 3.852	3.595 65.704 4.000	3.595 65.704 2.117	2.868 41.450 1.765
152	6.129 93.387 3.877	3.623 66.077 4.014	3.623 66.077 2.129	2.883 41.776 1.778
153	6.159 94.298 3.901	3.650 66.450 4.029	3.650 66.450 2.141	2.898 42.102 1.791
154	6.189 95.209 3.926	3.677 66.823 4.043	3.677 66.823 2.152	2.913 42.428 1.803
155	6.219 96.121 3.951	3.705 67.197 4.057	3.705 67.197 2.164	2.927 42.754 1.816
156	6.313 97.599 4.030	3.767 69.206 4.117	3.767 69.206 2.205	2.969 44.233 1.849
157	6.407 99.077 4.110	3.829 71.215 4.176	3.829 71.215 2.247	3.011 45.712 1.882
158	6.501 100.555 4.190	3.891 73.225 4.236	3.891 73.225 2.289	3.053 47.191 1.915

159	6.595 102.033 4.269	3.953 75.234 4.295	3.953 75.234 2.330	3.095 48.670 1.948
160	6.689 103.511 4.349	4.015 77.243 4.355	4.015 77.243 2.372	3.136 50.149 1.981
161	7.010 107.552 4.542	4.078 79.985 4.551	4.078 79.985 2.472	3.182 51.569 2.071
162	7.331 111.593 4.736	4.142 82.727 4.747	4.142 82.727 2.571	3.227 52.988 2.162
163	7.652 115.634 4.930	4.205 85.469 4.943	4.205 85.469 2.671	3.272 54.408 2.252
164	7.972 119.676 5.123	4.268 88.211 5.139	4.268 88.211 2.770	3.318 55.828 2.343
165	8.293 123.717 5.317	4.332 90.953 5.335	4.332 90.953 2.870	3.363 57.247 2.434
166	8.576 125.252 5.496	4.380 93.266 5.516	4.380 93.266 2.961	3.410 58.958 2.509
167	8.859 126.786 5.676	4.428 95.579 5.696	4.428 95.579 3.053	3.458 60.670 2.584
168	9.142 128.321 5.855	4.477 97.892 5.876	4.477 97.892 3.144	3.505 62.381 2.659
169	9.425 129.855 6.034	4.525 100.205 6.056	4.525 100.205 3.235	3.552 64.092 2.735
170	9.708 131.390 6.213	4.573 102.517 6.237	4.573 102.517 3.327	3.600 65.804 2.810
171	9.788 132.095 6.318	4.618 103.813 6.345	4.618 103.813 3.373	3.644 66.939 2.863
172	9.868 132.801 6.422	4.664 105.109 6.452	4.664 105.109 3.420	3.688 68.075 2.916
173	9.948 133.506 6.527	4.709 106.404 6.560	4.709 106.404 3.467	3.732 69.210 2.969
174	10.028 134.211 6.632	4.754 107.700 6.668	4.754 107.700 3.513	3.776 70.345 3.022
175	10.107 134.917 6.736	4.799 108.995 6.776	4.799 108.995 3.560	3.821 71.481 3.075
176	10.174 137.703 6.876	4.858 110.733 6.910	4.858 110.733 3.626	3.856 73.077 3.130
177	10.242 140.490 7.016	4.917 112.471 7.045	4.917 112.471 3.692	3.891 74.674 3.185
178	10.309 143.276 7.155	4.977 114.209 7.179	4.977 114.209 3.758	3.927 76.271 3.240
179	10.376 146.063 7.295	5.036 115.946 7.313	5.036 115.946 3.824	3.962 77.867 3.295
180	10.443 148.849 7.435	5.095 117.684 7.447	5.095 117.684 3.889	3.997 79.464 3.350
181	10.506 152.900 7.603	5.158 119.775 7.621	5.158 119.775 3.979	4.024 81.282 3.430
182	10.570 156.950 7.772	5.221 121.866 7.795	5.221 121.866 4.069	4.050 83.100 3.509
183	10.634 161.001 7.941	5.284 123.956 7.969	5.284 123.956 4.159	4.077 84.919 3.589
184	10.698 165.051 8.110	5.347 126.047 8.143	5.347 126.047 4.248	4.104 86.737 3.668
185	10.761 169.102 8.279	5.411 128.138 8.318	5.411 128.138 4.338	4.131 88.555 3.748
186	10.836 171.850 8.477	5.428 129.673 8.499	5.428 129.673 4.443	4.154 90.333 3.841
187	10.911 174.598 8.675	5.446 131.209 8.681	5.446 131.209 4.547	4.178 92.110 3.934
188	10.986 177.345 8.873	5.463 132.745 8.862	5.463 132.745 4.652	4.202 93.888 4.026
189	11.061 180.093 9.071	5.481 134.281 9.043	5.481 134.281 4.756	4.225 95.665 4.119
190	11.136 182.841 9.269	5.499 135.816 9.225	5.499 135.816 4.861	4.249 97.442 4.212
191	11.307 184.591 9.422	5.561 137.198 9.386	5.561 137.198 4.932	4.285 98.856 4.274
192	11.477 186.341 9.576	5.623 138.580 9.547	5.623 138.580 5.003	4.321 100.271 4.336
193	11.648 188.091 9.730	5.686 139.961 9.708	5.686 139.961 5.074	4.357 101.685 4.398
194	11.819 189.841 9.884	5.748 141.343 9.869	5.748 141.343 5.146	4.393 103.099 4.459
195	11.990 191.591 10.038	5.810 142.724 10.030	5.810 142.724 5.217	4.430 104.513 4.521
196	12.067 194.037 10.193	5.828 144.052 10.188	5.828 144.052 5.301	4.460 106.134 4.589
197	12.144 196.482 10.348	5.845 145.381 10.346	5.845 145.381 5.385	4.490 107.755 4.658
198	12.221 198.927 10.503	5.863 146.709 10.504	5.863 146.709 5.469	4.520 109.376 4.726
199	12.298 201.373 10.658	5.880 148.037 10.662	5.880 148.037 5.553	4.550 110.997 4.795
200	12.376 203.818 10.813	5.898 149.365 10.820	5.898 149.365 5.637	4.580 112.617 4.863
201	12.463 204.868 10.912	5.942 150.214 10.948	5.942 150.214 5.692	4.623 113.207 4.906
202	12.551 205.918 11.012	5.986 151.063 11.075	5.986 151.063 5.746	4.666 113.796 4.949
203	12.639 206.967 11.111	6.029 151.912 11.203	6.029 151.912 5.801	4.709 114.385 4.993

204	12.726 208.017 11.211	6.073 152.760 11.330	6.073 152.760 5.856	4.752 114.974 5.036
205	12.814 209.067 11.310	6.117 153.609 11.458	6.117 153.609 5.911	4.795 115.563 5.079
206	12.891 211.915 11.381	6.174 154.888 11.530	6.174 154.888 5.951	4.848 116.847 5.119
207	12.969 214.764 11.452	6.231 156.166 11.601	6.231 156.166 5.990	4.901 118.131 5.160
208	13.046 217.612 11.523	6.288 157.445 11.673	6.288 157.445 6.030	4.955 119.415 5.201
209	13.124 220.460 11.594	6.345 158.724 11.745	6.345 158.724 6.070	5.008 120.699 5.241
210	13.201 223.309 11.665	6.401 160.002 11.817	6.401 160.002 6.110	5.061 121.983 5.282
211	13.243 226.365 11.862	6.451 161.606 11.984	6.451 161.606 6.194	5.090 123.498 5.355
212	13.285 229.421 12.060	6.500 163.210 12.152	6.500 163.210 6.278	5.119 125.012 5.429
213	13.327 232.478 12.257	6.550 164.814 12.319	6.550 164.814 6.362	5.147 126.526 5.502
214	13.370 235.534 12.455	6.599 166.418 12.486	6.599 166.418 6.446	5.176 128.040 5.576
215	13.412 238.591 12.653	6.649 168.022 12.653	6.649 168.022 6.530	5.204 129.554 5.649
216	13.470 240.891 12.778	6.693 168.948 12.780	6.693 168.948 6.585	5.240 130.345 5.695
217	13.528 243.191 12.904	6.737 169.874 12.906	6.737 169.874 6.640	5.275 131.136 5.741
218	13.586 245.492 13.030	6.782 170.800 13.032	6.782 170.800 6.695	5.310 131.928 5.787
219	13.645 247.792 13.156	6.826 171.726 13.159	6.826 171.726 6.750	5.345 132.719 5.833
220	13.703 250.092 13.282	6.870 172.653 13.285	6.870 172.653 6.804	5.380 133.510 5.879
221	13.896 250.710 13.307	6.946 173.200 13.314	6.946 173.200 6.818	5.436 133.899 5.888
222	14.088 251.329 13.332	7.022 173.748 13.343	7.022 173.748 6.831	5.492 134.287 5.896
223	14.281 251.947 13.358	7.098 174.295 13.371	7.098 174.295 6.844	5.548 134.676 5.905
224	14.474 252.565 13.383	7.173 174.843 13.400	7.173 174.843 6.857	5.604 135.064 5.913
225	14.667 253.184 13.409	7.249 175.391 13.429	7.249 175.391 6.870	5.660 135.453 5.922
226	14.845 253.888 13.422	7.334 175.611 13.440	7.334 175.611 6.877	5.699 135.633 5.927
227	15.023 254.593 13.436	7.419 175.831 13.452	7.419 175.831 6.884	5.738 135.814 5.931
228	15.201 255.297 13.450	7.504 176.051 13.464	7.504 176.051 6.891	5.776 135.995 5.936
229	15.379 256.002 13.464	7.589 176.271 13.475	7.589 176.271 6.897	5.815 136.176 5.941
230	15.557 256.706 13.478	7.674 176.491 13.487	7.674 176.491 6.904	5.854 136.356 5.946
231	15.658 257.286 13.488	7.710 176.612 13.498	7.710 176.612 6.910	5.875 136.581 5.951
232	15.759 257.866 13.499	7.746 176.732 13.508	7.746 176.732 6.916	5.897 136.806 5.956
233	15.861 258.445 13.510	7.782 176.853 13.519	7.782 176.853 6.922	5.918 137.031 5.962
234	15.962 259.025 13.521	7.818 176.974 13.530	7.818 176.974 6.928	5.940 137.256 5.967
235	16.063 259.605 13.531	7.853 177.095 13.540	7.853 177.095 6.934	5.961 137.482 5.972
236	16.104 259.940 13.543	7.867 177.463 13.551	7.867 177.463 6.940	5.977 137.680 5.978
237	16.144 260.276 13.554	7.881 177.830 13.561	7.881 177.830 6.946	5.994 137.879 5.983
238	16.185 260.612 13.566	7.894 178.198 13.572	7.894 178.198 6.951	6.010 138.078 5.989
239	16.225 260.947 13.577	7.908 178.566 13.582	7.908 178.566 6.957	6.026 138.277 5.994
240	16.265 261.283 13.589	7.922 178.933 13.592	7.922 178.933 6.962	6.042 138.476 6.000

Alternative Fast-Pass IM240 Standards Corresponding to Composite Start-up Emission Standards in §85.2205(a)(2)(vi)

Light Duty Truck 3&4

	1982-19	83		1984-198	37		1988-19	90		1991	
Sec	нс со	NOx	HC	СО	NOx	нс	СО	NOx	HC	СО	NOx
30	1.064 14.776	0.513	0.585	10.661	0.513	0.585	10.661	0.436	0.477	5.069	0.395
31	1.091 15.338	0.551	0.609	11.033	0.551	0.609	11.033	0.463	0.494	5.129	0.420
32	1.118 15.900	0.590	0.633	11.405	0.590	0.633	11.405	0.490	0.512	5.189	0.445
33	1.145 16.462	0.629	0.657	11.777	0.629	0.657	11.777	0.517	0.529	5.249	0.470
34	1.172 17.023	0.667	0.681	12.149	0.667	0.681	12.149	0.544	0.547	5.309	0.495
35	1.199 17.585	0.706	0.705	12.521	0.706	0.705	12.521	0.572	0.564	5.369	0.520
36	1.237 17.834	0.711	0.730	12.895	0.711	0.730	12.895	0.576	0.582	5.562	0.524
37	1.275 18.084	0.716	0.754	13.269	0.716	0.754	13.269	0.580	0.601	5.755	0.527
38	1.313 18.333	0.721	0.779	13.643	0.721	0.779	13.643	0.584	0.619	5.948	0.531
39	1.351 18.582	0.727	0.803	14.018	0.727	0.803	14.018	0.588	0.637	6.142	0.535
40	1.389 18.832	0.732	0.828	14.392	0.732	0.828	14.392	0.592	0.656	6.335	0.539
41	1.459 19.867	0.796	0.854	15.098	0.796	0.854	15.098	0.636	0.681	6.890	0.578
42	1.529 20.902	0.861	0.880	15.805	0.861	0.880	15.805	0.681	0.707	7.445	0.617
43	1.599 21.937	0.925	0.907	16.511	0.925	0.907	16.511	0.726	0.732	7.999	0.657
44	1.669 22.972	0.989	0.933	17.217	0.989	0.933	17.217	0.771	0.758	8.554	0.696
45	1.738 24.008	1.053	0.959	17.924	1.053	0.959	17.924	0.815	0.783	9.109	0.735
46	1.784 24.572	1.096	0.989	18.458	1.096	0.989	18.458	0.840	0.799	9.593	0.760
47	1.830 25.136	1.138	1.019	18.992	1.138	1.019	18.992	0.866	0.816	10.076	0.785
48	1.876 25.701	1.180	1.050	19.526	1.180	1.050	19.526	0.891	0.832	10.560	0.810
49	1.922 26.265	1.223	1.080	20.060	1.223	1.080	20.060	0.916	0.848	11.044	0.835
50	1.968 26.830	1.265	1.110	20.594	1.265	1.110	20.594	0.941	0.864	11.527	0.860
51	2.020 27.642	1.294	1.146	21.719	1.294	1.146	21.719	0.978	0.891	12.038	0.893
52	2.072 28.454	1.324	1.182	22.845	1.324	1.182	22.845	1.016	0.917	12.549	0.926
53	2.124 29.266	1.353	1.218	23.970	1.353	1.218	23.970	1.053	0.943	13.059	0.959
54	2.176 30.079	1.382	1.254	25.095	1.382	1.254	25.095	1.090	0.969	13.570	0.992
55	2.228 30.891	1.411	1.290	26.221	1.411	1.290	26.221	1.128	0.995	14.081	1.026
56	2.265 31.485	1.449	1.310	26.449	1.449	1.310	26.449	1.160	1.015	14.438	1.051
57	2.302 32.078	1.486	1.330	26.677	1.486	1.330	26.677	1.192	1.035	14.796	1.077
58	2.340 32.672				1.523		26.905				
59	2.377 33.266	1.560	1.370	27.133	1.560	1.370	27.133	1.256	1.075	15.512	1.129
60	2.415 33.860	1.597	1.390	27.361	1.597	1.390	27.361	1.288	1.095	15.870	1.155
61	2.451 34.487	1.611	1.405	27.372	1.611	1.405	27.372	1.301	1.109	16.268	1.166
62	2.487 35.113	1.625	1.420	27.383	1.625	1.420	27.383	1.313	1.124	16.667	1.177
63	2.523 35.740	1.639	1.434	27.393	1.639	1.434	27.393	1.326	1.138	17.066	1.188
64	2.559 36.367	1.653	1.449	27.404	1.653	1.449	27.404	1.338	1.153	17.465	1.200
65	2.595 36.994	1.667	1.464	27.415	1.667	1.464	27.415	1.351	1.167	17.863	1.211
66	2.639 37.728	1.699	1.497	28.054	1.699	1.497	28.054	1.366	1.182	18.249	1.230
67	2.683 38.462	1.732	1.530	28.694	1.732	1.530	28.694	1.382	1.196	18.635	1.250
68	2.728 39.197	1.765	1.563	29.333	1.765	1.563	29.333	1.397	1.211	19.020	1.269

69	2.772 39.931 1.7	97 1 596 29 972	1.797	1.596 29.972 1.412	1 225 19 406 1 289
70	2.817 40.666 1.8			•••••••••••••••••••••••••••••••••••••••	1.229 19.792 1.308
70	2.859 41.083 1.8				1.255 19.906 1.321
72	2.901 41.500 1.8				$\frac{1.233}{1.271} \ 20.020 \ 1.334$
72	2.943 41.918 1.9				1.271 20.020 1.334
73	2.945 42.335 1.9			1.715 32.554 1.491	1.303 20.248 1.361
74	3.027 42.753 1.9			1.713 32.334 1.491 1.737 33.039 1.507	
76	3.061 43.705 1.9			1.760 33.193 1.528	
77				$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.331 20.782 1.391 1.344 21.202 1.409
78	<u>3.096 44.657 2.0</u> 3.130 45.609 2.0			$\begin{array}{c} 1.782 & 33.547 & 1.550 \\ 1.805 & 33.501 & 1.571 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
78 79					1.370 22.043 1.444
80	3.165 46.562 2.0 3.200 47.514 2.0		• • • •	1.828 33.809 1.615	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
81	3.237 47.873 2.1				1.382 22.403 1.401 1.407 22.571 1.475
82					
83	3.275 48.233 2.1 3.313 48.592 2.1			1.894 34.261 1.632	$\frac{1.431}{1.455} \ \frac{22.678}{22.786} \ \frac{1.489}{1.503}$
03 84	3.351 48.952 2.1 3.351 48.952 2.1			$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	
85				1.958 34.941 1.657	
86	3.432 49.503 2.2			1.973 35.115 1.659	$\frac{1.531}{1.558} \begin{array}{c} 23.112 \\ 1.532 \\ 1.558 \\ 1.558 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 \\ 1.522 $
87	3.475 49.694 2.2			1.988 35.289 1.661	1.558 23.223 1.532
88	3.518 49.886 2.2			2.002 35.463 1.663	1.586 23.334 1.533
89	3.562 50.077 2.2			2.017 35.637 1.665	1.613 23.445 1.533
90	3.605 50.269 2.2			2.032 35.811 1.667	
91	3.645 50.447 2.2			2.044 35.968 1.668	1.654 23.558 1.534
92	3.686 50.626 2.2			2.056 36.125 1.669	1.668 23.560 1.534
93	3.727 50.805 2.2			2.068 36.282 1.671	$\frac{1.682}{1.682} \begin{array}{c} 23.562 \\ 1.535 \\ 1.696 \\ 23.564 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535 \\ 1.535$
94	3.767 50.984 2.2			2.081 36.440 1.672	1.696 23.564 1.535
95	3.808 51.162 2.2				1.710 23.567 1.535
96	3.853 51.779 2.2				1.727 23.924 1.547
97	3.898 52.395 2.2			2.129 37.339 1.686	1.744 24.282 1.558
98	3.943 53.012 2.2				1.762 24.639 1.570
99	3.988 53.628 2.2			2.165 38.081 1.698	1 = 0 (
100	4.033 54.245 2.2				1.796 25.355 1.593
101	4.081 55.131 2.3				1.819 25.871 1.636
102	4.128 56.016 2.4				1.842 26.387 1.678
103	4.175 56.902 2.4				1.865 26.903 1.721
104	4.223 57.788 2.5				1.887 27.419 1.764
105	4.270 58.674 2.6	••••••			1.910 27.935 1.807
106	4.300 59.222 2.7	•••••••		•••••••••••••••••••••••••••••••••••••••	1.936 28.221 1.864
107	4.331 59.771 2.8				1.962 28.506 1.921
108	4.361 60.319 2.9				1.988 28.792 1.978
109	4.391 60.868 2.9	•••••••		•••••••••••••••••••••••••••••••••••••••	2.014 29.077 2.035
110	4.421 61.416 3.0		••••••		2.040 29.363 2.092
111	4.449 61.935 3.1	•••••••	••••••		2.057 29.405 2.107
112	4.476 62.455 3.1				2.074 29.447 2.121
113	4.503 62.974 3.1	36 2.604 52.417	3.136	2.604 52.417 2.396	2.090 29.489 2.135

1114	4 521 (2 402 2 152	2 (25 52 5(0 2 152	2 (25 52 5(0 2 411	2 107 20 521 2 140
114			2.625 52.569 2.411	
115	4.558 64.013 3.170	2.647 52.721 3.170	2.647 52.721 2.426	
116	4.600 64.559 3.173	2.673 52.723 3.173	2.673 52.723 2.430	2.152 29.865 2.166
117	4.642 65.105 3.175	2.698 52.724 3.175	2.698 52.724 2.433	2.179 30.157 2.169
118	4.684 65.651 3.178	2.723 52.726 3.178	2.723 52.726 2.437	2.207 30.449 2.173
119	4.726 66.197 3.181	2.749 52.728 3.181	2.749 52.728 2.441	2.234 30.741 2.176
120	4.768 66.743 3.184	2.774 52.729 3.184	2.774 52.729 2.445	2.262 31.033 2.179
121	4.804 67.600 3.206	2.799 53.168 3.206	2.799 53.168 2.467	2.276 31.230 2.200
122	4.840 68.458 3.229	2.824 53.606 3.229	2.824 53.606 2.489	2.290 31.428 2.222
123	4.876 69.315 3.251	2.850 54.044 3.251	2.850 54.044 2.512	2.304 31.625 2.243
124	4.911 70.173 3.274	2.875 54.483 3.274	2.875 54.483 2.534	2.318 31.823 2.265
125	4.947 71.030 3.296	2.900 54.921 3.296	2.900 54.921 2.557	2.332 32.020 2.286
126	4.983 71.729 3.310	2.920 55.078 3.310	2.920 55.078 2.569	2.355 32.099 2.297
127	5.019 72.427 3.323	2.941 55.236 3.323	2.941 55.236 2.580	2.377 32.178 2.307
128	5.055 73.126 3.337	2.961 55.393 3.337	2.961 55.393 2.592	2.399 32.256 2.318
129	5.091 73.825 3.350	2.981 55.551 3.350	2.981 55.551 2.604	2.422 32.335 2.329
130	5.126 74.523 3.364	3.001 55.708 3.364	3.001 55.708 2.616	2.444 32.413 2.339
131	5.178 75.331 3.370	3.027 55.921 3.370	3.027 55.921 2.619	2.464 32.638 2.343
132	5.230 76.139 3.376	3.052 56.134 3.376	3.052 56.134 2.623	2.485 32.862 2.347
133	5.282 76.947 3.382	3.078 56.346 3.382	3.078 56.346 2.627	2.505 33.086 2.350
134	5.334 77.755 3.388	3.103 56.559 3.388	3.103 56.559 2.630	2.525 33.310 2.354
135	5.386 78.563 3.394	3.129 56.771 3.394	3.129 56.771 2.634	2.545 33.534 2.358
136	5.468 79.372 3.432	3.167 57.854 3.432	3.167 57.854 2.672	2.573 34.147 2.395
137	5.549 80.181 3.469	3.206 58.937 3.469	3.206 58.937 2.711	2.600 34.760 2.431
138	5.630 80.990 3.507	3.244 60.020 3.507	3.244 60.020 2.749	2.628 35.373 2.468
139	5.712 81.798 3.544	3.283 61.102 3.544	3.283 61.102 2.787	2.655 35.985 2.505
139	5.793 82.607 3.582	3.322 62.185 3.582	3.322 62.185 2.826	2.682 36.598 2.542
141		3.322 02.105 3.302 3.342 62.366 3.639	3.342 62.366 2.851	2.702 36.880 2.574
142	5.856 84.365 3.697	3.363 62.548 3.697	3.363 62.548 2.875	2.722 37.162 2.606
143	5.888 85.245 3.754	3.383 62.729 3.754	3.383 62.729 2.900	2.742 37.444 2.638
144	5.920 86.124 3.811	3.404 62.910 3.811	3.404 62.910 2.925	2.762 37.727 2.671
145	5.951 87.003 3.869	3.425 63.091 3.869	• • • • • • • • • • • • • • • • • • • •	2.782 38.009 2.703
146	5.975 87.915 3.892	3.453 63.539 3.892	3.453 63.539 2.959	
147	5.998 88.827 3.916	3.482 63.987 3.916	3.482 63.987 2.968	
148	6.022 89.739 3.939	3.510 64.435 3.939	3.510 64.435 2.978	2.825 39.878 2.738
149	6.046 90.652 3.963	3.539 64.883 3.963	3.539 64.883 2.987	2.839 40.501 2.750
150	6.069 91.564 3.986	3.568 65.331 3.986	3.568 65.331 2.997	2.853 41.124 2.762
151	6.099 92.475 4.000	3.595 65.704 4.000	3.595 65.704 3.007	2.868 41.450 2.774
152	6.129 93.387 4.014	3.623 66.077 4.014	3.623 66.077 3.017	2.883 41.776 2.786
153	6.159 94.298 4.029	3.650 66.450 4.029	3.650 66.450 3.028	2.898 42.102 2.799
154	6.189 95.209 4.043	3.677 66.823 4.043	3.677 66.823 3.038	2.913 42.428 2.811
155	6.219 96.121 4.057	3.705 67.197 4.057	3.705 67.197 3.049	2.927 42.754 2.823
156	6.313 97.599 4.117	3.767 69.206 4.117	3.767 69.206 3.113	2.969 44.233 2.870
157	6.407 99.077 4.176	3.829 71.215 4.176	3.829 71.215 3.178	3.011 45.712 2.917
158	6.501 100.555 4.236	3.891 73.225 4.236	3.891 73.225 3.242	3.053 47.191 2.964
•			•••••••••••••••••••••••••••••••••••••••	•••••••••

159	6.595 102.033 4.295	3.953 75.234 4.295	3 953 75 234 3 307	3.095 48.670 3.011
160	6.689 103.511 4.355	4.015 77.243 4.355	4.015 77.243 3.371	
161	7.010 107.552 4.551	4.078 79.985 4.551	4.078 79.985 3.503	3.182 51.569 3.181
162	7.331 111.593 4.747	4.142 82.727 4.747	4.142 82.727 3.635	3.227 52.988 3.306
162	7.652 115.634 4.943	4.205 85.469 4.943	4.205 85.469 3.767	3.272 54.408 3.430
164	7.972 119.676 5.139	4.268 88.211 5.139	4.268 88.211 3.899	3.318 55.828 3.554
165	8.293 123.717 5.335	4.332 90.953 5.335	4.332 90.953 4.030	3.363 57.247 3.678
166	8.671 125.252 5.516	4.380 93.266 5.516	4.380 93.266 4.145	3.410 58.958 3.796
167	9.050 126.786 5.696		4.428 95.579 4.260	3.410 38.938 3.790 3.458 60.670 3.914
167	9.428 128.321 5.876	4.428 95.579 5.696 4.477 97.892 5.876	4.477 97.892 4.375	3.505 62.381 4.033
169	9.806 129.855 6.056	4.525 100.205 6.056	4.525 100.205 4.490	3.552 64.092 4.151
109	10.184 131.390 6.237	4.573 102.517 6.237	4.573 102.517 4.605	3.600 65.804 4.269
171	10.134 131.390 0.237	4.618 103.813 6.345	4.618 103.813 4.673	3.644 66.939 4.322
171		4.664 105.109 6.452	4.664 105.109 4.741	3.688 68.075 4.374
172	10.667 132.801 6.452 10.909 133.506 6.560	4.709 106.404 6.560	4.709 106.404 4.808	3.732 69.210 4.426
	11.150 134.211 6.668	4.754 107.700 6.668	4.754 107.700 4.876	3.776 70.345 4.479
174 175			4.799 108.995 4.944	
	11.392 134.917 6.776 11 439 137 703 6 910	4.799 108.995 6.776		3.821 71.481 4.531
176	11.439 137.703 6.910 11 486 140 400 7 045	4.858 110.733 6.910 4.917 112.471 7.045	4.858 110.733 5.057 4.917 112.471 5.171	3.856 73.077 4.626
177	11.486 140.490 7.045 11 533 143 276 7 170			3.891 74.674 4.722
178	11.533 143.276 7.179	4.977 114.209 7.179	4.977 114.209 5.284	3.927 76.271 4.817
179	11.581 146.063 7.313	5.036 115.946 7.313	5.036 115.946 5.398	3.962 77.867 4.912
180	11.628 148.849 7.447	5.095 117.684 7.447	5.095 117.684 5.511	3.997 79.464 5.008
181	11.671 154.282 7.621	5.158 119.775 7.621	5.158 119.775 5.641	4.024 81.282 5.111
182	11.715 159.715 7.795	5.221 121.866 7.795	5.221 121.866 5.770	4.050 83.100 5.214
183	11.759 165.147 7.969	5.284 123.956 7.969	5.284 123.956 5.900	4.077 84.919 5.318
184	11.803 170.580 8.143	5.347 126.047 8.143	5.347 126.047 6.029	4.104 86.737 5.421
185	11.846 176.013 8.318	5.411 128.138 8.318	5.411 128.138 6.159	4.131 88.555 5.524
186	11.887 179.970 8.499	5.428 129.673 8.499	5.428 129.673 6.285	4.154 90.333 5.656
187	11.928 183.927 8.681	5.446 131.209 8.681	5.446 131.209 6.411	4.178 92.110 5.787
188	11.969 187.884 8.862	5.463 132.745 8.862	5.463 132.745 6.537	4.202 93.888 5.919
189	12.010 191.841 9.043	5.481 134.281 9.043	5.481 134.281 6.663	4.225 95.665 6.050
190		5.499 135.816 9.225	5.499 135.816 6.789	4.249 97.442 6.182
191		5.561 137.198 9.386	5.561 137.198 6.875	4.285 98.856 6.266
192	12.128 199.584 9.547	5.623 138.580 9.547	5.623 138.580 6.961	4.321 100.271 6.350
193	12.166 201.476 9.708	5.686 139.961 9.708	5.686 139.961 7.047	4.357 101.685 6.435
194	12.205 203.369 9.869	5.748 141.343 9.869	5.748 141.343 7.133	4.393 103.099 6.519
195	12.243 205.262 10.030	5.810 142.724 10.030	5.810 142.724 7.219	4.430 104.513 6.603
196	12.281 208.341 10.188	5.828 144.052 10.188	5.828 144.052 7.346	4.460 106.134 6.706
197	12.319 211.419 10.346	•••••••••••••••••••••••••••••••••••••••	5.845 145.381 7.473	4.490 107.755 6.810
198	12.357 214.498 10.504		5.863 146.709 7.600	4.520 109.376 6.913
199	12.395 217.577 10.662		5.880 148.037 7.727	4.550 110.997 7.017
200	12.433 220.656 10.820		5.898 149.365 7.853	4.580 112.617 7.120
201	12.509 221.810 10.948	5.942 150.214 10.948	5.942 150.214 7.929	4.623 113.207 7.195
202	12.585 222.965 11.075		5.986 151.063 8.005	4.666 113.796 7.270
203	12.661 224.119 11.203	6.029 151.912 11.203	6.029 151.912 8.080	4.709 114.385 7.345

204	12.738 225.274 11.330	6.073 152.760 11.330	6.073 152.760 8.156	4.752 114.974 7.419
205	12.814 226.429 11.458	6.117 153.609 11.458	6.117 153.609 8.232	4.795 115.563 7.494
206	12.891 228.364 11.530	6.174 154.888 11.530	6.174 154.888 8.295	4.848 116.847 7.544
207	12.969 230.299 11.601	6.231 156.166 11.601	6.231 156.166 8.357	4.901 118.131 7.594
208	13.046 232.235 11.673	6.288 157.445 11.673	6.288 157.445 8.420	4.955 119.415 7.644
209	13.124 234.170 11.745	6.345 158.724 11.745	6.345 158.724 8.483	5.008 120.699 7.694
210	13.201 236.105 11.817	6.401 160.002 11.817	6.401 160.002 8.545	5.061 121.983 7.744
211	13.233 239.385 11.984	6.451 161.606 11.984	6.451 161.606 8.670	5.090 123.498 7.846
212	13.264 242.664 12.152	6.500 163.210 12.152	6.500 163.210 8.794	5.119 125.012 7.948
213	13.296 245.943 12.319	6.550 164.814 12.319	6.550 164.814 8.919	5.147 126.526 8.051
214	13.328 249.223 12.486	6.599 166.418 12.486	6.599 166.418 9.043	5.176 128.040 8.153
215	13.359 252.502 12.653	6.649 168.022 12.653	6.649 168.022 9.168	5.204 129.554 8.255
216	13.423 253.243 12.780	6.693 168.948 12.780	6.693 168.948 9.251	5.240 130.345 8.328
217	13.487 253.983 12.906	6.737 169.874 12.906	6.737 169.874 9.334	5.275 131.136 8.400
218	13.551 254.724 13.032	6.782 170.800 13.032	6.782 170.800 9.417	5.310 131.928 8.472
219	13.615 255.464 13.159	6.826 171.726 13.159	6.826 171.726 9.500	5.345 132.719 8.545
220	13.679 256.204 13.285	6.870 172.653 13.285	6.870 172.653 9.584	5.380 133.510 8.617
221	13.852 256.417 13.314	6.946 173.200 13.314	6.946 173.200 9.598	5.436 133.899 8.630
222	14.025 256.629 13.343	7.022 173.748 13.343	7.022 173.748 9.612	5.492 134.287 8.642
223	14.198 256.841 13.371	7.098 174.295 13.371	7.098 174.295 9.627	5.548 134.676 8.655
224	14.371 257.053 13.400	7.173 174.843 13.400	7.173 174.843 9.641	5.604 135.064 8.667
225	14.544 257.265 13.429	7.249 175.391 13.429	7.249 175.391 9.655	5.660 135.453 8.680
226	14.737 257.645 13.440	7.334 175.611 13.440	7.334 175.611 9.664	5.699 135.633 8.688
227	14.929 258.025 13.452	7.419 175.831 13.452	7.419 175.831 9.674	5.738 135.814 8.696
228	15.122 258.405 13.464	7.504 176.051 13.464	7.504 176.051 9.683	5.776 135.995 8.704
229	15.315 258.785 13.475	7.589 176.271 13.475	7.589 176.271 9.692	5.815 136.176 8.712
230	15.507 259.165 13.487	7.674 176.491 13.487	7.674 176.491 9.701	5.854 136.356 8.720
231	15.616 259.629 13.498	7.710 176.612 13.498	7.710 176.612 9.710	5.875 136.581 8.727
232	15.725 260.092 13.508	7.746 176.732 13.508	7.746 176.732 9.719	5.897 136.806 8.733
233	15.834 260.556 13.519	7.782 176.853 13.519	7.782 176.853 9.728	5.918 137.031 8.740
234	15.944 261.020 13.530	7.818 176.974 13.530		5.940 137.256 8.746
235	16.053 261.484 13.540	7.853 177.095 13.540		5.961 137.482 8.753
236	16.085 261.890 13.551	7.867 177.463 13.551	7.867 177.463 9.754	5.977 137.680 8.760
237	16.117 262.296 13.561	7.881 177.830 13.561	7.881 177.830 9.761	5.994 137.879 8.767
238	16.149 262.701 13.572	7.894 178.198 13.572	7.894 178.198 9.769	6.010 138.078 8.774
239	16.181 263.107 13.582	7.908 178.566 13.582	7.908 178.566 9.777	6.026 138.277 8.781
240	16.214 263.513 13.592	7.922 178.933 13.592	7.922 178.933 9.785	6.042 138.476 8.788
Appendix C

Fast Pass IM240 Standards Developed for Wisconsin

Fast Pass IM240 Standards Developed for Wisconsin

Wisconsin requested EPA provide fast-pass cutpoints for final and intermediate standards. A method is outlined below. This was applied only to the Appendix. A fast-pass cutpoints but could be used on others also.

1) A scale factor for each pollutant at each second is defined. This was done to calculate the cutpoint at second i for each pollutant at each standard.

For example: HC Scale Factor for the 0.8 cutpoint

FPHC Scale Factor = [HC(0.8)Fast Pass Cutpoint at t= i] / [HC(0.8) Fast Pass Cutpoint at t=239]

2) The ratio of the Fast Pass cutpoint at t=239 to the distance traveled (1.973 mi) was found. This was done so the new fast-pass cut points could be scaled to the new full 240 second standard

For HC (0.8g/mi):

FPHC 239 =	1.615	g
Distance =	1.973	mi
FPHC 239 g/mi =	0.81855	
% above 0.8 g/mi standard	1 = (0.818	8-0.8)/0.8*100 = 2.2%

For new HC standard (0.6 g/mi):

(FPHC 239 g/mi - 0.6)/0.6 * 100 = 2.2%

(This provides the same 2.2% overshoot as the phase-in fast-pass standards.)

FPHC 239 g/mi = 0.6132g/mi FPHC 239 g = 1.2098

3) The new fast pass standards will then be calculated as:

HC(0.6)FP = FP(0.6)239 * HCSF(0.8)i

t	HC(0.8) g	FPHC SF	HC(0.6) g
30	0.124	0.0768	0.0929

31	0.126	0.0780	0.0944
238 239	1.614 1.615	0.9994 1.0000	1.2091 1.2098

4) For Phase 2 cut points, where needed:

Take the old standard, for example, FPHC Phase 2 = 0.5 g/mi

The distance traveled from second 108 to second 239 is 1.359 mi

The old FPHC 239 cutpoint is 0.716 g

In terms of g/mi this is 0.716/1.359 = 0.527 g/mi

The delta between this value and the actual standard is: (0.527-0.5) = 0.027 g/mi

The new FPHC 239 g/mi cutpoint is: 0.4 + 0.027 = 0.427 g/mi . In terms of g, this is FPHC 239 g/mi * 1.359 mi = 0.580 g

The Scale Factor is calculated as before for each second of the test, and the Phase 2 cutpoint at each second is calculated by multiplying this Scale Factor times the new FP cutpoint in g at 239. In this case, that new FP cutpoint would be 0.580 * Scale Factor for each second.

			Hydroca	arbon(g)	1				Carbon M		Oxid	es of Nitro	gen (g)		
	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2	Composite	Phase 2	Composit	Composite	Composite		
Sec	(0.6)	(0.4)	(0.8)	(0.5)	(1.1)	(0.7)	(10.0)	(0.8)	(15.0)	(12.0)	(20.0)	(16.0)	e (1.5)	(2.0)	(2.5)
30	0.093	n/a	0.124	n/a	0.226	n/a	0.462	n/a	0.693	n/a	1.502	n/a	0.125	0.167	0.262
31	0.095	n/a	0.126	n/a	0.232	n/a	0.515	n/a	0.773	n/a	1.546	n/a	0.133	0.177	0.275
32	0.097	n/a	0.129	n/a	0.237	n/a	0.558	n/a	0.837	n/a	1.568	n/a	0.141	0.188	0.301
33	0.101	n/a	0.135	n/a	0.241	n/a	0.567	n/a	0.851	n/a	1.582	n/a	0.161	0.214	0.317
34	0.105	n/a	0.140	n/a	0.246	n/a	0.569	n/a	0.853	n/a	1.593	n/a	0.174	0.232	0.327
35	0.110	n/a	0.146	n/a	0.254	n/a	0.571	n/a	0.857	n/a	1.602	n/a	0.180	0.240	0.330
36	0.113	n/a	0.150	n/a	0.259	n/a	0.600	n/a	0.900	n/a	1.621	n/a	0.182	0.243	0.332
37	0.115	n/a	0.153	n/a	0.269	n/a	0.640	n/a	0.960	n/a	1.631	n/a	0.184	0.245	0.334
38	0.117	n/a	0.156	n/a	0.272	n/a	0.689	n/a	1.034	n/a	1.702	n/a	0.185	0.246	0.336
39	0.120	n/a	0.160	n/a	0.273	n/a	0.713	n/a	1.070	n/a	1.784	n/a	0.185	0.246	0.337
40	0.124	n/a	0.165	n/a	0.287	n/a	0.717	n/a	1.076	n/a	1.879	n/a	0.188	0.250	0.354
41	0.127	n/a	0.169	n/a	0.293	n/a	0.722	n/a	1.083	n/a	2.162	n/a	0.195	0.260	0.366
42	0.129	n/a	0.172	n/a	0.300	n/a	0.735	n/a	1.102	n/a	2.307	n/a	0.208	0.277	0.410
43	0.130	n/a	0.173	n/a	0.314	n/a	0.741	n/a	1.111	n/a	2.343	n/a	0.233	0.311	0.414
44	0.133	n/a	0.177	n/a	0.330	n/a	0.743	n/a	1.114	n/a	2.376	n/a	0.246	0.328	0.438
45	0.148	n/a	0.197	n/a	0.345	n/a	0.771	n/a	1.157	n/a	2.406	n/a	0.257	0.343	0.477
46	0.150	n/a	0.200	n/a	0.357	n/a	0.896	n/a	1.344	n/a	2.433	n/a	0.269	0.359	0.506
47	0.156	n/a	0.208	n/a	0.374	n/a	0.988	n/a	1.482	n/a	2.458	n/a	0.280	0.373	0.518
48	0.166	n/a	0.221	n/a	0.388	n/a	1.020	n/a	1.530	n/a	2.483	n/a	0.287	0.383	0.522
49	0.174	n/a	0.232	n/a	0.398	n/a	1.028	n/a	1.542	n/a	2.774	n/a	0.289	0.385	0.526
50	0.176	n/a	0.235	n/a	0.407	n/a	1.035	n/a	1.553	n/a	2.844	n/a	0.300	0.400	0.554
51	0.179	n/a	0.238	n/a	0.416	n/a	1.047	n/a	1.571	n/a	2.900	n/a	0.308	0.410	0.574
52	0.180	n/a	0.240	n/a	0.426	n/a	1.063	n/a	1.595	n/a	2.936	n/a	0.326	0.434	0.587
53	0.182	n/a	0.242	n/a	0.433	n/a	1.089	n/a	1.633	n/a	3.133	n/a	0.348	0.464	0.601
54	0.185	n/a	0.242	n/a	0.438	n/a	1.123	n/a	1.685	n/a	3.304	n/a	0.354	0.472	0.615
55	0.185	n/a	0.240	n/a	0.435	n/a	1.125	n/a	1.689	n/a	3.407	n/a	0.360	0.472	0.629
56	0.187	n/a	0.249	n/a	0.452	n/a	1.120	n/a	1.693	n/a	3.456	n/a	0.368	0.491	0.643
57	0.135	n/a	0.252	n/a	0.458	n/a	1.123	n/a	1.093	n/a	3.480	n/a	0.305	0.500	0.667
58	0.190	n/a	0.201	n/a	0.463	n/a	1.135	n/a	1.700	n/a	3.518	n/a	0.380	0.506	0.678
59	0.203	n/a	0.271	n/a	0.405	n/a	1.145	n/a	1.852	n/a	3.560	n/a	0.382	0.509	0.683
<u>60</u>	0.207	n/a	0.278	n/a	0.471	••••••	1.233	n/a	1.872	n/a	3.593	n/a	0.384	0.512	0.686
61	0.209	n/a	0.278	n/a	0.492	n/a n/a	1.248	n/a	1.872	n/a	3.628	n/a	0.387	0.512	0.693
62	0.210	n/a	0.280	n/a	0.495	n/a	1.248	n/a	1.872	n/a	3.641	n/a	0.387	0.510	0.699
63	0.212	n/a	0.283	n/a	0.501	n/a	1.243	n/a	1.900	n/a	3.655	n/a	0.392	0.523	0.703
64	0.212	n/a	0.283	n/a	0.501	n/a	1.207	n/a	1.900	n/a	3.680	n/a	0.392	0.529	0.703
65	0.213				••••••	••••••	•								
		n/a	0.285	n/a	0.512	n/a	1.296	n/a	1.944	n/a	3.700	n/a	0.400	0.533	0.711
66 67	0.215	n/a	0.286	n/a	0.520	n/a	1.333	n/a	2.000	n/a	3.728	n/a	0.401	0.535	0.716
67	0.216	n/a	0.288	n/a	0.527	n/a	1.373	n/a	2.060	n/a	3.857	n/a	0.405	0.540	0.721
68	0.218	n/a	0.291	n/a	0.539	n/a	1.376	n/a	2.064	n/a	3.894	n/a	0.413	0.551	0.726
69 70	0.221	n/a	0.294	n/a	0.545	n/a	1.384	n/a	2.076	n/a	3.943	n/a	0.422	0.563	0.742
70	0.222	n/a	0.296	n/a	0.551	n/a	1.403	n/a	2.104	n/a	3.983	n/a	0.431	0.575	0.759
71	0.224	n/a	0.298	n/a	0.556	n/a	1.411	n/a	2.117	n/a	4.009	n/a	0.441	0.588	0.773
72	0.225	n/a	0.300	n/a	0.559	n/a	1.417	n/a	2.125	n/a	4.023	n/a	0.450	0.600	0.784
73	0.227	n/a	0.302	n/a	0.566	n/a	1.420	n/a	2.130	n/a	4.023	n/a	0.452	0.603	0.790
74	0.228	n/a	0.304	n/a	0.578	n/a	1.425	n/a	2.138	n/a	4.053	n/a	0.453	0.604	0.794
75	0.230	n/a	0.307	n/a	0.589	n/a	1.435	n/a	2.152	n/a	4.063	n/a	0.460	0.613	0.799
76	0.231	n/a	0.308	n/a	0.597	n/a	1.447	n/a	2.170	n/a	4.077	n/a	0.468	0.624	0.809
77	0.231	n/a	0.308	n/a	0.604	n/a	1.459	n/a	2.188	n/a	4.225	n/a	0.485	0.646	0.821

78	0.231	n/a	0.308	n/a	0.611	n/a	1.467	n/a	2.200	n/a	4.243	n/a	0.488	0.651	0.833
79	0.236	n/a	0.314	n/a	0.620	n/a	1.475	n/a	2.212	n/a	4.260	n/a	0.494	0.659	0.839
80	0.240	n/a	0.320	n/a	0.624	n/a	1.475	n/a	2.212	n/a	4.282	n/a	0.505	0.673	0.844
81	0.243	n/a	0.324	n/a	0.628	n/a	1.481	n/a	2.221	n/a	4.322	n/a	0.522	0.696	0.857
82	0.245	n/a	0.327	n/a	0.632	n/a	1.481	n/a	2.222	n/a	4.398	n/a	0.530	0.706	0.870
83	0.247	n/a	0.329	n/a	0.636	n/a	1.485	n/a	2.227	n/a	4.482	n/a	0.536	0.715	0.883
84	0.250	n/a	0.333	n/a	0.642	n/a	1.491	n/a	2.236	n/a	4.515	n/a	0.543	0.724	0.894
85	0.252	n/a	0.336	n/a	0.646	n/a	1.495	n/a	2.243	n/a	4.518	n/a	0.553	0.737	0.902
86	0.254	n/a	0.339	n/a	0.650	n/a	1.508	n/a	2.262	n/a	4.520	n/a	0.560	0.747	0.907
87	0.257	n/a	0.343	n/a	0.654	n/a	1.514	n/a	2.271	n/a	4.522	n/a	0.561	0.748	0.910
88	0.260	n/a	0.347	n/a	0.657	n/a	1.523	n/a	2.284	n/a	4.522	n/a	0.561	0.748	0.912
89	0.263	n/a	0.350	n/a	0.661	n/a	1.533	n/a	2.299	n/a	4.523	n/a	0.561	0.748	0.913
90	0.267	n/a	0.356	n/a	0.664	n/a	1.539	n/a	2.308	n/a	4.526	n/a	0.561	0.748	0.914
91	0.269	n/a	0.358	n/a	0.666	n/a	1.551	n/a	2.326	n/a	4.527	n/a	0.561	0.748	0.915
92	0.270	n/a	0.360	n/a	0.668	n/a	1.553	n/a	2.330	n/a	4.527	n/a	0.561	0.748	0.916
93	0.272	n/a	0.363	n/a	0.670	n/a	1.554	n/a	2.331	n/a	4.528	n/a	0.561	0.748	0.917
94	0.275	n/a	0.367	n/a	0.673	n/a	1.563	n/a	2.344	n/a	4.528	n/a	0.561	0.748	0.918
95	0.278	n/a	0.370	n/a	0.678	n/a	1.565	n/a	2.347	n/a	4.528	n/a	0.561	0.748	0.919
96	0.279	n/a	0.372	n/a	0.686	n/a	1.570	n/a	2.355	n/a	4.529	n/a	0.561	0.748	0.920
97	0.282	n/a	0.376	n/a	0.696	n/a	1.597	n/a	2.395	n/a	4.575	n/a	0.561	0.748	0.921
98	0.291	n/a	0.388	n/a	0.707	n/a	1.634	n/a	2.451	n/a	4.703	n/a	0.561	0.748	0.922
99	0.297	n/a	0.396	n/a	0.718	n/a	1.672	n/a	2.508	n/a	4.805	n/a	0.563	0.751	0.924
100	0.304	n/a	0.405	n/a	0.727	n/a	1.727	n/a	2.590	n/a	4.886	n/a	0.573	0.764	0.929
101	0.308	n/a	0.410	n/a	0.743	n/a	1.773	n/a	2.660	n/a	4.957	n/a	0.592	0.789	0.941
102	0.308	n/a	0.411	n/a	0.754	n/a	1.833	n/a	2.749	n/a	5.104	n/a	0.617	0.822	0.970
103	0.309	n/a	0.412	n/a	0.766	n/a	1.942	n/a	2.913	n/a	5.340	n/a	0.650	0.867	1.027
104	0.310	n/a	0.413	n/a	0.782	n/a	2.108	n/a	3.162	n/a	5.496	n/a	0.679	0.905	1.093
105	0.316	n/a	0.421	n/a	0.798	n/a	2.113	n/a	3.170	n/a	5.625	n/a	0.694	0.925	1.155
106	0.321	n/a	0.428	n/a	0.813	n/a	2.131	n/a	3.197	n/a	5.815	n/a	0.716	0.955	1.234
107	0.323	n/a	0.430	n/a	0.824	n/a	2.192	n/a	3.288	n/a	6.473	n/a	0.739	0.985	1.275
108	0.341	n/a	0.455	n/a	0.853	n/a	2.279	n/a	3.419	n/a	7.037	n/a	0.745	0.993	1.305
109	0.344	0.012	0.459	0.015	0.868	0.037	2.391	0.115	3.587	0.168	7.419	0.246	0.746	0.995	1.320
110	0.347	0.014	0.462	0.017	0.877	0.044	2.397	0.119	3.595	0.173	7.643	0.257	0.747	0.996	1.332
111	0.348	0.017	0.464	0.021	0.885	0.049	2.427	0.163	3.640	0.237	7.759	0.286	0.758	1.010	1.346
112	0.350	0.019	0.466	0.024	0.890	0.052	2.493	0.183	3.740	0.266	7.824	0.379	0.771	1.028	1.358
113	0.351	0.019	0.468	0.024	0.896	0.057	2.579	0.192	3.868	0.280	7.889	0.425	0.776	1.034	1.378
114	0.353		0.471	0.025		0.060	2.585	0.200	3.877		7.960			1.044	1.406
115	0.366	0.021	0.488	0.026	0.919	0.067	2.623	0.216	3.934	0.314	8.024 8.076	0.477	0.794	1.059	1.426
116 117	0.385 0.404	0.023	0.513	0.029	0.944	0.076 0.077	2.677 2.707	0.227	4.015	0.331		0.494	0.806 0.810	1.075 1.080	1.438
117	0.404	0.026	0.538 0.561	0.032	0.954 0.963	0.077	2.707	0.237	4.061 4.063	0.345	8.111 8.130	0.504 0.512	0.810	1.080	1.448 1.460
110	0.421	0.028	0.501	0.035	0.963	0.078	2.709	0.240	4.005	0.350	8.130	0.512	0.810	1.080	1.460
119	0.435	0.028	0.577	0.035	0.964	0.088	2.719	0.245	4.079	0.350	8.211	0.519	0.811	1.091	1.462
120	0.435	0.029	0.580	0.030	0.907	0.000	2.700	0.252	4.140	0.388	8.478	0.529	0.822	1.091	1.407
121	0.440	0.031	0.594	0.038	0.973	0.091	2.790	0.207	4.105	0.388	8.548	0.529	0.822	1.111	1.470
122	0.440	0.032	0.594	0.040	0.982	0.094	2.199	0.280	4.205	0.407	8.561	0.530	0.833	1.111	1.505
123	0.458	0.033	0.610	0.041	1.000	0.090	2.803	0.330	4.203	0.480	8.568	0.531	0.851	1.135	1.505
124	0.450	0.034	0.615	0.042	1.000	0.101	2.808	0.348	4.232	0.506	8.572	0.532	0.854	1.133	1.546
125	0.468	0.034	0.624	0.042	1.010	0.101	2.865	0.346	4.298	0.518	8.584	0.548	0.854	1.139	1.569
120	0.400	0.034	0.628	0.042	1.013	0.105	2.896	0.359	4.344	0.522	8.592	0.610	0.854	1.139	1.586
127	0.474	0.037	0.632	0.045	1.025	0.105	2.907	0.361	4.361	0.525	8.596	0.614	0.854	1.139	1.596
120	0.474	0.037	0.637	0.040	1.020	0.107	2.907	0.363	4.366	0.525	8.597	0.622	0.854	1.139	1.603
130	0.470	0.037	0.641	0.040	1.031	0.111	2.911	0.364	4.369	0.520	8.601	0.631	0.854	1.139	1.605
130	0.401	0.040	0.041	0.042	1.0.34	V.111	L	0.304	т.303	0.550	0.001	0.031	0.034	1.137	1.005

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.854 0.854 0.854 0.854 0.854 0.870 0.881 0.887 0.898 0.917 0.941 0.954 0.965 0.978	1.139 1.139 1.139 1.139 1.139 1.139 1.160 1.174 1.183 1.197 1.223 1.255 1.272	1.606 1.607 1.607 1.608 1.614 1.614 1.616 1.631 1.643 1.656 1.673 1.703
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.854 0.854 0.870 0.881 0.887 0.898 0.917 0.941 0.954 0.965	1.139 1.139 1.139 1.160 1.174 1.183 1.197 1.223 1.255	1.607 1.608 1.614 1.616 1.631 1.643 1.656 1.673
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.854 0.870 0.881 0.887 0.898 0.917 0.941 0.954 0.965	1.139 1.139 1.160 1.174 1.183 1.197 1.223 1.255	1.608 1.614 1.616 1.631 1.643 1.656 1.673
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.870 0.881 0.887 0.898 0.917 0.941 0.954 0.965	1.160 1.174 1.183 1.197 1.223 1.255	1.616 1.631 1.643 1.656 1.673
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.881 0.887 0.898 0.917 0.941 0.954 0.965	1.174 1.183 1.197 1.223 1.255	1.631 1.643 1.656 1.673
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.887 0.898 0.917 0.941 0.954 0.965	1.183 1.197 1.223 1.255	1.643 1.656 1.673
1390.5010.0480.6680.0591.0870.1373.0350.4554.5530.6629.3890.8041400.5030.0490.6700.0611.1490.1403.0360.4694.5540.6839.4930.8101410.5040.0490.6720.0611.1570.1413.0360.4784.5540.6969.5830.8151420.5060.0490.6750.0611.1650.1433.0360.4864.5540.7089.6260.818	0.898 0.917 0.941 0.954 0.965	1.197 1.223 1.255	1.656 1.673
1400.5030.0490.6700.0611.1490.1403.0360.4694.5540.6839.4930.8101410.5040.0490.6720.0611.1570.1413.0360.4784.5540.6969.5830.8151420.5060.0490.6750.0611.1650.1433.0360.4864.5540.7089.6260.818	0.917 0.941 0.954 0.965	1.197 1.223 1.255	1.673
141 0.504 0.049 0.672 0.061 1.157 0.141 3.036 0.478 4.554 0.696 9.583 0.815 142 0.506 0.049 0.675 0.061 1.165 0.143 3.036 0.486 4.554 0.696 9.583 0.815	0.941 0.954 0.965	1.255	
142 0.506 0.049 0.675 0.061 1.165 0.143 3.036 0.486 4.554 0.708 9.626 0.818	0.954 0.965		1.703
	0.965	1.272	
			1.739
[143] 0.509 0.051 0.678 0.063 1.171 0.145 3.036 0.495 4.554 0.721 9.669 0.821	0.978	1.286	1.767
144 0.511 0.052 0.681 0.064 1.176 0.147 3.036 0.508 4.554 0.739 9.716 0.825		1.304	1.774
145 0.513 0.053 0.684 0.065 1.183 0.152 3.036 0.510 4.554 0.742 9.763 0.840	0.980	1.307	1.785
146 0.515 0.053 0.686 0.066 1.186 0.154 3.036 0.510 4.554 0.743 9.809 0.847	0.984	1.312	1.806
147 0.516 0.054 0.688 0.067 1.188 0.156 3.036 0.512 4.554 0.745 9.852 0.855	0.988	1.317	1.830
148 0.518 0.055 0.690 0.068 1.190 0.157 3.036 0.514 4.554 0.748 9.885 0.865	0.991	1.321	1.844
149 0.519 0.056 0.692 0.069 1.194 0.158 3.036 0.516 4.554 0.751 9.932 0.874	0.994	1.325	1.845
150 0.521 0.057 0.694 0.070 1.206 0.159 3.036 0.524 4.554 0.762 9.986 0.891	0.996	1.328	1.846
151 0.522 0.058 0.696 0.071 1.219 0.160 3.037 0.542 4.556 0.789 10.039 0.914	0.999	1.332	1.852
152 0.524 0.058 0.698 0.072 1.230 0.161 3.037 0.543 4.556 0.790 10.072 0.929	1.004	1.338	1.868
153 0.525 0.059 0.700 0.073 1.236 0.162 3.043 0.546 4.565 0.794 10.090 0.937	1.008	1.344	1.877
154 0.527 0.059 0.702 0.073 1.240 0.164 3.075 0.549 4.612 0.799 10.105 0.942	1.013	1.350	1.879
155 0.528 0.060 0.704 0.074 1.249 0.167 3.223 0.553 4.834 0.805 10.146 0.949	1.018	1.357	1.886
156 0.530 0.062 0.706 0.077 1.251 0.169 3.801 0.578 5.702 0.842 10.245 1.375	1.024	1.365	1.900
157 0.531 0.064 0.708 0.079 1.252 0.177 3.894 0.680 5.841 0.990 10.397 1.576	1.034	1.379	1.910
158 0.533 0.066 0.710 0.082 1.259 0.185 4.113 0.713 6.170 1.038 10.923 1.943	1.061	1.414	1.936
159 0.534 0.066 0.712 0.082 1.281 0.190 4.447 0.932 6.670 1.357 11.970 2.820	1.100	1.466	1.954
160 0.537 0.070 0.716 0.086 1.304 0.194 4.950 1.000 7.425 1.455 13.421 3.281	1.136	1.514	1.986
161 0.563 0.077 0.750 0.095 1.320 0.200 5.586 1.062 8.379 1.546 15.289 3.483	1.169	1.559	2.050
162 0.588 0.087 0.784 0.107 1.331 0.207 6.432 1.253 9.648 1.824 15.912 3.620	1.193	1.591	2.131
163 0.604 0.093 0.805 0.115 1.343 0.215 7.279 1.887 10.918 2.746 16.530 4.168	1.231	1.641	2.235
164 0.630 0.099 0.840 0.122 1.383 0.231 8.105 2.111 12.157 3.073 17.622 4.338	1.289	1.719	2.320
165 0.640 0.103 0.853 0.127 1.405 0.257 8.487 2.496 12.731 3.633 18.366 4.682	1.333	1.777	2.395
166 0.656 0.129 0.874 0.159 1.425 0.289 8.554 3.095 12.831 4.505 19.869 5.633	1.374	1.832	2.488
167 0.677 0.151 0.903 0.186 1.445 0.298 8.595 3.402 12.892 4.952 20.711 6.137	1.439	1.919	2.563
168 0.683 0.153 0.910 0.189 1.465 0.302 8.621 3.610 12.932 5.254 22.319 6.853	1.479	1.972	2.645
169 0.686 0.162 0.914 0.200 1.483 0.312 9.135 3.937 13.702 5.730 23.751 7.136	1.510	2.013	2.746
170 0.687 0.178 0.916 0.220 1.500 0.321 9.426 4.157 14.139 6.051 24.842 7.320	1.575	2.100	2.778
171 0.689 0.191 0.919 0.236 1.527 0.333 9.976 4.351 14.964 6.333 25.410 7.685	1.650	2.200	2.792
172 0.698 0.200 0.931 0.247 1.545 0.361 10.469 4.459 15.704 6.490 25.798 8.052	1.688	2.251	2.810
173 0.711 0.208 0.948 0.257 1.582 0.383 10.835 4.669 16.253 6.796 26.122 8.344	1.703	2.270	2.847
174 0.737 0.216 0.983 0.267 1.597 0.406 11.271 4.950 16.907 7.205 26.353 8.602	1.726	2.301	2.874
175 0.764 0.229 1.018 0.283 1.610 0.424 11.770 5.600 17.655 8.151 26.638 8.898	1.739	2.318	2.905
176 0.770 0.239 1.027 0.295 1.622 0.434 12.013 5.654 18.020 8.230 27.219 9.251	1.751	2.335	2.950
177 0.776 0.253 1.035 0.312 1.635 0.475 12.233 5.898 18.349 8.584 27.279 10.253	1.762	2.349	3.001
178 0.788 0.258 1.051 0.318 1.652 0.490 12.447 6.046 18.671 8.800 27.320 10.828	1.790	2.387	3.047
179 0.806 0.262 1.074 0.323 1.670 0.495 12.648 6.078 18.972 8.847 27.352 10.933	1.817	2.423	3.104
180 0.813 0.273 1.084 0.337 1.689 0.507 12.819 6.124 19.228 8.913 27.822 11.060	1.847	2.462	3.173
181 0.824 0.280 1.099 0.345 1.709 0.514 13.415 6.267 20.123 9.122 28.763 11.188	1.877	2.503	3.238
182 0.841 0.284 1.121 0.350 1.727 0.524 13.603 6.549 20.405 9.532 29.402 11.345	1.909	2.545	3.302
183 0.849 0.291 1.132 0.359 1.738 0.535 13.836 7.046 20.754 10.256 29.971 11.733	1.940	2.586	3.372

184	0.864	0.314	1.152	0.387	1.755	0.547	14.456	7.463	21.684	10.862	30.276	12.598	1.970	2.627	3.452
185	0.871	0.322	1.161	0.398	1.778	0.560	14.637	7.555	21.955	10.996	30.988	12.953	2.005	2.673	3.545
186	0.876	0.324	1.168	0.400	1.795	0.574	15.100	7.699	22.650	11.206	31.095	13.213	2.062	2.749	3.648
187	0.881	0.326	1.175	0.402	1.808	0.585	15.326	7.911	22.989	11.514	31.314	14.131	2.103	2.804	3.701
188	0.886	0.328	1.181	0.405	1.820	0.589	15.690	8.172	23.535	11.894	31.833	14.839	2.138	2.851	3.759
189	0.891	0.339	1.188	0.418	1.825	0.589	15.917	8.258	23.876	12.019	32.239	15.137	2.171	2.894	3.821
190	0.902	0.348	1.203	0.429	1.827	0.598	16.012	8.361	24.018	12.170	32.547	15.138	2.198	2.931	3.870
191	0.914	0.358	1.219	0.442	1.829	0.607	16.309	8.600	24.464	12.517	32.855	15.141	2.228	2.971	3.892
192	0.925	0.370	1.233	0.457	1.834	0.617	16.457	8.655	24.685	12.598	33.153	15.595	2.265	3.020	3.914
193	0.938	0.383	1.251	0.473	1.847	0.621	16.621	8.674	24.931	12.625	33.444	15.658	2.308	3.077	3.955
194	0.941	0.395	1.255	0.487	1.862	0.629	16.792	8.693	25.188	12.653	33.482	15.704	2.349	3.132	3.997
195	0.944	0.406	1.258	0.501	1.876	0.638	16.979	8.778	25.468	12.777	33.516	15.729	2.389	3.185	4.035
196	0.949	0.413	1.265	0.510	1.891	0.649	17.085	8.867	25.627	12.906	33.549	16.058	2.414	3.219	4.089
197	0.960	0.415	1.280	0.512	1.906	0.664	17.164	8.924	25.746	12.989	33.653	16.987	2.451	3.268	4.146
198	0.970	0.416	1.293	0.514	1.920	0.679	17.233	8.973	25.850	13.060	33.973	17.064	2.474	3.299	4.206
199	0.976	0.418	1.301	0.516	1.933	0.693	17.316	9.045	25.974	13.165	34.159	17.073	2.513	3.350	4.243
200	0.985	0.420	1.313	0.518	1.945	0.706	17.427	9.098	26.141	13.242	34.191	17.153	2.555	3.406	4.295
201	0.993	0.427	1.324	0.527	1.953	0.719	17.483	9.215	26.225	13.412	34.250	17.332	2.600	3.466	4.351
202	0.999	0.438	1.332	0.540	1.959	0.726	17.559	9.386	26.338	13.662	34.469	17.406	2.623	3.497	4.398
203	1.006	0.443	1.341	0.547	1.977	0.737	17.698	9.463	26.547	13.773	34.716	17.641	2.636	3.514	4.410
204	1.018	0.448	1.357	0.553	1.991	0.745	17.879	9.579	26.818	13.942	34.969	17.922	2.638	3.517	4.419
205	1.031	0.453	1.375	0.559	2.011	0.752	18.035	9.680	27.052	14.090	35.144	18.484	2.639	3.519	4.426
206	1.044	0.456	1.392	0.563	2.037	0.800	18.262	9.773	27.393	14.224	35.418	18.553	2.642	3.523	4.429
207	1.056	0.459	1.408	0.567	2.058	0.805	18.334	9.911	27.501	14.426	35.766	18.658	2.659	3.545	4.453
208	1.067	0.463	1.422	0.571	2.079	0.817	18.421	9.961	27.632	14.498	35.949	18.953	2.678	3.570	4.486
209	1.075	0.466	1.433	0.575	2.089	0.836	18.535	10.152	27.803	14.776	36.010	19.266	2.700	3.600	4.542
210	1.082	0.469	1.443	0.579	2.097	0.839	18.635	10.242	27.953	14.907	36.548	19.309	2.714	3.619	4.598
211	1.090	0.482	1.453	0.595	2.109	0.846	18.803	10.248	28.205	14.916	37.179	19.731	2.729	3.639	4.638
212	1.097	0.490	1.463	0.605	2.123	0.866	19.029	10.315	28.543	15.014	37.651	19.902	2.765	3.686	4.715
213	1.101	0.497	1.468	0.614	2.138	0.879	19.331	10.458	28.997	15.221	38.041	20.012	2.799	3.732	4.774
214	1.103	0.504	1.470	0.622	2.150	0.882	19.333	10.630	29.000	15.472	38.591	20.260	2.843	3.791	4.829
215	1.106	0.508	1.474	0.627	2.158	0.891	19.337	10.687	29.005	15.555	38.852	20.739	2.875	3.833	4.872
216	1.109	0.517	1.478	0.638	2.165	0.905	19.387	10.754	29.081	15.652	38.861	21.346	2.918	3.890	4.931
217	1.111	0.521	1.481	0.643	2.171	0.917	19.521	10.971	29.281	15.969	38.926	21.810	2.949	3.932	4.960
218	1.113	0.521	1.484	0.643	2.178	0.918	19.655	11.012	29.483	16.028	39.194	22.001	2.970	3.960	4.963
219	1.115	0.523	1.487	0.645	2.185	0.919	19.823	11.250	29.734	16.375	39.474	22.290	2.998	3.997	4.965
220	1.118	0.527	1.490	0.651	2.192	0.941	19.869	11.327	29.803	16.487	39.668	22.324	3.010	4.013	4.968
221	1.120	0.531	1.493	0.655	2.195	0.952		11.353	29.821		39.781	22.343	3.026	4.035	4.971
222	1.128	0.537	1.504	0.663	2.200	0.957	19.898	11.390	29.847			22.522	3.029	4.038	4.974
223	1.142	0.544	1.522	0.671	2.205	0.963	19.908	11.463	29.862	16.684	39.954	22.661	3.038	4.050	4.977
224	1.160	0.547	1.547	0.675	2.208	0.970	19.915	11.511	29.873	16.755	39.984	22.666	3.050	4.066	4.979
225	1.162	0.554	1.549	0.684	2.212	0.975			30.008		39.989	22.667	3.053	4.070	4.980
226	1.172	0.562	1.562	0.694	2.214	0.979	20.084	11.546	30.126				3.054	4.072	4.981
227	1.181	0.568	1.574	0.701	2.216	0.985	20.085	11.587	30.127	16.865	39.990	22.669	3.054	4.072	4.982
228	1.184	0.569	1.579	0.702	2.217	0.988	20.085	11.652	30.127	16.960	39.990	22.670	3.055	4.073	4.983
229	1.188	0.574	1.584	0.708	2.218	0.992	20.139	11.652	30.208	16.960	39.991	22.671	3.055	4.073	4.984
230	1.192	0.574	1.589	0.708	2.219	0.995	20.209	11.654	30.314	16.962	40.012	22.671	3.055	4.073	4.985
231	1.193	0.574	1.590	0.709	2.221	0.996	20.215	11.672	30.323	16.988	40.061	22.672	3.055	4.073	4.986
232	1.197	0.575	1.596	0.710	2.223	0.996	20.217	11.729	30.325	17.072	40.116	22.673	3.056	4.074	4.987
233	1.199	0.575	1.598	0.710	2.225	0.996	20.245	11.744	30.368	17.094	40.249	22.673	3.056	4.074	4.988
234	1.203	0.576	1.604	0.711	2.227	0.997	20.274	11.806	30.411	17.184	40.253	22.673	3.056	4.075	4.989
235	1.208	0.577	1.610	0.712	2.228	0.997	20.277	11.808	30.416	17.187	40.290	22.674	3.056	4.075	4.990
236	1.209	0.577	1.612	0.712	2.228	0.999	20.285	11.809	30.428	17.188	40.385	22.675	3.057	4.076	4.991
s		•••••	•••••		•••••		••••••	•••••	•••••	•••••	•• •• • • • • • • • • • • • • • • • • •			•• •• •• •• •• •• •• •• •• •• ••	

237	1.210	0.577	1.613	0.712	2.229	1.001	20.287	11.810	30.430	17.189	40.488	22.675	3.057	4.076	4.992
238	1.211	0.578	1.614	0.713	2.230	1.004	20.301	11.845	30.452	17.241	40.720	22.675	3.057	4.076	4.993
239	1.211	0.580	1.615	0.716	2.231	1.007	20.325	11.934	30.488	17.370	40.763	22.677	3.057	4.076	4.994

Appendix D

Fast Pass IM240 Standards: Modal Regression Technique

Developed by Sierra Research Contract 68-C4-0056 Work Assignment 2-04

Fast Pass IM240 Standards: Modal Regression Technique

Sierra Research Contract 68-C4-0056 Work Assignment 2-04

Development of Fast-Pass Standards

This method differs from those presented in Appendices A, B, and C in that second-by-second standards are not used, rather the second-by-second emissions are used to project a final IM240 score which is then compared to the appropriate IM240 standard as listed on pages 1-4 of this document. A sample of the regression coefficients used to project the full IM240 scores are presented in this appendix. The complete set of coefficients, including an example calculation, can be downloaded from the EPA web site.

Full-duration, second-by-second IM240 data collected in the Arizona I/M program were used for this analysis. Nearly 110,000 individual tests were in the database used in the analysis, which is comprised of all full-duration IM240 tests conducted in Arizona from April 1995 through April 1997. Regression coefficients were generated separately for light-duty gasoline vehicles (i.e., passenger cars) and light-duty trucks for the following model year groups listed below.

- 1981 to 1984,
- 1985 to 1989, and
- 1990 and later.

Regression coefficients were developed for HC, CO, and NOx and for both the composite IM240 and for Phase 2 of the IM240 after dividing the IM240 drive trace into 24 separate modes. The Phase 2 regressions used mode 11 as the first mode and continued through mode 23. The composite IM240 regressions used modes 1 through 23. (Although the trace was divided into 24 modes, if a fast-pass decision is not made by mode 23, then the vehicle would run the full IM240. At that point, a pass/fail decision should be made on the actual IM240 score, not the predicted score.) Finally, it is recommended that the first mode at which a pass/fail decision should be made is mode 4 (which ends at second 32 of the IM240) for a composite IM240 prediction, or mode 13 (which ends at second 113 of the IM240) for a Phase 2 prediction.

The regression coefficients for a 0.8 g/mi HC composite IM240 cutpoint are given in this appendix, along with the coefficients for a 0.5 g/mi HC Phase 2 IM240 cutpoint. The full series of regression coefficients developed in this effort were provided to EPA electronically, and are available on the OMS web page.

Using the 2% Random Sample from the Arizona program (which consists of 26,000 records), pass/fail rates were calculated with the modal regression procedures outlined above as well as the current fast-pass cutpoint tables. This analysis was performed using the final IM240 HC, CO, and NOx standards, and the results are presented in Table D1.

As observed in Table D1, the revised fast-pass methodology results in a lower fraction of false passes than the current method, particularly for older cars. However, this improvement in failing vehicle identification is offset by a longer average test time for passing vehicles in the older model year groups. For newer vehicles (i.e., 1990 and later), the revised methodology results in significant improvements in average test time, without a significant increase in the fraction of false passes.

			Table D1			
Compar	rison of Curren			dologies Under t	he Final IM24	10 Standards
		(26	5,000 Vehicle S	Sample)		
Vehicle	Model	"True"	Current Fas	st-Pass	Revised Fa	st-Pass
Class	Year	Failure				
	Group	Rate ^a				
			Failure	Pass Time	Failure	Pass Time
			Rate	(seconds)	Rate	(seconds)
LDV	81 - 84	79%	76%	125	78%	157
	85 - 89	45%	41%	130	43%	121
	1990+	8%	7%	88	7%	57
LDT	81 - 84	62%	51%	71	60%	113
	85 - 89	42%	35%	70	40%	93
	1990+	9%	7%	60	7%	57

^a The "true" failure rate is based on full-duration IM240 test scores.

Composite IM240 HC Regression Coefficients Developed from Modal IM240 Data Analysis 1981-1984 Model Year Light-Duty Gasoline Vehicles 0.8 g/mi Cutpoint

				Regression Coefficients																					
Mode	RMS Error	Const	C1	C2	C3	C4	C5	C6	C7	C8	С9	C10	C11	C12	C13	C14	C15	C16	C17	C18	C19	C20	C21	C22	C23
M1	0.301	0.566	5.043																					•	
M2	0.253	0.378	0.187	2.802																				•	
M3	0.247	0.371	-0.383	2.022	2.586				•		•	•	•					•						•	
M4	0.232	0.337	-0.363	0.828	0.771	3.854			•		•	•	•					•							
M5	0.228	0.325	-0.454	1.046	-0.497	2.884	3.156		•		•	•	•					•							
M6	0.214	0.286	0.371	0.566	0.327	-0.040	1.592	4.850	•		•	•	•					•							
M7	0.202	0.274	0.697	0.468	0.136	-0.077	1.315	2.032	2.632		•	•	•			•		•							
M8	0.194	0.260	0.489	0.715	-0.044	-0.411	1.211	2.268	0.853	2.410	•	•	•			•		•							
M9	0.189	0.247	0.452	0.747	0.049	-0.370	1.228	2.028	0.757	0.664	2.993	•	•					•						•	
M10	0.185	0.242	0.163	0.947	-0.410	-0.223	0.801	1.855	0.909	0.463	2.017	2.189	•					•							
M11	0.182	0.236	-0.613	1.036	-0.076	-0.458	0.652	1.882	0.997	0.312	1.900	1.397	4.130					•							
M12	0.160	0.179	0.127	0.496	0.458	-0.049	0.861	0.657	0.532	0.742	0.756	1.363	1.119	2.786				•							
M13	0.151	0.160	0.257	0.519	0.463	-0.050	0.494	0.783	0.574	0.498	0.793	1.013	1.266	2.081	2.388			•							
M14	0.149	0.156	0.285	0.535	0.377	0.080	0.324	0.741	0.578	0.480	0.878	0.729	1.310	2.069	1.748	1.228		•						•	
M15	0.146	0.152	0.397	0.612	0.326	-0.091	0.754	0.525	0.543	0.420	0.631	0.591	0.768	1.894	1.505	0.562	2.644	•						•	
M16	0.144	0.150	0.428	0.652	0.276	-0.140	0.404	0.656	0.668	0.406	0.658	0.454	-0.393	1.833	1.390	0.498	1.810	1.915						•	
M17	0.140	0.142	0.463	0.579	0.511	-0.148	0.619	0.189	0.756	0.455	0.462	0.632	-0.086	1.551	1.247	0.516	0.846	1.432	2.815						
M18	0.138	0.140	0.505	0.566	0.462	-0.015	0.443	0.386	0.676	0.317	0.386	0.622	-0.033	1.600	1.086	0.435	0.399	1.133	1.908	1.738					
M19	0.134	0.128	0.506	0.528	0.820	-0.205	0.294	0.539	0.735	0.259	0.147	1.098	-0.693	1.478	0.929	0.550	0.693	0.252	1.463	1.566	1.476			•	
M20	0.102	0.058	0.441	0.520	0.567	0.283	0.334	0.275	0.678	0.396	0.600	1.082	0.232	0.525	0.815	0.244	0.831	1.083	0.721	1.244	0.809	0.931			
M21	0.068	0.032	0.507	0.551	0.501	0.508	0.307	0.466	0.393	0.487	0.542	1.195	0.446	0.329	0.563	0.546	0.500	0.690	0.700	0.763	0.805	0.426	1.089	•	
M22	0.041	0.013	0.518	0.516	0.564	0.503	0.329	0.622	0.398	0.508	0.395	1.055	0.557	0.394	0.483	0.526	0.715	0.469	0.615	0.618	0.444	0.540	0.430	1.148	
M23	0.030	0.007	0.517	0.526	0.512	0.515	0.448	0.487	0.455	0.519	0.429	0.938	0.682	0.389	0.577	0.509	0.500	0.654	0.403	0.575	0.458	0.517	0.386	0.681	0.819

NOTE: Results for only 23 modes are shown here because if the 24th mode is completed the actual IM240 score would then be used rather than the predicted score.

Phase 2 IM240 HC Regression Coefficients Developed from Modal IM240 Data Analysis
1981-1984 Model Year Light-Duty Gasoline Vehicles
0.5 g/mi Cutpoint

				Regression Coefficients													
Mode Number	RMS Error	Reg. Const.	C11	C12	C13	C14	C15	C16	C17	C18	C19	C20	C21	C22	C23		
P11	0.179	0.346	8.141														
P12	0.145	0.219	2.349	3.104							•	•					
P13	0.136	0.198	1.727	2.209	2.823												
P14	0.134	0.192	1.330	2.210	2.034	1.470					•	•					
P15	0.131	0.188	0.571	1.862	1.732	0.807	2.665										
P16	0.129	0.184	-0.983	1.887	1.610	0.588	1.883	2.208			•	•					
P17	0.125	0.171	-0.505	1.456	1.415	0.728	0.712	1.820	3.193	•	•	•	•		•		
P18	0.122	0.168	-0.516	1.481	1.215	0.533	0.276	1.426	2.227	1.985							
P19	0.118	0.154	-0.904	1.381	1.041	0.803	0.703	0.602	1.573	1.758	1.711	•					
P20	0.086	0.076	0.344	0.701	0.965	0.539	1.035	1.357	0.881	1.678	0.988	1.091	•		•		
P21	0.061	0.041	0.994	0.508	0.691	0.796	0.735	1.173	0.792	1.146	0.925	0.640	1.372				
P22	0.039	0.016	1.142	0.562	0.700	0.745	1.010	0.779	0.752	0.874	0.560	0.732	0.647	1.544			
P23	0.029	0.007	1.198	0.561	0.777	0.755	0.770	1.005	0.484	0.833	0.607	0.715	0.560	0.975	1.098		

NOTE: Results for only modes are presented only for modes 11 through 23. Mode 11 is the first mode of Phase 2 and if the 24th mode is completed the actual IM240 full or composite score would be used rather than the predicted score.

Composite IM240 HC Regression Coefficients Developed from Modal IM240 Data Analysis 1985-1989 Model Year Light-Duty Gasoline Vehicles 0.8 g/mi Cutpoint

												Reg	ression	Coeffi	cients										
Mode	RMS Error	Const	C1	C2	C3	C4	C5	C6	C7	C8	С9	C10	C11	C12	C13	C14	C15	C16	C17	C18	C19	C20	C21	C22	C23
M1	0.301	0.430	5.602																						
M2	0.248	0.259	0.159	3.044																					
M3	0.242	0.255	-0.183	2.108	2.824							•		•					•						
M4	0.224	0.223	0.012	1.015	0.555	3.864						•		•					•				•		
M5	0.219	0.212	-0.084	1.168	-0.763	2.919	3.395					•		•											
M6	0.207	0.189	0.424	0.758	-0.026	0.591	1.742	4.092				•		•											
M7	0.194	0.181	0.649	0.668	-0.372	0.443	1.314	1.053	3.066	•	•	•		•	•	•	•	•	•	•	•	•			
M8	0.184	0.169	0.369	0.880	-0.438	0.037	1.302	1.440	0.797	2.830		•	•	•					•						
M9	0.174	0.157	0.342	0.927	-0.266	-0.055	1.335	1.391	0.656	0.035	4.534	•		•					•				•		
M10	0.171	0.154	0.180	1.101	-0.631	0.068	0.949	1.233	0.822	-0.082	3.332	2.217								•					
M11	0.167	0.150	-0.536	1.168	-0.318	-0.082	0.705	1.264	0.846	-0.127	3.103	1.373	4.334												
M12	0.144	0.106	0.170	0.593	0.221	0.266	0.883	0.515	0.448	0.428	1.462	1.314	1.001	2.829											
M13	0.137	0.095	0.153	0.601	0.146	0.360	0.542	0.548	0.519	0.277	1.402	1.109	1.248	2.159	2.122										
M14	0.135	0.091	0.169	0.583	0.126	0.499	0.226	0.547	0.530	0.265	1.482	0.760	1.225	2.183	1.358	1.490									
M15	0.131	0.089	0.272	0.609	0.139	0.358	0.572	0.388	0.544	0.195	1.174	0.605	0.985	1.914	1.217	0.696	2.684								
M16	0.129	0.087	0.278	0.683	0.092	0.322	0.166	0.487	0.671	0.212	1.115	0.457	-0.039	1.831	1.143	0.626	1.714	2.124	•						
M17	0.125	0.081	0.348	0.641	0.274	0.241	0.418	0.209	0.775	0.207	0.887	0.657	0.145	1.602	0.944	0.500	0.969	1.584	2.648						
M18	0.122	0.080	0.348	0.651	0.147	0.387	0.291	0.439	0.622	0.115	0.812	0.631	0.217	1.651	0.809	0.246	0.548	1.358	1.605	1.837					
M19	0.116	0.070	0.355	0.591	0.583	0.180	0.199	0.559	0.697	0.082	0.426	1.018	-0.368	1.511	0.738	0.346	0.826	0.523	1.293	1.374	1.818				
M20	0.085	0.029	0.432	0.465	0.545	0.443	0.311	0.226	0.677	0.359	0.604	1.148	0.387	0.555	0.731	0.187	1.034	0.908	0.755	1.211	0.916	0.953			
M21	0.055	0.018	0.542	0.524	0.385	0.537	0.398	0.546	0.373	0.556	0.462	1.214	0.466	0.368	0.484	0.520	0.679	0.708	0.564	0.703	0.808	0.426	1.126		
M22	0.035	0.009	0.575	0.503	0.544	0.511	0.339	0.596	0.434	0.512	0.371	1.085	0.490	0.400	0.498	0.500	0.819	0.484	0.555	0.610	0.493	0.533	0.467	1.096	
M23	0.024	0.004	0.574	0.499	0.516	0.525	0.455	0.493	0.482	0.528	0.353	0.981	0.668	0.420	0.558	0.534	0.542	0.577	0.422	0.576	0.522	0.504	0.427	0.599	0.842

NOTE: Results for only 23 modes are shown here because if the 24th mode is completed the actual IM240 score would then be used rather than the predicted score.

Phase 2 IM240 HC Regression Coefficients Developed from Modal IM240 Data Analysis 1985-1989 Model Year Light-Duty Gasoline Vehicles 0.5 g/mi Cutpoint

							F	Regressi	ion Coe	fficient	S				
Mode Number	RMS Error	Reg. Const.	C11	C12	C13	C14	C15	C16	C17	C18	C19	C20	C21	C22	C23
P11	0.177	0.259	9.328	•											
P12	0.140	0.150	2.179	3.452				•							
P13	0.132	0.131	1.779	2.527	2.741										
P14	0.129	0.125	1.374	2.545	1.628	1.888		•							
P15	0.125	0.121	0.861	2.070	1.387	1.001	2.991								
P16	0.123	0.119	-0.368	2.053	1.269	0.818	2.160	2.195	•	•	•		•		
P17	0.118	0.109	0.059	1.736	1.014	0.823	1.032	1.762	3.119						
P18	0.115	0.107	-0.009	1.760	0.833	0.559	0.556	1.401	2.128	2.030					
P19	0.109	0.094	-0.526	1.622	0.698	0.823	0.762	0.636	1.569	1.573	2.175		•		
P20	0.077	0.041	0.637	0.716	0.900	0.635	1.081	1.205	1.005	1.455	1.267	1.123	•		
P21	0.057	0.025	0.945	0.562	0.700	0.868	0.834	1.063	0.867	0.971	1.063	0.658	1.363		
P22	0.037	0.013	0.917	0.590	0.738	0.748	1.105	0.785	0.740	0.839	0.583	0.740	0.631	1.554	
P23	0.027	0.006	1.052	0.609	0.774	0.810	0.757	0.906	0.536	0.802	0.675	0.711	0.575	0.903	1.137

NOTE: Results for only modes are presented only for modes 11 through 23. Mode 11 is the first mode of Phase 2 and if the 24th mode is completed the actual IM240 full or composite score would be used rather than the predicted score.

Composite IM240 HC Regression Coefficients Developed from Modal IM240 Data Analysis 1990+ Model Year Light-Duty Gasoline Vehicles 0.8 g/mi Cutpoint

												Regre	ession	Coef	ficien	ts									
Mode	RMS Error	Const.	C1	C2	C3	C4	C5	C6	C7	C8	C9	C10	C11	C12	C13	C14	C15	C16	C17	C18	C19	C20	C21	C22	C23
M1	0.368	0.162	10.855					•			•														•
M2	0.271	0.028	0.252	4.621																					•
M3	0.253	0.036	0.096	2.693	4.788		•	•	•			•	•	•					•				•		•
M4	0.230	0.031	0.720	0.868	1.740	4.997	•	•	•			•	•	•					•				•		•
M5	0.221	0.026	0.391	1.110	0.060	3.325	5.174	•	•			•	•	•					•				•		•
M6	0.207	0.021	0.862	0.623	1.005	0.397	2.743	5.132	•			•	•	•					•				•		•
M7	0.192	0.025	1.279	0.372	0.699	0.393	2.028	1.127	3.732			•	•	•	•		•		•				•		•
M8	0.175	0.030	1.076	0.515	0.477	0.150	1.178	1.750	0.608	3.725		•	•	•					•				•		•
M9	0.162	0.032	1.111	0.490	0.510	0.142	1.351	1.370	0.587	0.494	5.180	•	•	•					•				•		•
M10	0.155	0.034	0.742	0.835	-0.133	0.470	0.754	0.829	0.980	0.287		3.511	•	•					•				•	•	•
M11	0.149	0.037	-0.292	0.916	0.270	0.141	0.342	0.923	1.049	0.326	2.661	2.172	5.629	•					•				•	•	•
M12	0.123	0.028	0.433	0.321	0.650	0.528	0.818	-0.003	0.245	1.037	0.672	2.127	1.234	3.583					•						•
M13	0.115	0.025	0.578	0.296	0.562	0.394	0.374	0.234	0.492	0.715	0.629	1.553	1.271	2.743	2.839				•						•
M14	0.113	0.025	0.618	0.262	0.555	0.503	-0.034	0.227	0.569	0.714	0.776	1.121	1.069	2.758	1.607	2.069			•						•
M15	0.107	0.027	0.747	0.284	0.574	0.244	0.529	0.033	0.676	0.571	0.487			2.369	1.258	0.591	3.362								•
M16	0.102	0.027	0.719	0.462	0.356	0.136	0.065	0.303	0.778	0.668	0.345	0.659	-0.008	2.189	1.033	0.401	2.153	2.766	•						•
M17	0.098	0.026	0.794	0.426	0.518	0.062	0.242	0.168	0.786	0.737	0.079	0.882	0.127	1.928	0.726	0.488	1.245	1.994	2.960						•
M18	0.095	0.026	0.769	0.455	0.367	0.197	0.174	0.420	0.710	0.561	0.016	0.870	0.128	2.015		0.256	0.759	1.521	1.733	2.083					•
M19	0.090	0.023	0.816	0.385	0.654	0.080	0.083	0.642	0.717	0.557	-0.358	1.269	-0.488	1.916	0.340	0.282	0.819	0.888	1.357	1.477	1.846				•
M20	0.068	0.009	0.575	0.360	0.539	0.382	0.257	0.458	0.639	0.556	0.034	1.205		0.804			0.693	1.266		1.203	0.837	1.073			•
M21	0.041	0.007	0.544		0.489		0.539	0.520	0.388	0.588	0.284	1.157	0.523	0.367					0.677	0.674	0.583	0.370	1.309	•	•
M22	0.027	0.003	0.559		0.535		0.444	0.602		0.514	0.284			0.407			0.656				0.470		0.525	1.112	•
M23	0.019	0.002	0.553	0.496	0.515	0.537	0.525	0.518	0.438	0.535	0.349	0.870	0.650	0.429	0.549	0.567	0.521	0.624	0.554	0.536	0.443	0.510	0.387	0.654	0.853

NOTE: Results for only 23 modes are shown here because if the 24th mode is completed the actual IM240 score would then be used rather than the predicted score.

Phase 2 IM240 HC Regression Coefficients Developed from Modal IM240 Data Analysis
1990+ Model Year Light-Duty Gasoline Vehicles
0.5 g/mi Cutpoint

								Regress	sion Coef	ficients					
Mode Number	RMS Error	Reg. Const.	C11	C12	C13	C14	C15	C16	C17	C18	C19	C20	C21	C22	C23
P11	0.153	0.098	13.195												
P12	0.114	0.048	3.112	4.074		•	•	•	•	•	•		•		
P13	0.102	0.041	1.873	2.680	3.765										
P14	0.099	0.039	1.406	2.668	2.167	2.454						•	•		
P15	0.095	0.040	1.107	2.141	1.738	1.122	3.342	•	•	•	•	•	•	•	•
P16	0.091	0.040	-0.030	2.065	1.365	0.858	2.119	3.157				•			
P17	0.088	0.038	0.165	1.791	1.043	0.931	1.028	2.401	3.357	•	•	•	•	•	•
P18	0.085	0.038	0.093	1.843	0.719	0.663	0.610	1.854	2.189	2.206	•	•	•	•	•
P19	0.081	0.035	-0.272	1.779	0.514	0.829	0.678	1.356	1.669	1.515	1.952	•			
P20	0.057	0.016	0.581	0.846	0.727	0.616	0.627	1.840	1.313	1.345	0.856	1.195		•	•
P21	0.040	0.010	0.817	0.585	0.723	0.936	0.588	1.434	1.014	0.886	0.731	0.623	1.512		
P22	0.028	0.005	0.823	0.606	0.751	0.837	0.740	1.015	0.843	0.855	0.581	0.717	0.749	1.426	•
P23	0.020	0.003	0.909	0.612	0.790	0.837	0.609	0.957	0.714	0.775	0.632	0.719	0.591	0.868	1.158

NOTE: Results for only modes are presented only for modes 11 through 23. Mode 11 is the first mode of Phase 2 and if the 24th mode is completed the actual IM240 full or composite score would be used rather than the predicted score.

Appendix E

Calculation of Raw Emission Scores from Dilute Measurements

Calculation of Raw Emission Scores from Dilute Measurements

The constant volume sampling technique, which has been part of the FTP for the exhaust emissions testing of passenger cars and light-duty trucks since the 1972 model year, involves the collection of a sample of exhaust gas after it has been diluted to a known, constant volume. Using this procedure, a device called a "constant volume sampler" dilutes the vehicle exhaust and then samples a constant volume fraction of the dilute mixture. In a typical test facility, the dilution is achieved by drawing "background" air from the room where the vehicle is being driven on a chassis dynamometer. A slipstream from the diluted exhaust is pumped into a series of sample bags during the test. Three sample bags are used for dilute exhaust samples: the first represents the "cold start" phase of the test, the second represents "stabilized" operation, and the third represents the "hot start" phase of the test. Samples of background air are simultaneously collected in three additional bags. At the end of the test, measurement of the concentration of pollutants in the sample bags and calculation of the total flow of the dilute mixture during each phase allows the mass of emissions emitted during each phase of the test to be calculated. Division of the calculated mass by the associated driving distance provides the mass emissions rate (normally expressed in grams per mile).

A variation of the FTP test procedure is used in CVS-based I/M testing. Instead of filling sample bags with dilute mixture during separate phases of the test, the concentrations of pollutants in the dilute exhaust stream are continuously monitored. Mass emissions per mile of travel are calculated from integration of the continuous measurements divided by the distance driven during the test. (This technique facilitates the use of "fast pass" and "fast fail" algorithms for shortening the test in cases where a vehicle is extremely clean or extremely dirty during the early portion of the test.)

In CVS-based testing, the volume of background (dilution) air in the sample substantially exceeds the volume of exhaust gas, usually by a factor of ten or more. As a result, the extent to which the dilution air is contaminated with pollutants can significantly affect the calculated mass emissions. To eliminate this interference, the extent to which the vehicle exhaust has been diluted must be known. The FTP specifies that the ratio of total volume to exhaust volume ("dilution factor") be calculated using the following equation:

[1]
$$DFEPA = \frac{13.4}{CO_{2e} + CO_{e} + HC_{e}}$$

where: CO_{2e}, CO_e, and HC_e are the concentrations measured in the dilute sample expressed as percent volume.

In the above equation, the DF calculated in accordance with the FTP is specified as " DF_{EPA} " to distinguish it from an improved formulation of the DF discussed below. As noted above, DF_{EPA} is used in the FTP to correct the emissions concentration in the sample bag for pollutants in the dilution (background) air. Although not required by the FTP, the average DF can also be used to calculate the average concentration of the undiluted tailpipe emissions emitted while the sample bag was being filled. If there were no pollutants in the dilution air, the tailpipe concentrations could be calculated simply by multiplying the dilute measurement by the DF:

[2]
$$Ctp = Cconc * DF$$

where: Ctp is the actual raw tailpipe concentration, and Cconc is the concentration of a pollutant in the dilute sample defined as:

[3]
$$C_{conc} = C_e - C_d (1 - \frac{1}{DF})$$

where Ce is the pollutant dilute concentration and Cd is the pollutant background concentration.

Substituting [3] into [2] yields:

[4]
$$C tp = \left[C e - C d\left(1 - \frac{1}{DF}\right)\right] DF$$

As noted above, the CVS technique used to measure emissions in I/M programs involves calculating mass emissions by integrating the continuously monitored dilute sample. An average dilution factor can still be calculated from the integrated average of the dilute emissions. The DF can also be calculated continuously and used to calculate the undiluted tailpipe concentration at any point in time. This capability makes it possible to use the CVS emissions measurement system to determine whether a vehicle meets emissions standards that are based on tailpipe concentrations. If, for example, a CO concentration of 0.1% is measured in the dilute exhaust stream, and if the calculated DF is 10, then the tailpipe emission concentration would be calculated to be 1.0% CO (assuming background concentrations were zero).

Although there are several advantages associated with the use of the reverse dilution calculation method, some error is introduced in the calculation of the tailpipe concentration due to the discrepancies that can exist between actual test conditions and the assumptions on which the standard DF calculation is based. As described in detail in a previously referenced technical paper (SAE paper 980678), the DF equation contained in the FTP is based on three assumptions:

- 1. Exhaust emissions of vehicles are the product of a chemically balanced (i.e., stoichiometric) ratio of air and fuel;
- 2. The concentrations of pollutants in the background air have an insignificant effect on the calculation of the DF; and
- 3. No water vapor has been removed from the sample.

Each of these assumptions is problematic when the reverse dilution technique is used to calculate the concentration of pollutants in a vehicle tailpipe that would otherwise be measured directly in an I/M program. First, although most vehicles run very close to a stoichiometric air-fuel ratio, this is not always the case. Second, in the

environment of an I/M test lane, pollution in the background air can be significant. Third, analyzers routinely used for raw exhaust measurement remove a substantial amount of water from the sample.³

A more complicated expression of the DF is required to address the limitations of the DF equation contained in the FTP. The recommended equation is as follows:⁴

$$DF = \frac{100 - K_1(CO_{2d}) - K_2(CO_d) - K_3(HC_d)}{K_1(CO_{2e} - CO_{2d}) + K_2(CO_e - CO_d) + K_3(HC_e - HC_d)}$$

where: K₁, K₂, and K₃ are constants that depend on the fuel type (see below);

 CO_{2d} is the concentration of CO_2 in the background air; CO_d is the concentration of CO in the background air;

HC_d is the concentration of HC in the background air;

 CO_{2e} is the concentration of CO_2 in the dilute sample;

^{CO}e is the concentration of CO in the dilute sample; and

HC_e is the concentration of HC in the dilute sample.

All of the concentrations in the above equation are expressed in volume percent. The HC values are expressed in hexane equivalent. The values of K_1 , K_2 , and K_3 depend on the type of fuel and whether the calculated pollutant concentrations are on a wet or dry basis. When attempting to match measurements that would be made by typical systems for raw exhaust measurement, the values for dry exhaust should be used. For gasoline fuel with pollutant concentrations measured on a wet basis, such as in IM240 set-ups, the value of K_1 is 6.5431, the value for K_2 is 4.6561, and the value of K_3 is 57.0945.

Dilution Correction of Tailpipe Measurements

As noted earlier, one of the problems associated with I/M standards based on maximum allowable tailpipe concentrations is that certain causes of dilution (e.g., air injection,⁵ exhaust leaks, or inadequate sample probe insertion

³So-called "BAR90" analyzers actually use a condensate removal system to dispose of the water that condenses when raw exhaust is drawn through the sample probe; however, the efficiency of water removal depends on the temperature of the exhaust sample because no temperature control is provided by the analyzer.

^{*}The DF equation in the previously referenced SAE paper is based on the simplifying assumption that there is no residual oxygen in the exhaust of stoichiometric or richer air-fuel mixtures. This assumption holds unless there is substantial misfire. In the case of misfire, the exhaust may contain oxygen that dilutes the concentration of other constituents. Equation 4 is a refinement of the equation contained in the SAE paper that accounts for misfire.

⁵Air injection can reduce mass emissions by facilitating more complete combustion in either the exhaust manifold or the catalytic converter. However, the dilution associated with air injection causes the measured concentration to be

depth) may cause measured concentrations to be substantially lower than for another vehicle with identical mass emissions. Because of this problem, EPA guidance for concentration measurement during simple I/M tests specifies that the sum of CO plus CO_2 emissions should be at least 6% in order for the test to be considered valid. Although the basis for the recommendation is not documented, it appears to represent the maximum level of exhaust dilution that might be expected with a relatively high output air injection system installed on a relatively small engine. As a result, it allows the exhaust concentration to be reduced by more than 50% due to various sources of dilution.⁶ It is therefore a relatively ineffective means of preventing exhaust dilution from affecting the results of an I/M test.

Recently, the California Bureau of Automotive Repair (BAR) devised an improved procedure for eliminating the effects of exhaust dilution. BAR's procedure uses equations developed from basic combustion chemistry to determine the extent to which an exhaust sample must have been diluted before a concentration measurement was made. The measured concentrations are adjusted to what they would be under stoichiometric conditions with no dilution air from any source (including leaner than stoichiometric operation). BAR's exhaust dilution correction essentially involves the application of a dilution factor to the concentrations measured at the tailpipe. As described in Sierra's SAE paper, BAR's method is more sophisticated than the DF calculation incorporated into the FTP because it accounts for variations in air-fuel ratio. However, the BAR procedure ignores the effects of background air, which is not a factor during tailpipe measurements. As the SAE paper illustrates, Sierra's recommended DF equation incorporates the same basic dilution correction used by BAR in combination with a correction for pollutants in the background air. When correcting tailpipe concentrations for dilution, where no background air is involved, Sierra's DF calculation and BAR's dilution adjustment produce the same result.

Recognizing the advantages of BAR's new dilution correction procedure, EPA has incorporated it in Guidance to states on Acceleration Simulation Mode (ASM) testing. Although BAR's procedure is equally applicable to other tests that rely on concentration measurement, it has not yet been incorporated into revised guidance for idle, 2500 rpm, and other steady-state tests. However, when CVS testing is used in combination with Sierra's recommended reverse dilution calculation procedure, the effect is similar to using BAR's dilution correction.

reduced by more than the true reduction in mass emissions.

⁶With measurement systems that remove water, and for an engine running a stoichiometric, a 6% sum of CO and CO₂ represents each part exhaust being diluted with 1.5 parts air.

Appendix F

Modal Analysis of Second-by-Second Data Preconditioning Guidelines

Developed by Sierra Research Contract 68-C4-0056 Work Assignment 2-04

Modal Analysis of Second-by-Second Data Preconditioning Guidelines

Developed by Sierra Research Contract 68-C4-0056 Work Assignment 2-04

Using the replicate IM240 data collected by Gordon-Darby, it was possible, through trial and error, to identify criteria to determine whether a vehicle failing an initial IM240 is inadequately preconditioned and should be tested again. This analysis was performed for each pollutant individually, and then for all pollutants combined. The analysis included 283 LDVs and 83 LDTs. The evaluation followed a step-wise progression in which the aim was to maximize the identification of vehicles that could benefit from a second test, while minimizing testing of vehicles likely to fail a second test. Recommendations for passenger cars are summarized below. A similar set of conditions was also developed for light-duty trucks, which are subject to different IM240 standards than passenger cars.

IM240 Retest Criteria for Passenger Cars

HC Failures - If PPmHC209-214 is less than 1,500, a retest is recommended if any of the following occur:

1. Phase 2 HC < 0. 8 g/mi; or 2. massHC₁₇₅₋₁₉₉ < 0.2 g; or 3. (ppmHC₇₅₋₈₀/ppmHC₂₁₄) > 4.0

For vehicles failing only HC, the following additional constraints are required for a vehicle to be retested:

1. Mass $HC_{175-199} < 0.3g$ and $(ppmHC_{75-80}/ppmHC_{209-214}) > 1.5; or$

2. Mass $HC_{175-199} < 0.3g$ and Phase 2 HC < 1.0 g/mi

CO Failures - For CO failures, the above criteria for HC are recommended. In addition, the following constraints are recommended:

 do not retest if Phase 2 CO > 20 g/mi and (Phase 1 CO/Phase 2 CO) <2; and
 if the vehicle fails both HC and CO, retest if Mass HC₁₇₅₋₁₉₉ <0.3 g and mass CO₁₇₅₋₁₉₉ < 5.0 g.

If the vehicle is a CO-only failure, then a vehicle would benefit from a retest if:

1. Mass CO₁₇₅₋₁₉₉ < 6.0 g; or 2. (ppmCO₇₅₋₈₀/ppmCO₂₀₉₋₂₁₄) > 4.0; or 3. Mass CO_{175.199} < 10 g and (Phase I CO > 0.75 x Phase 2 CO).

NOx Failures - For vehicles failing HC or CO and NOx, a retest is recommended if the following condition occurs: 1. Mass $NOx_{175-199} = 1.0g$ For NOx Only failures, retest is recommended if the following criteria are met:

1. Mass NOx175199<9; or

- 2. Mass NOx175-199<1.1 and (ppmNOx40-45/ppmNOx209-215)>1.5; or
- 3. IM240 NOx<2.2 and (ppmNOx₄₀₋₄₅/ppmNOx₂₀₉₋₂₁₅)> 1.0

Multiple Pollutants - For multiple pollutant failures, a retest is eliminated under the following conditions:

1. the vehicle fails for all pollutants; or

- 2. the vehicle fails HC and CO and (Phase 2 CO > 20 g/mi and mass $CO_{175-199} > 6.0$ g); or
- 3. the vehicle fails HC and NOx and (ppmHC₂₀₉₋₂₁₄ >1,200) or (ppmNOx₂₀₉₋₂₁₄ > 1,200)

IM240 Retest Criteria for Light-Duty Trucks

Because they are subject to different numerical IM240 emission standards, a different set of retest criteria were developed for light-duty trucks. These criteria are similar to those established for passenger cars, with adjustments to account for standards differences.

HC Failures - For <u>1981 to 1983</u> model year vehicles, if $ppmHC_{209-214} < 2,000$ and any of the following conditions exist, then a retest is recommended:

- 1. Phase 2 HC < 3.0 g/mi; or
- 2. Mass HC₁₇₅₋₁₉₉ < 0.8 g; or
- 3. (ppmHC₇₅₋₈₀/ppmHC₂₀₉₋₂₁₄)>4.0

In addition, if the full IM240 is less than 3.5 g/mi HC (regardless of the value of $ppmHC_{209-214}$), then a retest is recommended.

For 1984 <u>and later</u> model year vehicles, if ppmHC₂₀₉₋₂₁₄<1,500 and any of the following conditions exist a retest is recommended:

- 1. Phase 2 HC< 2.0 g/mi; or
- 2. MassHC₁₇₅₋₁₉₉ < 0.4 g; or
- 3. (ppmHC₇₅₋₈₀/ppmHC₂₀₉₋₂₁₄)>4.0

In addition, if 0.4<Mass HC₁₇₅₋₁₉₉<0.8 and (ppmHC₇₅₋₈₀/ppmHC₂₀₉₋₂₁₄)>2.0 (regardless of the value of ppmHC₂₀₉₋₂₁₄) then a retest is recommended.

A retest is not recommended if Phase 2 HC > 3.2 g/mi.

CO Failures - For CO failures, the above criteria outlined for HC were also used. In addition, the following conditions were also imposed to cut down on the number of vehicles incorrectly identified as needing a retest:

- 1. If $\underline{1981}$ to $\underline{1983}$ model year and Mass CO₁₇₅₋₁₉₉>36g then do not retest.
- 2. If <u>1984 or later</u> model year and Mass $CO_{175-199}$ >18g then do not retest.
- 3. If Phase 2 CO>40 and Phase 2 CO > Phase I CO then do not retest.

NOx Failures - If the vehicle failed NOx and either HC or CO, the above criteria were used to determine the need for a retest. For LDT1&2s, if the vehicle failed <u>only NOx</u>. then a retest is recommended if Mass $NOx_{175-199} < 1.4$ g. For 1988 and later LDT3&4s, a retest is recommended only if Mass $NOx_{175-199} < 2.5$ g.

Appendix G

Full and Fast-Pass IM240 Positive Kinetic Energy Speed Variation Limits

Developed by Sierra Research Contract 68-C4-0056

Full and Fast-Pass IM240 Positive Kinetic Energy Speed Variation Limits

Developed by Sierra Research Contract 68-C4-0056

Evaluation of Alternative Statistical Measures

Based upon similar work conducted by the New York Automotive Emissions Laboratory (AEL,)⁷ two easily determined, alternative statistical metrics were evaluated for their ability to identify and quantify IM240 speed variations that significantly affect emissions:

- (1). DPWRSUM the sum of absolute changes in specific power; and
- (2). Positive Kinetic Energy (PKE) the sum of positive differences in kinetic energy per unit distance.

Each of these metrics are explained in more detail below.

DPWRSUM - Specific power is defined as power per unit mass, which can be restated as follows:

Specific Power =
$$\frac{\text{power}}{\text{mass}} = \frac{\text{work}}{\text{mass} \times \Delta \text{time}} = \frac{\Delta \text{kinetic energy}}{\text{mass} \times \Delta \text{time}} = \frac{\frac{1}{2} \times \text{mass} \times \Delta \text{V}^2}{\text{mass} \times \Delta \text{time}}$$

Over a transient driving cycle of second-by-second speeds, EPA defines the specific power P at any time t (and dropping the factor of $\frac{1}{2}$) as:

$$Pt = Vt^2 - Vt - 1^2$$

The absolute difference in specific power at time t can then be written as:

$$\mathbf{D} \mathbf{P}_{t} = |\mathbf{P}_{t} - \mathbf{P}_{t-1}| = |\mathbf{V}_{t}^{2} - 2 \mathbf{V}_{t-1}^{2} + \mathbf{V}_{t-2}^{2}|$$

The DPWRSUM statistic then is defined over a cycle of N seconds as:

⁷ W. J. Webster and C. Shih, "A Statistically Derived Metric to Monitor Time-Speed Variability in Practical Emissions Testing," New York State Department of Environmental Conservation, presented at the 6th CRC On-Road Vehicle Emissions Workshop, March 18-20, 1996.

$$DPWRSUM = \sum_{t=0}^{N} DP_{t} = \sum_{t=0}^{N} |V_{t}^{2} - 2V_{t-1}^{2} + V_{t-2}^{2}|$$

PKE - Positive Kinetic Energy has been defined mathematically as:

$$PKE = \frac{\sum_{t=0}^{N} PP_{t}}{\int_{0}^{x} dx}$$

over a traveled driving cycle of distance x where PP is the positive specific power and is given by the following expression when $V_t > V_{t-1}$, and is zero when $V_t \le V_{t-1}$.

$$PP_t = V_t^2 - V_{t-1}^2$$

Each of these metrics can be easily computed from the second-by-second speed measurements collected in IM240 testing. In comparing their relative ability to identify speed variations that produce high emissions, it is helpful to consider which speed variations contribute to the value of each metric (similar to the earlier examination of the SE statistic) over an IM240 test.

Note that although both DPWRSUM and PKE are affected by differences in specific power or squared speeds over "adjacent" seconds of an IM240 trace, the value of DPWRSUM is increased during decelerations as well as accelerations. PKE on the other hand, is only increased during acceleration periods.

IM24	0 REFE DATA	RENCE	PKE VA	RIATIO	N CUTPOI	NTS (m	iles/hr2)
		CUM PKE	"BASE "	MULT.	VARYING		LATIVE KE
TIME	SPEED	(miles/hr2)	<u>DELTA</u>	<u>FACTO</u> <u>R</u>	<u>DELTA</u>	<u>LOW</u>	<u>HIGH</u>
0	0.0	0.0	•	•	•	•	•
1	0.0	0.0	•	•	•	•	•
2	0.0	0.0	•	•	•	•	•
3	0.0	0.0	٠	•	٠	•	•
4	0.0	0.0	٠	•	٠	•	•
5	3.0	10,800.0	٠	•	٠	•	•
6	5.9	14,080.4	٠	•	٠	•	•
7	8.6	15,214.6	•	•	٠	•	•
8	11.5	16,417.2	٠	•	٠	•	•
9	14.3	17,001.5	•	•	•	•	•
10	16.9	17,079.7	•	•	٠	•	•
11	17.3	13,902.5	•	•	٠	•	•
12	18.1	12,336.8	•	•	٠	•	•
13	20.7	13,263.7	•	٠	٠	•	•
14	21.7	12,284.1	•	٠	٠	•	•
15	22.4	11,261.4	•	•	٠	•	•
16	22.5	9,964.5	٠	•	٠	•	•
17	22.1	8,890.2	٠	•	٠	•	•
18	21.5	8,046.4	•	•	•	•	•
19	20.9	7,366.6	•	•	•	•	•
20	20.4	6,805.5	•	•	•	•	•
21	19.8	6,336.9	•	•	٠	•	•
22	17.0	5,983.3	٠	•	٠	•	•
23	14.9	5,704.2	٠	•	٠	•	•
24	14.9	5,450.1	•	•	•	٠	•
25	15.2	5,306.1	•	•	•	٠	•
26	15.5	5,171.6	•	•	•	٠	•
27	16.0	5,103.3	•	•	•	•	•
28	17.1	5,213.3	•	•	•	•	•
29	19.1	5,599.3	•	•	•	٠	•
30	21.1	5,990.0	342.3	4.000	1,369.3	4,621	7,359
31	22.7	6,242.3	356.7	3.986	1,421.8	4,820	7,664
32	22.9	6,014.8	343.7	3.971	1,365.1	4,650	7,380
33	22.7	5,745.3	328.3	3.957	1,299.3	4,446	7,045
34	22.6	5,500.0	314.3	3.943	1,239.3	4,261	6,739
35	21.3	5,287.2	302.2	3.929	1,187.0	4,100	6,474
36	19.0	5,110.8	292.1	3.914	1,143.3	3,968	6,254
37	17.1	4,961.9	283.6	3.900	1,105.9	3,856	6,068

38	15.8	4,831.8	276.1	3.886	1,072.9	3,759	5,905
39	15.8	4,708.3	269.1	3.871	1,041.7	3,667	5,750
40	17.7	4,937.5	282.2	3.857	1,088.4	3,849	6,026
41	19.8	5,220.8	298.4	3.843	1,146.5	4,074	6,367
42	21.6	5,450.3	311.5	3.829	1,192.5	4,258	6,643
43	23.2	5,638.2	322.2	3.814	1,229.0	4,409	6,867
44	24.2	5,685.3	324.9	3.800	1,234.6	4,451	6,920
45	24.6	5,592.5	319.6	3.786	1,209.9	4,383	6,802
46	24.9	5,481.7	313.3	3.771	1,181.5	4,300	6,663
47	25.0	5,332.7	304.8	3.757	1,145.0	4,188	6,478
48	25.7	5,321.5	304.1	3.743	1,138.2	4,183	6,460
49	26.1	5,245.9	299.8	3.729	1,117.8	4,128	6,364
50	26.7	5,216.3	298.1	3.714	1,107.2	4,109	6,323
51	27.5	5,230.2	298.9	3.700	1,105.9	4,124	6,336
52	28.6	5,307.9	303.3	3.686	1,118.0	4,190	6,426
53	29.3	5,298.0	302.8	3.671	1,111.6	4,186	6,410
54	29.8	5,246.1	299.8	3.657	1,096.4	4,150	6,343
55	30.1	5,155.0	294.6	3.643	1,073.2	4,082	6,228
56	30.4	5,068.3	289.6	3.629	1,051.0	4,017	6,119
57	30.7	4,985.6	284.9	3.614	1,029.8	3,956	6,015
58	30.7	4,848.3	277.1	3.600	997.5	3,851	5,846
59	30.5	4,719.2	269.7	3.586	967.0	3,752	5,686
60	30.4	4,597.2	262.7	3.571	938.3	3,659	5,535
61	30.3	4,481.7	256.1	3.557	911.1	3,571	5,393
62	30.4	4,389.2	250.8	3.543	888.7	3,501	5,278
63	30.8	4,352.1	248.7	3.529	877.6	3,474	5,230
64	30.4	4,250.1	242.9	3.514	853.6	3,397	5,104
65	29.9	4,154.4	237.4	3.500	831.0	3,323	4,985
66	29.5	4,064.1	232.3	3.486	809.6	3,255	4,874
67	29.8	4,022.9	229.9	3.471	798.1	3,225	4,821
68	30.3	4,013.3	229.3	3.457	792.9	3,220	4,806
69	30.7	3,988.8	228.0	3.443	784.8	3,204	4,774
70	30.9	3,935.5	224.9	3.429	771.1	3,164	4,707
71	31.0	3,869.4	221.1	3.414	755.0	3,114	4,624
72	30.9	3,791.8	216.7	3.400	736.8	3,055	4,529
73	30.4	3,718.5	212.5	3.386	719.5	2,999	4,438
74	29.8	3,649.2	208.5	3.371	703.1	2,946	4,352
75	29.9	3,595.5	205.5	3.357	689.8	2,906	4,285
76	30.2	3,569.2	204.0	3.343	681.9	2,887	4,251
77	30.7	3,569.2	204.0	3.329	678.9	2,890	4,248
78	31.2	3,569.3	204.0	3.314	676.0	2,893	4,245
79	31.8	3,582.2	204.7	3.300	675.6	2,907	4,258
80	32.2	3,569.2	204.0	3.286	670.2	2,899	4,239

81	32.4	3,531.2	201.8	3.271	660.2	2,871	4,191
82	32.2	3,469.8	198.3	3.257	645.9	2,824	4,116
83	31.7	3,411.4	195.0	3.243	632.2	2,779	4,044
84	28.6	3,360.3	192.0	3.229	620.0	2,740	3,980
85	25.1	3,316.8	189.5	3.214	609.3	2,708	3,926
86	21.6	3,280.2	187.5	3.200	599.9	2,680	3,880
87	18.1	3,250.2	185.7	3.186	591.7	2,658	3,842
88	14.6	3,226.3	184.4	3.171	584.7	2,642	3,811
89	11.1	3,208.4	183.4	3.157	578.9	2,630	3,787
90	7.6	3,196.3	182.7	3.143	574.1	2,622	3,770
91	4.1	3,189.8	182.3	3.129	570.3	2,619	3,760
92	0.6	3,188.9	182.2	3.114	567.5	2,621	3,756
93	0.0	3,188.9	182.2	3.100	564.9	2,624	3,754
94	0.0	3,188.9	182.2	3.086	562.3	2,627	3,751
95	0.0	3,188.9	182.2	3.071	559.7	2,629	3,749
96	0.0	3,188.9	182.2	3.057	557.1	2,632	3,746
97	0.0	3,188.9	182.2	3.043	554.5	2,634	3,743
98	3.3	3,203.1	183.0	3.029	554.4	2,649	3,757
99	6.6	3,250.7	185.8	3.014	560.0	2,691	3,811
100	9.9	3,331.3	190.4	3.000	571.1	2,760	3,902
101	13.2	3,443.8	196.8	2.986	587.6	2,856	4,031
102	16.5	3,587.2	205.0	2.971	609.1	2,978	4,196
103	19.8	3,760.1	214.9	2.957	635.4	3,125	4,396
104	22.2	3,892.7	222.5	2.943	654.7	3,238	4,547
105	24.3	4,013.3	229.4	2.929	671.7	3,342	4,685
106	25.8	4,090.8	233.8	2.914	681.3	3,409	4,772
107	26.4	4,093.0	233.9	2.900	678.3	3,415	4,771
108	25.7	4,045.3	231.2	2.886	667.1	3,378	4,712
109	25.1	3,999.9	228.6	2.871	656.4	3,344	4,656
110	24.7	3,956.1	226.1	2.857	646.0	3,310	4,602
111	25.2	3,951.8	225.8	2.843	642.0	3,310	4,594
112	25.4	3,924.1	224.3	2.829	634.3	3,290	4,558
113	27.2	4,024.3	230.0	2.814	647.2	3,377	4,672
114	26.5	3,979.2	227.4	2.800	636.7	3,342	4,616
115	24.0	3,939.2	225.1	2.786	627.1	3,312	4,566
116	22.7	3,902.0	223.0	2.771	618.0	3,284	4,520
117	19.4	3,870.9	221.2	2.757	609.9	3,261	4,481
118	17.7	3,842.9	219.6	2.743	602.4	3,241	4,445
119	17.2	3,816.0	218.1	2.729	595.0	3,221	4,411
120	18.1	3,834.3	219.1	2.714	594.8	3,240	4,429
121	18.6	3,832.2	219.0	2.700	591.3	3,241	4,423
122	20.0	3,879.0	221.7	2.686	595.4	3,284	4,474
123	20.7	3,887.7	222.2	2.671	593.5	3,294	4,481

124	21.7	3,914.4	223.7	2.657	594.4	3,320	4,509
125	22.4	3,923.5	224.2	2.643	592.6	3,331	4,516
126	22.5	3,895.8	222.6	2.629	585.2	3,311	4,481
127	22.1	3,863.1	220.8	2.614	577.1	3,286	4,440
128	21.5	3,831.7	219.0	2.600	569.3	3,262	4,401
129	20.9	3,801.8	217.3	2.586	561.8	3,240	4,364
130	20.4	3,772.9	215.6	2.571	554.4	3,219	4,327
131	19.8	3,745.4	214.0	2.557	547.3	3,198	4,293
132	17.0	3,722.1	212.7	2.543	540.9	3,181	4,263
133	17.1	3,703.4	211.6	2.529	535.1	3,168	4,239
134	15.8	3,682.2	210.4	2.514	529.1	3,153	4,211
135	15.8	3,661.2	209.2	2.500	523.1	3,138	4,184
136	17.7	3,720.0	212.6	2.486	528.4	3,192	4,248
137	19.8	3,794.6	216.9	2.471	535.9	3,259	4,330
138	21.6	3,860.2	220.6	2.457	542.1	3,318	4,402
139	22.2	3,863.3	220.8	2.443	539.3	3,324	4,403
140	24.5	3,964.6	226.6	2.429	550.2	3,414	4,515
141	24.7	3,943.1	225.3	2.414	544.0	3,399	4,487
142	24.8	3,915.9	223.8	2.400	537.1	3,379	4,453
143	24.7	3,883.2	221.9	2.386	529.4	3,354	4,413
144	24.6	3,851.1	220.1	2.371	521.9	3,329	4,373
145	24.6	3,819.6	218.3	2.357	514.5	3,305	4,334
146	25.1	3,817.5	218.2	2.343	511.1	3,306	4,329
147	25.6	3,815.4	218.0	2.329	507.7	3,308	4,323
148	25.7	3,789.6	216.6	2.314	501.2	3,288	4,291
149	25.4	3,758.6	214.8	2.300	494.0	3,265	4,253
150	24.9	3,728.8	213.1	2.286	487.1	3,242	4,216
151	25.0	3,704.9	211.7	2.271	480.9	3,224	4,186
152	25.4	3,698.2	211.3	2.257	477.0	3,221	4,175
153	26.0	3,702.8	211.6	2.243	474.6	3,228	4,177
154	26.0	3,673.1	209.9	2.229	467.8	3,205	4,141
155	25.7	3,644.1	208.3	2.214	461.1	3,183	4,105
156	26.1	3,637.9	207.9	2.200	457.4	3,181	4,095
157	26.7	3,643.0	208.2	2.186	455.0	3,188	4,098
158	27.3	3,648.1	208.5	2.171	452.7	3,195	4,101
159	30.5	3,812.6	217.9	2.157	470.0	3,343	4,283
160	33.5	3,978.0	227.3	2.143	487.1	3,491	4,465
161	36.2	4,133.0	236.2	2.129	502.8	3,630	4,636
162	37.3	4,172.3	238.4	2.114	504.1	3,668	4,676
163	39.3	4,282.5	244.7	2.100	513.9	3,769	4,796
164	40.5	4,330.6	247.5	2.086	516.2	3,814	4,847
165	42.1	4,412.1	252.1	2.071	522.3	3,890	4,934
166	43.5	4,477.8	255.9	2.057	526.4	3,951	5,004

167	45.1	4,561.4	260.7	2.043	532.5	4,029	5,094
168	46.0	4,584.2	262.0	2.029	531.4	4,053	5,116
169	46.8	4,598.2	262.8	2.014	529.3	4,069	5,127
170	47.5	4,603.2	263.1	2.000	526.1	4,077	5,129
171	47.5	4,546.8	259.8	1.986	516.0	4,031	5,063
172	47.3	4,492.0	256.7	1.971	506.1	3,986	4,998
173	47.2	4,438.6	253.7	1.957	496.4	3,942	4,935
174	47.2	4,386.5	250.7	1.943	487.0	3,899	4,874
175	47.4	4,352.1	248.7	1.929	479.7	3,872	4,832
176	47.9	4,343.2	248.2	1.914	475.1	3,868	4,818
177	48.5	4,342.6	248.2	1.900	471.5	3,871	4,814
178	49.1	4,342.0	248.1	1.886	467.9	3,874	4,810
179	49.5	4,324.9	247.2	1.871	462.5	3,862	4,787
180	50.0	4,316.3	246.7	1.857	458.1	3,858	4,774
181	50.6	4,316.0	246.7	1.843	454.5	3,861	4,771
182	51.0	4,299.3	245.7	1.829	449.3	3,850	4,749
183	51.5	4,291.0	245.2	1.814	444.9	3,846	4,736
184	52.2	4,299.3	245.7	1.800	442.3	3,857	4,742
185	53.2	4,332.3	247.6	1.786	442.1	3,890	4,774
186	54.1	4,356.8	249.0	1.771	441.0	3,916	4,798
187	54.6	4,347.7	248.5	1.757	436.6	3,911	4,784
188	54.9	4,322.3	247.0	1.743	430.5	3,892	4,753
189	55.0	4,280.9	244.6	1.729	422.9	3,858	4,704
190	54.9	4,232.4	241.9	1.714	414.6	3,818	4,647
191	54.6	4,185.2	239.2	1.700	406.6	3,779	4,592
192	54.6	4,139.1	236.5	1.686	398.7	3,740	4,538
193	54.8	4,109.5	234.9	1.671	392.5	3,717	4,502
194	55.1	4,088.2	233.6	1.657	387.2	3,701	4,475
195	55.5	4,075.0	232.9	1.643	382.6	3,692	4,458
196	55.7	4,046.6	231.3	1.629	376.6	3,670	4,423
197	56.1	4,034.0	230.5	1.614	372.1	3,662	4,406
198	56.3	4,006.4	229.0	1.600	366.3	3,640	4,373
199	56.6	3,986.7	227.8	1.586	361.3	3,625	4,348
200	56.7	3,952.4	225.9	1.571	354.9	3,597	4,307
201	56.7	3,911.4	223.5	1.557	348.1	3,563	4,259
202	56.3	3,871.4	221.2	1.543	341.3	3,530	4,213
203	56.0	3,832.5	219.0	1.529	334.8	3,498	4,167
204	55.0	3,795.0	216.9	1.514	328.4	3,467	4,123
205	53.4	3,759.3	214.8	1.500	322.3	3,437	4,082
206	51.6	3,725.4	212.9	1.486	316.3	3,409	4,042
207	51.8	3,704.9	211.7	1.471	311.5	3,393	4,016
208	52.1	3,691.1	210.9	1.457	307.4	3,384	3,998
209	52.5	3,683.7	210.5	1.443	303.7	3,380	3,987

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210	53.0	3,682.8	210.5	1.429	300.7	3,382	3,984
211	53.5	3,682.0	210.4	1.414	297.6	3,384	3,980
212	54.0	3,681.1	210.4	1.400	294.5	3,387	3,976
213	54.9	3,705.8	211.8	1.386	293.5	3,412	3,999
214	55.4	3,704.7	211.7	1.371	290.4	3,414	3,995
215	55.6	3,684.4	210.6	1.357	285.8	3,399	3,970
216	56.0	3,677.1	210.1	1.343	282.2	3,395	3,959
217	56.0	3,644.6	208.3	1.329	276.7	3,368	3,921
218	55.8	3,612.7	206.5	1.314	271.3	3,341	3,884
219	55.2	3,581.7	204.7	1.300	266.1	3,316	3,848
220	54.5	3,551.6	203.0	1.286	261.0	3,291	3,813
221	53.6	3,522.5	201.3	1.271	255.9	3,267	3,778
222	52.5	3,494.5	199.7	1.257	251.1	3,243	3,746
223	51.5	3,467.4	198.2	1.243	246.3	3,221	3,714
224	50.5	3,441.2	196.7	1.229	241.6	3,200	3,683
225	48.0	3,416.8	195.3	1.214	237.1	3,180	3,654
226	44.5	3,394.4	194.0	1.200	232.8	3,162	3,627
227	41.0	3,374.0	192.8	1.186	228.6	3,145	3,603
228	37.5	3,355.6	191.8	1.171	224.6	3,131	3,580
229	34.0	3,339.0	190.8	1.157	220.8	3,118	3,560
230	30.5	3,324.3	190.0	1.143	217.1	3,107	3,541
231	27.0	3,311.4	189.2	1.129	213.6	3,098	3,525
232	23.5	3,300.3	188.6	1.114	210.2	3,090	3,510
233	20.0	3,290.9	188.1	1.100	206.9	3,084	3,498
234	16.5	3,283.1	187.6	1.086	203.7	3,079	3,487
235	13.0	3,277.1	187.3	1.071	200.7	3,076	3,478
236	9.5	3,272.7	187.0	1.057	197.7	3,075	3,470
237	6.0	3,269.9	186.9	1.043	194.9	3,075	3,465
238	2.5	3,268.7	186.8	1.029	192.1	3,077	3,461
239	0.0	3,268.7	186.8	1.014	189.5	3,079	3,458
Cycle	Sums	3,268.7				3,079	3,458

Appendix H

Derivation of TRLHP Coefficients

Derivation of TRLHP Coefficients

(a) Road Load Equation

(1) <u>Vehicle Loading</u>. Road load is defined by the following equation relating track road load horsepower and vehicle velocity.

 $TRLHP_{@ Obmph} = (A_v * Obmph) + (B_v * Obmph^2) + (C_v * Omph^3)$

Where: TRLHP = Track Road Load Horsepower.

 $A_v, B_v, C_v = Coefficients$ relating TRLHP and velocity.

Obmph = Observed velocity in mph.

(2) <u>Coefficients</u>. A_V , B_V , and C_V are horsepower coefficients from EPA vehicle certification data or EPA default values. Coefficients shall be calculated to a minimum of five significant digits by the following equations. Power fractions determined from track coast-down data shall be calculated to a minimum of two significant digits. In the absence of new car certification coefficients, the default power fractions shall be used.

(A)
$$A_v = \frac{A_v PF}{50} * (TRLHP_{@50mph}) hp / mph$$

(B)
$$B_v = \frac{B_v PF}{2500} * (TRLHP_{@50mph}) hp / mph^2$$

(C)
$$C_v = \frac{C_v PF}{125,000} * (TRLHP_{@50mph}) hp / mph^3$$

Where: $A_V, B_V, C_V = Coefficients$ relating TRLHP and velocity.

 A_v PF, B_v PF, and C_v PF are power fractions, and indicate the fraction of the total power at 50 mph contributed by each of the A_v *50, B_v *2500, and C_v *125,000 terms.

TRLHP@50mph = Track Road Load Horsepower at 50mph.

(D)
$$A_V PF + B_V PF + C_V PF = 1$$

Derivation of $A_v PF$, $B_v PF$, and $C_v PF$ from known track coastdown curves shall be computed as follows:

(E)
$$A_v PF = \frac{A_v * 50}{(A_v * 50) + (B_v * 2500) + (C_v * 125,000)}$$

(F)
$$B_v PF = \frac{B_v * 2500}{(A_v * 50) + (B_v * 2500) + (C_v * 125,000)}$$

(G)
$$C_v PF = \frac{C_v * 125,000}{(A_v * 50) + (B_v * 2500) + (C_v * 125,000)}$$

Default values:

$$A_{V}PF = 0.35$$
$$B_{V}PF = 0.10$$
$$C_{V}PF = 0.55$$

(3) $\underline{\text{TRLHP}}_{@50\text{mph.}}$ In absence of new vehicle certification data, the 50 mph TRLHP shall be selected from the EPA I/M Look-up Table. It is based on the following equation:

$$TRLHP = \frac{\left(\frac{0.5 * ETW}{32.2} * (V_1^2 - V_2^2)\right)}{550 * ET}$$

Where: ET = Elapsed time for the vehicle on the road to coast down from 55 to 45 mph

ETW = Equivalent Test Weight in pounds

 $V_1 = Initial \ velocity \ in \ feet/second$

 $V_2 = Final \ velocity \ in \ feet/second$

Appendix I

Derivation of GTRL Coefficients

Derivation of Dynamometer Tire/Roll Interface Losses

(a) Generic Tire Roll Loss

(1) <u>Tire/Roll Interface Losses</u>. Tire/roll losses include vehicle drive train losses and may be determined on a vehicle and dynamometer roll size specific basis, or using the default values presented below.

Tire losses may be characterized on a vehicle and roll size specific basis by the following equation:

 $GTRL_{@ Obmph} = (A_t * Obmph) + (B_t * Obmph^2) + Obmph^3)$

Where: GTRL = Generic tire/roll interface losses, in horsepower.

A_t, B_t, C_t are coefficients derived by fitting a third order curve of tire losses, in horsepower, and velocity.

Obmph is the observed velocity in mph.

(A)
$$A_{t8} = \frac{0.76}{50} * (GTRL_{@50mph-8}) hp / mph$$

(B)
$$B_{t8} = \frac{0.33}{2500} * (GTRL_{@50mph-8}) hp / mph^2$$

(C)
$$C_{18} = \frac{-0.09}{125,000} * (GTRL_{@50mph-8}) hp / mph^{3}$$

Where: A_{t8} , B_{t8} , C_{t8} are coefficients relating tire losses, in horsepower, and velocity on an 8.65 inch twin roll dynamometer.

0.76, 0.33, -0.09 are default 50 mph power fraction values derived from experimental data.

 $GTRL_{@50mph-8} = -0.378193 + 0.0033207*DAXWT$

DAXWT = (VAXF + VAXE)/2

VAXF = Drive axle weight for a vehicle with a full fuel tank from EPA Certification database.

VAXE = Drive axle weight for a vehicle with an empty fuel tank from EPA Certification database.

(D)
$$A_{t20} = \frac{0.65}{50} * (GTRL_{@50mph-20}) hp / mph$$

(E)
$$B_{t20} = \frac{0.48}{2500} * (GTRL_{@50mph-20}) hp / mph^2$$

(F)
$$C_{120} = \frac{-0.13}{125,000} * (GTRL_{@50mph-20}) hp / mph^{3}$$

Where: A_{t20} , $B_{t,20}$, C_{t20} are coefficients relating tire losses, in horsepower, and velocity on a 20 inch twin roll dynamometer.

0.65, 0.48, -0.13 are default 50 mph power fraction values derived from experimental data.

 $GTRL_{@50mph-20} = 0.241645 + 0.0020844*DAXWT$

DAXWT = (VAXF + VAXE)/2

VAXF = Drive axle weight for a vehicle with a full fuel tank from EPA Certification database.

VAXE = Drive axle weight for a vehicle with an empty fuel tank from EPA Certification database.

(2) <u>Look-up Table</u>. The vehicle specific values for GTRL_{@50mph-8} and GTRL_{@50mph-20} using default values for 50 mph power fractions are published in the latest version of the EPA I/M Look-up Table.